

# electronics®

## RADAR MAKES WAR MAPS

*Dishes identify terrain samples, p 20*

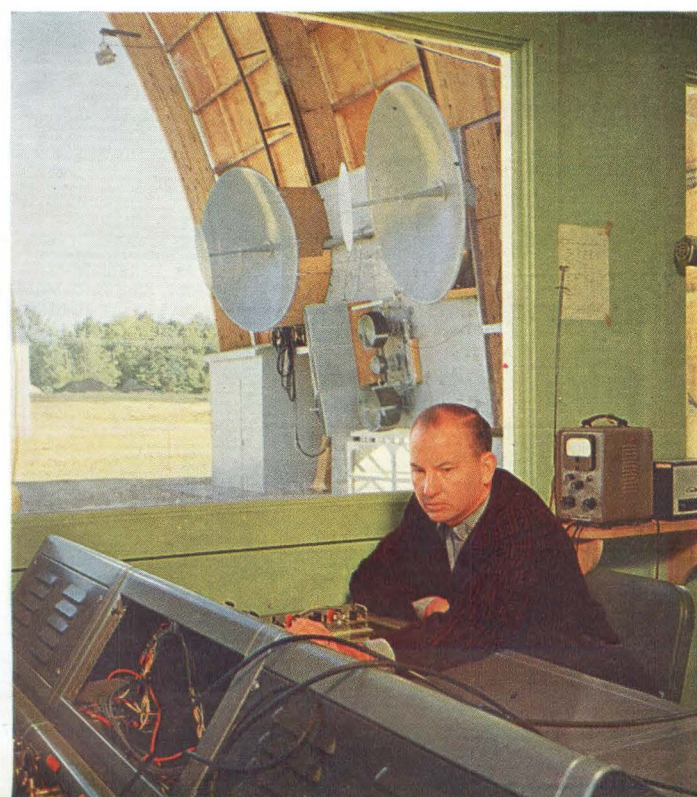
*(photo below)*

## THIN-FILM TRIODES

*What can they really do? p 29*

## SERVO AMPLIFIER ON PINHEAD

*Latest use of linear microcircuits, p 33*



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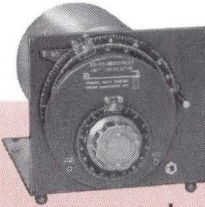
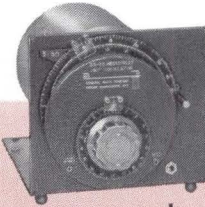

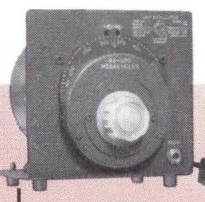

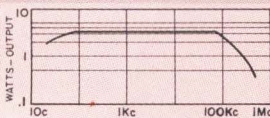
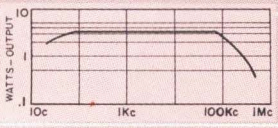
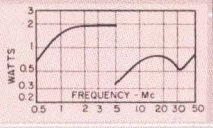
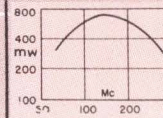
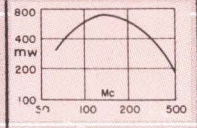
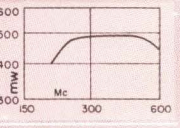


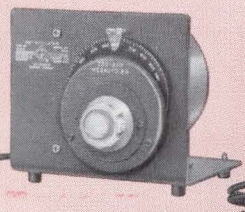
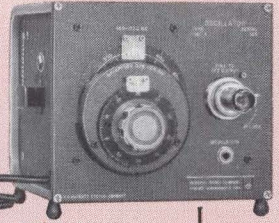
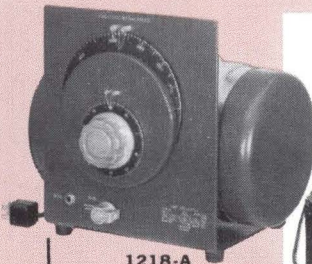
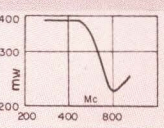
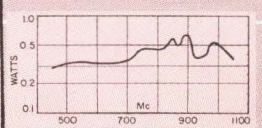
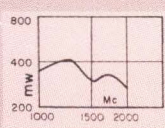
# FREQUENCY IN "CHUNKS"

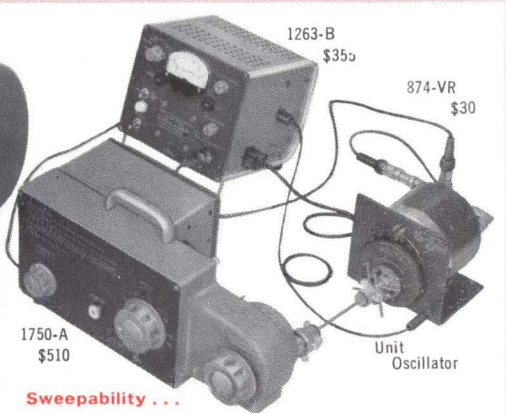


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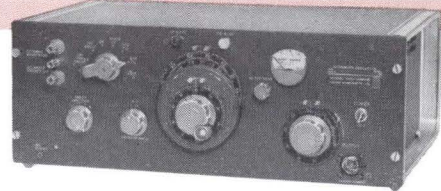
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|                                                                                                                                                                                    |                                                                                                                                                                                                       |                                                                                                                                                                      |                                                                                     |                                                                                                                       |                                                                                                                        |                                                                                                                          |                                                                                   |              |              |              |
|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|--------------|--------------|--------------|
|  <p><b>1203-B</b><br/>Unit Power Supply<br/>required for all<br/>Unit Oscillators<br/>...\$50</p> |  <p><b>1210-C</b><br/>20 cps-0.5 Mc<br/>(5 ranges)<br/>± 3%<br/>less than 1%, essentially<br/>complete in 1 hour</p> |  <p><b>1211-C</b><br/>0.5-50 Mc<br/>(2 ranges)<br/>± 2% at<br/>no load<br/>0.4%</p> | <p><b>Type</b></p>                                                                  |  <p><b>1215-B</b><br/>50-250 Mc</p> |  <p><b>1208-B</b><br/>65-500 Mc</p> |  <p><b>1209-BL</b><br/>180-600 Mc</p> |                                                                                   |              |              |              |
|                                                                                                                                                                                    | <p>3 outputs: Low Z (less than 500Ω) : 0-7v<br/>High Z: 0-45v<br/>Square wave: 0-30v, open circuit</p>                                                                                                | <p><b>Frequency</b></p>                                                                                                                                              | <p><b>Calibration accuracy</b></p>                                                  | <p><b>Warm-up drift</b></p>                                                                                           | <p><b>Specified output into 50Ω</b></p>                                                                                | <p><b>Price</b></p>                                                                                                      | <p><b>Typical output characteristic (Using Type 1203-B Unit Power Supply)</b></p> |              |              |              |
| <p>Output of 1210-C and 1206-B Unit Amplifier, \$90, into 600-ohm load</p>                       |                                                                                                                     |                                                                                    |  |                                   |                                    | <p>\$180</p>                                                                                                             | <p>\$305</p>                                                                      | <p>\$210</p> | <p>\$230</p> | <p>\$260</p> |

|                                                                                                                                                     |                                                                                                                                                       |                                                                                   |                                                                                                                                                        |
|-----------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------|
|  <p><b>1209-B</b><br/>250-960 Mc<br/>± 1%<br/>0.2%<br/>200 mw</p> |  <p><b>1361-A</b><br/>450-1050 Mc<br/>± 1%<br/>0.2%<br/>125 mw</p> | <p><b>Type</b></p>                                                                |  <p><b>1218-A</b><br/>900-2000 Mc<br/>± 1%<br/>0.1%<br/>200 mw</p> |
|                                                                  |                                                                    | <p><b>Typical output characteristic (Using Type 1203-B Unit Power Supply)</b></p> |                                                                     |
| <p>\$260</p>                                                                                                                                        | <p>\$285</p>                                                                                                                                          | <p><b>Price</b></p>                                                               | <p>\$465</p>                                                                                                                                           |



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**RADAR TERRAIN ANALYSIS.** Radar dishes covering K<sub>a</sub>, X, C and P bands travel along track inside the arch and illuminate soil samples below. Army Corps of Engineers uses Texas Instruments installation to determine reflecting characteristics of soils as a function of incident angle and frequency. *When these data are known radar can plot soil maps for tactical purposes and flood control. See p 20* COVER

**AUTO TRAFFIC CONTROLS.** More cities are beginning to use computers, both analog and digital, to unsnarl traffic. *This is a coming market for radar, ultrasonic sensors, tv and radio* 14

**RADAR SOIL ANALYZERS Will Help Army Map Campaigns.** Four-band radar is now gathering soil signatures to aid in system design. *What Army wants is an airborne system, with other sensors as well as radar, that will tell field commanders whether a region's ground conditions are suitable for troop movements* 20

**MAN ON MARS—That's Project Rover's Target.** AEC and NASA are making progress in a three-stage program to develop and fly a nuclear rocket engine. *But a funds squeeze may slow development. The money decision depends on the success of tests in the next six months* 24

**THIN-FILM TRIODES: How Well Will They Perform?** There are three distinct classes of thin-film triodes: space-charge-limited, field-effect or hot-electron devices. Each type has unique advantages and disadvantages. *The SCL triode is fastest; field-effect triodes are easiest to make; hot-electron devices may be most tolerant of radiation.*  
 By W. Tantraporn, General Electric 29

**MICROCIRCUIT SERVO AMPLIFIER.** It's only  $\frac{3}{4}$ -inch square but it can drive a size-8 servo motor. This direct-coupled class-A amplifier contains the equivalent of four dozen components on and within a single silicon block. *So-called inside-out transistors are key to its performance.*  
 By M. W. Aarons, United Aircraft 33

**ELECTROSTATIC KLYSTRONS: New Design Concept.** This S-band klystron produces 15.5 kilowatts peak power with 25-percent efficiency and weighs only five pounds complete. *It uses electrostatic focusing of the electron beam instead of the conventional solenoid or permanent magnet.*  
 By J. R. Hechtel and A. Mizuhara, Litton Electron Tube Corp. 36

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**electronics**

December 28, 1962 Volume 35 No. 52

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By R. P. Rufer and W. A. Karlotski,  
Lawrence Radiation Lab, U. of C. 38

**REFERENCE SHEET:** Faster Selection of VHF Bypass Capacitors. Chart takes inductance of capacitor leads into account and can avoid errors as great as an order of magnitude. *It is useful at frequencies from 1 Mc to 1,000 Mc and with lead-wire gages from Awg 18 to 24.*

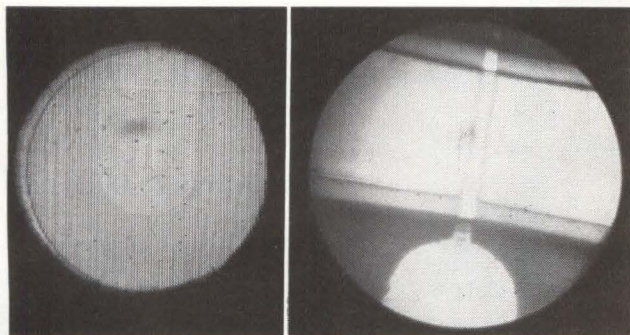
By L. E. Lee, Ball Brothers Research Corp. 44

**DEPARTMENTS**

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# CROSSTALK



**THIN-FILM TUBES.** There is no doubt that the design of future electronic equipment will lean heavily upon the now-developing art of thin-film circuits. Vastly reduced size is but one of the glowing predictions. Significant advantages are anticipated in certain performance parameters, in the cost of mass-produced circuits and in design flexibility.

Considerable progress has been made in production techniques. Methods of making passive devices like capacitors and resistors have been tamed quite successfully. They can be made by a process akin to the household spray gun. But such active components as transistors and diodes don't get built as easily in the form of thin films.

One class of thin-film active device that does respond to the spray-gun approach is the thin-film triode. They can be built up from layers of electrode and insulating materials, producing a solid-state analog of the familiar vacuum tube. The space charge in a solid, for example, can behave like the space charge in a vacuum.

People working on thin-film triodes don't say that there aren't applications better suited to integrated semiconductor circuits. Nor do they contend that there are no more problems to be solved. But several varieties of thin-film triodes have already been built, they do offer easier solutions to some fabrication problems and they do merit the attention of designers working in the microelectronics field.

Because of these considerations—and because it makes for a darned interesting technical story—our lead feature article this week is all about thin-film triodes and how they perform. The author, W. Tantraporn, of GE, sets forth the basic designs and mechanisms for three distinct types: the space-charge-limited (SCL), field-effect and hot-electron versions. And he candidly discusses the advantages, disadvantages

and prospects for each type of triode.

Illustrations in the article show the configurations of these devices schematically, because that makes the explanations easier to follow. The photos here show the hearts of the SCL and field-effect triodes.

On the left is a grid for an SCL triode. Less than an eighth of an inch in diameter, it is formed from lines of gold wrapped in silicon monoxide. On right is a closeup of a field-effect triode's gate electrodes.

●  
**MARKETING REPORT.** New Year's resolutions to do good and work harder are fine for the man in the street, but the businessmen and engineering planners in industry must make plans far more concrete than a few generalizations. This is the time of the year when manufacturers must resolve, in terms of sales and profit prospects, such questions as:

- Are international trends in the electronics field working for or against the manufacturers in the U.S.?

- Is there a profit squeeze in military electronics and if so should we take a longer look at industrial and consumer electronics?

- What about component manufacturing overcapacity?

These are just a few of the questions we asked and got answers to from informed people in the industry during the past few months, while gathering the raw material for our annual market report.

Of course, any manufacturer intimate with a particular facet of electronics has a pretty good idea right now where his specialty stands and where it is heading. The usefulness of our annual market reports—blending as they do informed opinion and statistics on all the facets of the industry—is twofold: it helps one specialist determine what other specialists are up to, and it helps him to determine how to broaden his product range and fit his specialties into growing fields.

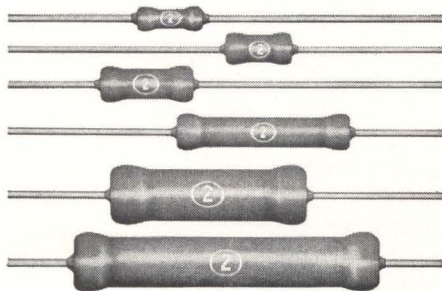
For the latest word on where the electronics industry is heading—**ELECTRONICS**, January 4, 1963.

●  
**EDITORIAL INDEX.** The article-author index beginning on page 59 of this issue is self-explanatory. It represents the end of a series of experiments with respect to frequency and placement.

Next year, we will return to the traditional policy of indexing **ELECTRONICS** just once, in our issue of December 27, 1963. This appears to best meet the needs of a majority of subscribers and, in particular, librarians.



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## COMMENT

### Diodes and Transients

This is in regard to the *Comment* letter from reader P. Prouty (p 4, Nov. 9), which concerned my letters (p 4, Sept. 28) and author S. P. Fairchild's response concerning his article, *Avalanche Breakdown of Silicon Rectifiers* (p 68, June 1).

I have a hard time visualizing how capacitance toward ground could carry enough energy from a single transient to kill a diode. If this were possible, then it would be possible to kill it by applying a d-c overvoltage in series with a capacitor of 10 pf (or whatever the ground capacitance of the diode is), and even though I did not make this experiment, I have a hard time imagining that it should ever succeed.

But what reader Prouty writes under (2) perfectly agrees with what I had merely theorized in the last paragraph of my second letter: that continuous exposure of the diode with (not to) smaller inverse current to its Zener voltage, slowly undermines its resistance to overvoltage, for about 60 percent of diodes available. Then, if we use four diodes in series without the screening reader Prouty suggested, we have a chance of  $(0.6)^4 = 13$  percent, of getting failure. This percentage agrees with the order of magnitude of experienced failures.

JOSEPH C. FROMMER  
Cincinnati, Ohio

Reader Prouty's reply includes a drawing of a series diode string and calculations to show that if a 15,000-volt pulse is impressed across 50 cells, then the voltage across a diode is 5,400 volts, "certainly an impressive value." He continues:

To the best of my knowledge, the exact mechanism by which a voltage transient destroys a semiconductor junction is not well understood. It does appear, however, that the destruction occurs in sub-microsecond times and with only small amounts of energy being consumed in the process. Therefore, calculations

based on the time duration of the transient and the stored charge in the stray capacitances will have to be applied very carefully—particularly if they are to be used to establish criteria for an acceptable situation.

T. P. PROUTY  
MHD Research, Inc.  
Newport Beach, California

### To Obsolete Or Not To Obsolete

Much has been written about engineers' inability to write English well. Naturally we look to ELECTRONICS to lead the way. Imagine my astonishment, therefore, to find in your Nov. 23 issue (p 3) your use of "obsolete" as a verb. I am wondering if you are going to fall in the same class as writers of cigarette ads and write "like" an editor should not.

JULIAN LOEBENSTEIN  
General Instrument Corporation  
Newark, New Jersey

Our dictionary says the use of "obsolete" as a verb is "now rare." In using it as a verb, we have either gone back to the time when it was common to do so, or have moved ahead to the future, when it may again become acceptable by repeated usage. It's only a case of being out of sync.

### Feedline Impedances

I am very pleased with your presentation of my article, *Smith-Chart Short Cut Renormalizes Feedline Impedances* (p 53, Nov. 16).

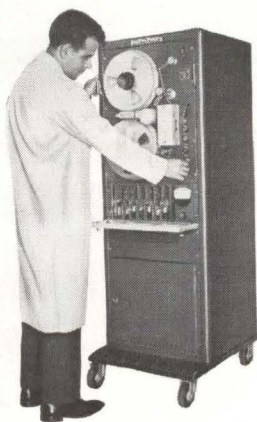
I detect two errors, however, which somehow slipped through. On p 54 under "Broadband Matching," third paragraph, third line, "counterclockwise" should read "clockwise," because the impedance locus is transformed from the antenna (load) towards the generator.

The second error, albeit minor, is in Fig. 1, where the arrows should point clockwise in order to be consistent with the text.

DONN V. CAMPBELL  
U. S. Army Electronics Research  
and Development Laboratory  
Fort Monmouth, New Jersey



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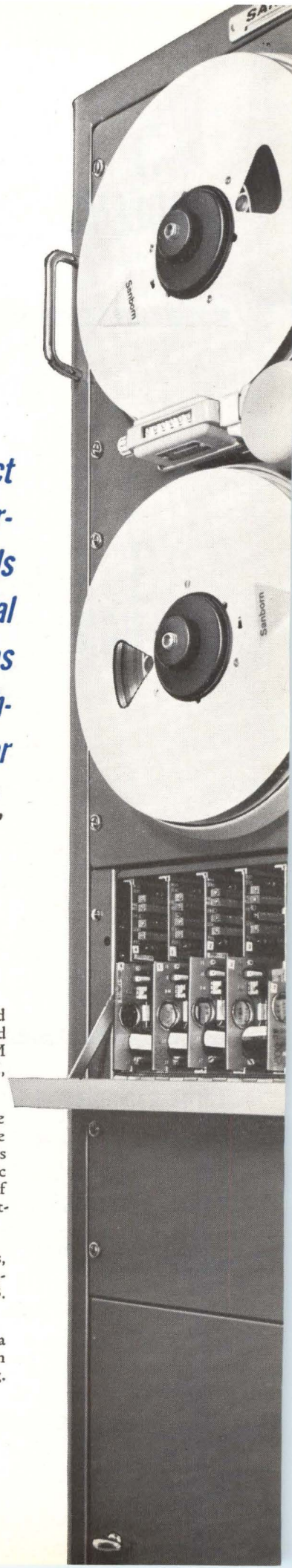
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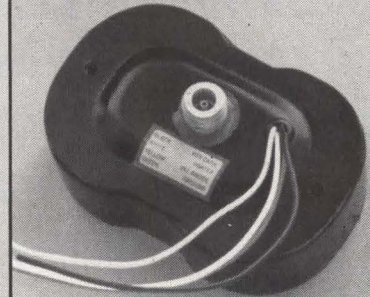
# 3 PROBLEMS

1. Light-weight, frequency-stable, efficient 10-watt S-Band oscillator for telemetry. Must operate at low voltage, be easily frequency-modulated, small, simple and reliable; must generate minimum stray electromagnetic interference; and must meet typical missile environment specifications.

2. Amplifier of at least 10 watts output over octave bandwidth 4.0 to 8.0 Gc, with minimum of 40 db saturated gain. Must not require separate power for focussing, nor forced air or liquid cooling. Size and weight must be minimum to meet typical missile environment specifications.

3. 15-watt oscillator voltage-tunable over 12% bandwidth in L-Band. Linear frequency/anode voltage characteristic required. Minimize frequency drift with temperature. Must be self-contained; only electrical connections; no mechanical adjustments. Minimum size and weight to meet typical missile environment specifications.

# 3 SOLUTIONS



# 1 COMPANY



Three examples of the way Eimac, by creative engineering, meets tomorrow's tube needs today.

**X1005 Supported Drift Tube Klystron... developed under AF33 (616)-8403...**  
 Weight: 2 $\frac{5}{8}$  pounds  
 Frequency Stability: 0.005%  
 Efficiency: Above 15%  
 Power Output: 10 watts CW  
 Frequency: 2.2 to 2.3 Gc.  
 Beam Voltage: 1500  
 Size: 4 x 4 x 4 $\frac{1}{2}$  inches overall  
 Focussing: Entirely internal, no magnets or coils  
 Environmental: Meets typical missile specifications.

**X1021 Traveling Wave Tube**  
 Power Output: 10 watts min.  
 Frequency Range: 4.0 to 8.0 Gc.  
 Saturated Gain: 40 db  
 Focussing: PPM  
 Cooling: Heat sink  
 Size: 13 x 1.83 x 1.89 inches  
 Weight: 3.5 pounds  
 Environmental: Meets typical missile specifications

**X1086 Voltage Tunable Magnetron**  
 Power Output: 15 watts min.  
 Power Output Variation: 1.5 db  
 Freq. & Bandwidth: 12% in L-Band  
 Frequency/Anode Voltage: Linear  
 Temperature Compensation: 0.008% of operating frequency/°C.  
 Electrical Connections: Heater, anode, injection voltage only  
 Output: Coaxial  
 Focussing: Permanent magnet  
 Size & Weight: 5 x 3 x 2 in.; 3.2 lbs.  
 Environmental: Meets typical missile specifications

More reasons to keep your eye on Eimac—for advanced microwave tubes, high power klystrons, power grid tubes, accessories. Eitel-McCullough, Inc., San Carlos, California. Subsidiaries: Eitel-McCullough, S.A., Geneva, Switzerland; National Electronics, Geneva, Ill. **KEEP YOUR EYE ON**





## DOD Casting Friendlier Eye on Dyna-Soar

DEFENSE DEPARTMENT will probably grant Air Force's request for \$135 million in fiscal 1964 for X-20 (Dyna-Soar). DOD had cut \$10 million, but Air Force is now substantiating the need and believes DOD will ask Congress for the full amount next month.

The program is on schedule. Air Force sees no technical problems to prevent development of the manned orbital glider. More money would, however, buy better subsystems. One that would be replaced is the guidance system.

Flights are to begin in early 1965 with a manned drop from a B-52. Titan III will boost an unmanned glider into orbit in late 1965 and a manned one in 1966. Titan III's second, third and fourth stages will be test fired in 1964.

Congress has shown more enthusiasm for X-20 than DOD. In 1962, Air Force asked for \$185 million and Congress appropriated it. DOD only wanted \$100 million and that's all it gave Air Force.

For 1963, DOD requested \$135 million, got \$157 million, but so far has only released \$60 million. Air Force hopes it gets at least the other \$75 million in the next six months.

## Ship-Base Polaris for Britain Deal is Cooking

WASHINGTON—As President Kennedy and Prime Minister Macmillan met at Nassau last week, Skybolt's fate was virtually sealed. Washington was prepared to offer Britain an alternative strategic nuclear weapon and the candidate was Polaris.

The U. S. appreciates Macmillan's political requirement for big nuclear weapons, say sources here, so Washington agreed to consider a British request for Polaris as an alternative to Skybolt.

As we went to press, odds were that an agreement would be reached to sell Polaris missiles to Britain, probably for deployment on surface vessels. The British are apparently in no shape to invest heavily in a fleet of missile-armed subs.

The British are not interested in Minuteman. They prefer mobile

---

missiles, not fixed-base missiles that could draw enemy fire to their island.

## Operational Transit Is Launched, Receiver Fails

MUCH OF THE USEFULNESS of the first operational Transit satellite, launched last week, was washed out by a failure in the command receiver. The system (p 148, Aug. 11, 1961) is designed to give precise navigational fixes. Day-to-day accuracy depends on corrected orbital data that was to be fed from computers at Point Mugu, Calif.

Navy officials said another Transit will be sent up in about 60 days. A four-satellite network is planned. Polaris submarines with position-keyed guidance systems should be principal early beneficiaries of the program. Position data, for ships or missile guidance systems, is automatically prepared when the ship-board system receives signals from the satellite. The equipment is now in place on some naval vessels.

The equipment may soon be made available to commercial navigators under agreements being worked out by the Defense Department and

NASA. Contractors for the Navy navigation sets (AN/BRN-3) include Westinghouse Electric, Thompson Ramo Wooldridge and Chew Associates. Johns Hopkins' Applied Physics Lab supervises the project.

## French Hope to Make Indium-Arsenide Laser

PARIS—Prof. Pierre Aigrain, of the Ecole Normal Superieure, has informed ELECTRONICS that his research group has developed theory for an indium-arsenide laser. They hope to have a device ready in time for the Quantum Electronics Symposium here in February.

Work done so far indicates the laser wavelength is 3 microns, compared to 0.85 micron for a gallium-arsenide laser (p 24, Nov. 16), and conversion efficiency is potentially 100 percent.

## Infrared Diode Transmits Voice on 30-Mile Path

BOSTON—MIT Lincoln Laboratory has had moderately good success in transmitting voice over a 30-mile path, using its infrared-generating gallium-arsenide diodes (p 44, Oct. 5) as a source of incoherent radiation. Development of the devices as lasers is also continuing, as is research with other materials, including gallium phosphide.

Emission of high-intensity infrared radiation at 1.6 microns has been observed from forward-biased

---

## Hot Line to Moscow Idea Cools Down

ALL THAT TALK about a Kennedy-Khrushchev hot line is still just talk. Nothing was down on paper last week, said the White House. The President, himself, twice doubted it would be a panacea. He says faster communication is desirable, not crucial.

If a hot line is installed, it would probably be a teletypewriter circuit, to provide printed records. But unless plain language is used, coding and decoding would consume time. One wag said that "if your readers would develop a machine to automatically code and translate presidential prose, we might get somewhere."

There's no problem with plain language messages. Contact has been made by open telephone (by the Soviet Embassy in Washington), radio and broadcasts in the past



gallium-antimonide *p-n* junctions. Optical pumping of the base material produces the same radiation spectrum as *p-n* junction injection.

MIT researchers have noted lack of significant line shifts in absorption measurements and in measurements in magnetic fields up to 90 kilogauss. This indicates, they say, that the radiation is not produced by band-to-band transitions and that it is probably connected with impurities. The radiation spectrum is changed a different impurity.

## South Africa Installing 600-Transmitter F-M Net

BONN—Siemens, Telefunken and Rohde & Schwarz have received the lion's share of orders for the first stage of South Africa's f-m station network. First stage includes 80 transmitters.

Bids for the second stage, 100 transmitters, will be published in early 1963. When the network is completed in 1967 it will have cost \$47.5 million and have 600 transmitters at 127 stations.

Each station will have 5 or 6 transmitters to broadcast programs in European and native languages. Switching systems enable 4 to 6 transmitters to use a common antenna.

F-m radio sales in South Africa have been booming, especially in native regions. Most sets sold come from Japan and cost \$50.

## Modulation Technique Handles 20 Megabits

YORKTOWN HEIGHTS, N. Y.—Computer information at the rate of 20 million bits a second has been transmitted over a conventional 40-mile microwave tv link by IBM Advanced Systems Development division. Another modulation technique transmitted 8,000 bits a second over a high-quality telephone line.

Emil Hopner, computer communications manager, said a tv-type channel offers possibilities for higher-speed computer communications because it has broad bandwidth and is designed for pulse transmission like the binary signals of computer language. Simple equipment can translate signals between computers and the tv link.

Basically, the system accepts two 10-megabit binary channels and encodes them into a composite signal with amplitude and polarity level dependent on instantaneous relationship between 0's and 1's. The outgoing 20-megabit composite signal modulates the microwave transmitter. At the receiver, a decoder clocks each pulse and delivers the two 10-megabit outputs that are fed to an encoder. The composite signal is recreated and passed through a low-pass filter back to the decoder to serve as the d-c restoration circuit.

## First Look at Mariner Data Puzzles Scientists

FIRST LOOK at the data gathered by Mariner II is puzzling NASA scientists. Tentative analysis shows that Venus has a smaller magnetic field than Earth and that its cloud cover is solid rather than broken by surface winds or other weather conditions.

Data on the magnetometer experiment was to be presented this week at the American Association for the Advancement of Science, in Philadelphia, and results on five other experiments at the American Geophysical meeting at Palo Alto, Calif.

If it turns out that Venus has a magnetic field like Earth, this will support theories that Venus was formed much like Earth and still has a hot interior. A weak field could mean that Venus spins very slowly.

## No Luck in First Ion Engine Test In Space

FIRST TEST of an ion engine in space was attempted by Air Force from Point Arguello, Calif. last week. Although the booster vehicle successfully placed the experimental equipment in the desired trajectory, Air Force said the ion engine could not operate due to a partial power failure.

This test was the first in a long-range program to investigate feasibility of electric propulsion systems for space applications being carried out by the Air Force Systems Command. The ion engine was a cesium-type made by Electro-Optical in an 80-lb. package.

## In Brief . . .

ADMIRAL and Motorola are both predicting black-and-white tv sales will be 6 million sets in 1963. Admiral expects 700,000 color set sales will increase total tv dollar volume by 10 percent.

ANOTHER seismological observatory for Project Vela-Uniform (p 28, Feb. 23, and p 28, May 18) was dedicated last week. Contractors are Texas Instruments and Geotechnical Corp.

RYAN AERONAUTICAL'S new VTOL flight simulator includes a panoramic wrap-around screen to give the pilot peripheral vision. The projector is tied to an analog computer.

AEROSPACE Industries Association sees an aircraft, missiles and space market as high as \$16 billion in 1963. Estimate for 1962 is \$15.5 billion.

BRITAIN won't be getting a second commercial tv network. The government said no. But it is giving BBC another channel and may permit pay-tv.

CON EDISON has asked AEC for permission to build a nuclear power plant in the Queens section of New York City. The 1,000-Mw plant would be the first built inside a city.

NIKE ZEUS passed its last test at Point Mugu, Calif. Army said all three stages of the rocket fired as planned. Testing will continue at White Sands, N. M., and Kwajalein.

THIS COUNTRY'S 200th ICBM went on the firing line last week. Strategic Air Command took over a 12-missile Atlas squadron at Plattsburgh AFB, N. Y. This completes the planned Atlas force.

FAIRCHILD CAMERA & Instrument will produce an advanced photo reconnaissance system for the Air Force. It will provide horizon-to-horizon coverage.

MOLECU-WIRE has been purchased by Superior Tube, which will operate it as a subsidiary.



ANOTHER SOLID-STATE INNOVATION  
FROM INTERNATIONAL RECTIFIER

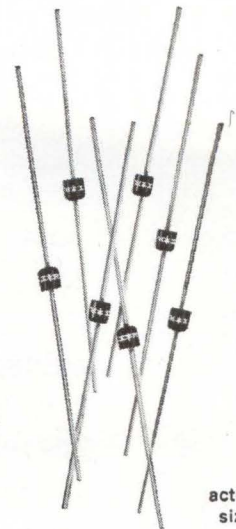
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1st of its kind, this new subminiature IR silicon rectifier series offers many circuit optimizing benefits.

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0.90 max. FVD... at 25°C and 1000 mA, d-c (0.50 volt max. at 500mA, F.C.A. and 100°C).

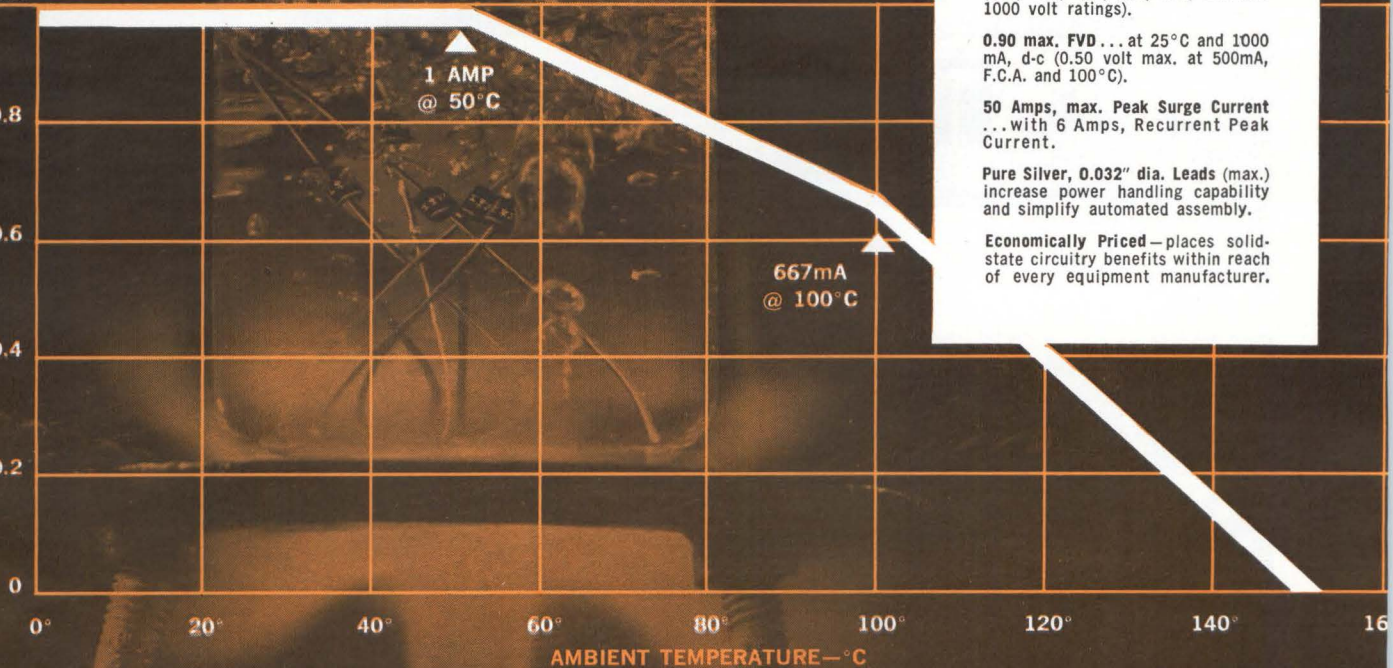
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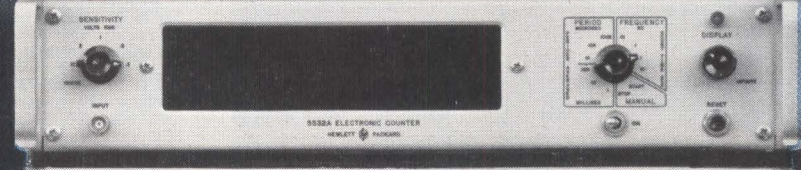
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# time related measurements

with

# 9



5211B

5512A

5212A

5532A

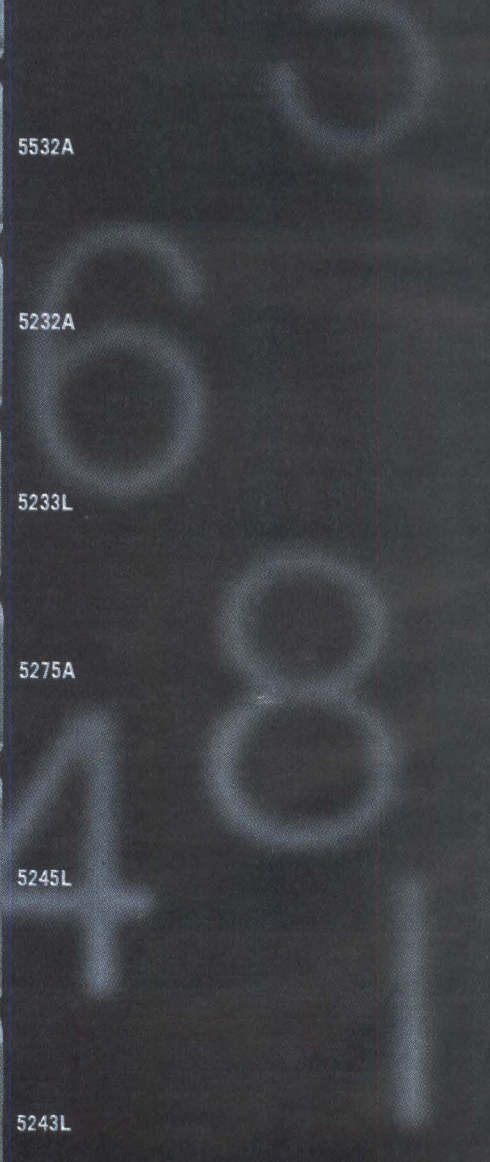
5232A

5233L

5275A

5245L

5243L





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Hewlett-Packard modular construction introduces counters that are bench and rack mount models in a single instrument, front panels are only  $3\frac{1}{2}$ " or  $5\frac{1}{4}$ " high. Operation is simple, straightforward, making every human-engineered instrument in the line easy to use, even by untrained personnel.

Check the brief description of individual models here. Then check your nearest representative or contact Hewlett-Packard direct for full information and demonstration of the instrument designed specifically for your job:

Ⓢ 5245L — Makes more measurements with greater accuracy than any other counter available today: Measures frequency, time interval, period, multiple period average, ratio, multiple ratio, scales by decades. Measures to 50 mc directly, 100 mc and 512 mc with plug-in converters. Additional plug-in permits time interval measurements. Time base stability, 3 parts in  $10^6$ /day. 8-digit resolution in rectangular, close-spaced numeric indicator tubes. Remote programmability of time base and function controls. Ⓢ 5245L 50 MC Counter, \$3,250.00. Ⓢ 5251A Frequency Converter, to extend counter frequency to 100 mc, \$300.00; Ⓢ 5253A Frequency Converter, to extend counter frequency from 100 to 512 mc, \$500.00; Ⓢ 5262A Time Interval Unit, 0.1  $\mu$ sec resolution, \$300.00.

Ⓢ 5243L — Identical to Ⓢ 5245L, but measures directly to 20 mc, \$2,950.00.

Ⓢ 5233L — This 2 mc counter measures time interval, frequency, period, multiple period, ratio, and multiples of ratio. Featuring 6-digit resolution in an in-line display of rectangular digital in-line tubes and superior trigger, level controls. Price, \$1,850.00.

Ⓢ 5232A, 5532A — These 1.2 mc counters measure frequency, period, multiple period average and ratio. Offering 6-digit resolution, they are identical except for readout. The 5232A provides display in improved neon columns, while

the 5532A provides display in long-life numeric indicator tubes. Operating temperature range, as with the other Ⓢ solid state counters, is  $-20$  to  $+65^{\circ}$  C. Ⓢ 5232A, \$1,300.00; Ⓢ 5532A, \$1,550.00.

Ⓢ 5212A, 5512A — Five-digit resolution is provided by these counters, which have a maximum counting rate of 300 kc. They measure frequency, period, multiple period average and ratio. The two instruments differ only in display, the 5212A presenting neon columnar readout, and the 5512A offering digital in-line tube readout. Ⓢ 5212A, \$975.00; Ⓢ 5512A, \$1,175.00.

Ⓢ 5211A, B — These counters use line frequency as a time base and measure frequency directly to a maximum counting rate of 300 kc, and they also measure ratio. They furnish 4-digit resolution with neon columnar display. The 5211A offers gate times of 0.1 second, 1 second, and manual. The 5211B offers an additional gate time of 10 seconds. Otherwise, the instruments are identical. Ⓢ 5211A, \$750.00; Ⓢ 5211B, \$825.00.

Ⓢ 5275A — This counter measures time interval 10 nsec to 0.1 sec., with 10 nanosecond resolution. The instrument counts 100 mc by a 100-to-1 multiplying circuit. Seven-digit display is in neon columns. Separate 1 mc time base, such as Ⓢ 101A required. Ⓢ 5275A, \$3,250.00; Ⓢ 101A, \$500.00.

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# WASHINGTON OUTLOOK

## BIDDING FOR SATELLITE STOCK STARTS JANUARY 2

**COMMUNICATIONS COMPANIES** can start filing January 2 for authorization to buy stock in the new, privately owned satellite communications company. FCC will determine what communications companies will own stock. There is little chance of any company being denied ownership rights, says an FCC spokesman. Actual stock sales are not expected for several more months.

There is no limit to how much stock a single company can own, but FCC has power to force stock sales between companies to insure wide distribution. Also, half the stock must be held by the general public. Some companies, including AT&T, wanted more definitive rules on initial stock allocations and subsequent offerings, but the FCC has adopted without amendments the rules it had previously proposed.

## CAN CIVILIANS SPEND THAT MUCH MONEY?

**THOSE RUMORS AND DENIALS** about Gen. Lauris Norstad being offered the presidency of the satellite communications corporation point up the caliber of person the 13-man group of incorporators want. Norstad, the allied commander in Europe, quickly denied a job offer was made. Sources close to the embryo company deny that a military man will be picked because that would give the company a semigovernment image, instead of carrying out the private company concept.

Picking a politically acceptable president is not the only problem facing the satellite corporation. Since the corporation will have to lean heavily upon what government programs have taught about communications satellites, the failure of the Relay satellite this month was a sobering development. It emphasized the problems—and costs—of establishing a working system of 30 to 50 satellites.

## KENNEDY TO TRY AGAIN FOR EDUCATION ACT

**THE WHITE HOUSE** will attempt early in the next Congress to win approval of a science and engineering education program. President Kennedy has spoken of the need twice in the last several days and his science adviser, Jerome B. Wiesner, recently made the same point in one of his rare public addresses. Both are seen as laying the political groundwork for the manpower needs report recently issued by a special panel of the President's Science Advisory Committee (p 8, Dec. 21).

The panel recommended an annual outlay rising to \$760 million a year by 1970, for student support and facilities. The panel proposes not only enriching the stream of trained personnel into the electronics and space fields, where talent is becoming concentrated, but improving the sources that feed all the nation's technical and economic needs.

## RULE ON LOUD TV ADS HANGS ON TECHNIQUES

**FCC ENGINEERS** think they may soon come up with objective measurements of factors contributing to objectionable loudness in radio and tv commercials. FCC plans a new rule, aimed at preventing too much contrast between commercials and programs. Volume alone is a minor problem. Rapid-fire delivery, volume expression, and recording techniques seem to cause many of the complaints FCC gets about excessive loudness. When the FCC engineers can measure these factors, the Commission will enact new controls.



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Indium Antimonide is available in a variety of grades with electron mobilities up to 800,000 cm<sup>2</sup>/volt-sec (78°K) and net carrier concentrations from 10<sup>14</sup> to 10<sup>18</sup> cm<sup>-3</sup> (78°K). We supply single and polycrystalline forms to your specification.

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Thermoelectric cooling alloys are available as dimensioned rods and capped elements of rectangular cross section having a figure of merit of 2.8 to 3.0 x 10<sup>-3</sup> per degree Centigrade. With matched elements, a  $\Delta T$  of 73°C-75°C, measured in vacuum, can be developed with the hot junction at 300°K.

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| product  | grade          | bars           | sheets | wire | powder | shot           | rod            | ribbon | preforms <sup>3</sup> | salts          |
|----------|----------------|----------------|--------|------|--------|----------------|----------------|--------|-----------------------|----------------|
| ALUMINUM | 59             |                | ✓      | ✓    |        |                | ✓              |        | ✓                     |                |
|          | 69             | ✓              | ✓      | ✓    |        |                | ✓              |        | ✓                     |                |
| ANTIMONY | 59             | ✓ <sup>4</sup> |        |      | ✓      | ✓              |                |        |                       |                |
|          | 69             | ✓ <sup>4</sup> |        |      | ✓      | ✓              |                |        |                       |                |
| ARSENIC  | 69             | ✓ <sup>5</sup> |        |      | ✓      |                |                |        |                       | E <sup>2</sup> |
| BISMUTH  | 59             | ✓              |        |      | ✓      | ✓              | ✓              |        |                       |                |
|          | 69             | ✓ <sup>4</sup> |        |      | ✓      | ✓              | ✓              |        |                       |                |
| CADMIUM  | 59             | ✓              | ✓      | ✓    | ✓      | ✓              | ✓              |        | ✓                     | ✓              |
|          | 69             | ✓ <sup>4</sup> | ✓      | ✓    | ✓      | ✓              | ✓              |        | ✓                     |                |
| GOLD     | S <sup>1</sup> |                | ✓      |      |        |                |                |        | ✓                     |                |
|          | 59             |                | ✓      |      |        |                |                |        | ✓                     |                |
| INDIUM   | S <sup>1</sup> | ✓              | ✓      | ✓    | ✓      | ✓              | ✓ <sup>6</sup> | ✓      | ✓                     | ✓              |
|          | 59             | ✓              | ✓      | ✓    | ✓      | ✓              | ✓ <sup>6</sup> | ✓      | ✓                     | ✓              |
| 69       | ✓ <sup>7</sup> |                |        |      |        |                |                |        |                       |                |
|          | 69             | ✓ <sup>4</sup> | ✓      | ✓    | ✓      | ✓              | ✓              | ✓      | ✓                     | E <sup>2</sup> |
| LEAD     | 59             | ✓              | ✓      | ✓    | ✓      | ✓              | ✓              | ✓      | ✓                     |                |
|          | 69             | ✓ <sup>4</sup> | ✓      | ✓    | ✓      | ✓              | ✓              | ✓      | ✓                     |                |
| SILVER   | 59             | ✓              | ✓      |      | ✓      | ✓ <sup>8</sup> | ✓ <sup>8</sup> |        | ✓                     |                |
|          | 69             | ✓ <sup>8</sup> | ✓      |      | ✓      | ✓ <sup>8</sup> | ✓ <sup>8</sup> |        | ✓                     |                |
| TIN      | 59             | ✓              | ✓      | ✓    | ✓      | ✓              | ✓              |        | ✓                     |                |
|          | 69             | ✓ <sup>4</sup> | ✓      | ✓    | ✓      | ✓              | ✓              |        | ✓                     |                |
| ZINC     | 59             | ✓              | ✓      | ✓    | ✓      | ✓              | ✓              |        | ✓                     |                |
|          | 69             | ✓ <sup>4</sup> | ✓      | ✓    | ✓      | ✓              | ✓              |        | ✓                     |                |

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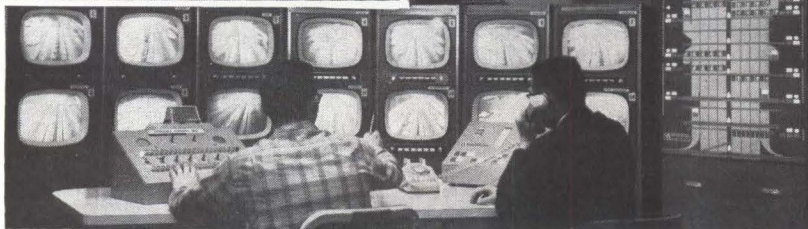
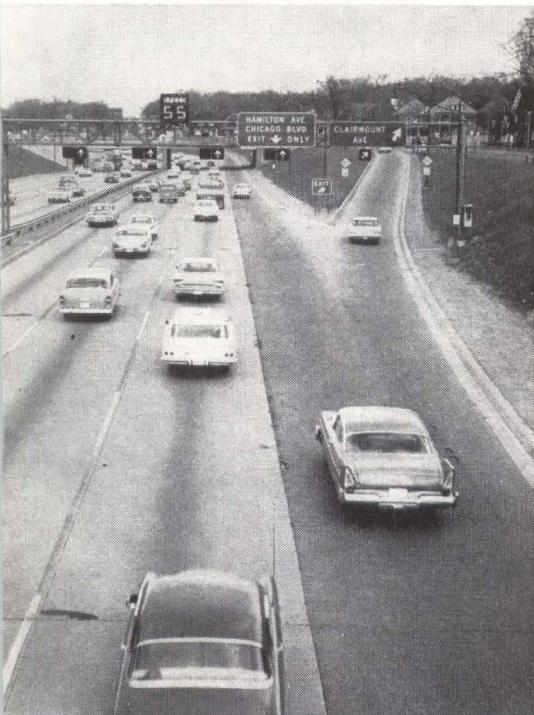
# More Computers Going into

*Both analog and digital types are now being used in several cities*

By **STEPHEN B. GRAY**  
Assistant Editor

**ELECTRONIC CONTROL** of vehicular traffic has quietly grown from a highway curiosity to an everyday working tool over the past five years. Within the past six months alone, seven major installations have been added to the traffic control networks of six large cities, and more on the way.

*SPEED AND LANE signals on John C. Lodge Freeway, in Detroit*



**TELEVISION MONITORING** and traffic-control center for the Detroit freeway with confirmation panel at right

Among the latest developments are:

- Emphasis is being placed on computers. Analog, digital and combination systems are all being actively used and studied.

- New vehicle detection methods to provide computer inputs. Ultrasonics is starting to compete with radar, magnetic detectors and pressure plates.

- Growing use of radio to transmit the collected data to central control locations. Radio is often cheaper than laying cables—one-third as expensive in New York, for example.

**TV MONITORS**—Last May, a big closed-circuit television system began monitoring a 3.2-mile north-south stretch of the John C. Lodge Freeway near mid-town Detroit. The freeway carries as many as 180,000 vehicles a day.

The tv system, installed by General Electric, has 14 cameras mounted on bridges crossing the freeway. Each camera has a one-inch wide-angle lens for general viewing and a six-inch telephoto lens for fine detail. The camera turrets are rotated from the control center, where they are monitored.

Freeway signs show motorists the most efficient driving speed and which lanes are open to traffic. A red  $\times$  over a lane closes it to traffic

when the lane is blocked. A green arrow means the lane is open. Entrance ramp signals regulate the amount of traffic entering the road.

The signals, actuated from the control center, are confirmed by a panel that is a miniature replica of the expressway and its speed and lane indicators. The operator, using data from traffic sensors and observing the 14 tv monitors, can change the control signals as traffic conditions change.

**ANALOG COMPUTER**—Pin-point data on the freeway's traffic is collected by 21 ultrasonic doppler detectors that measure traffic along the route. An analog computer keeps a simultaneous record of traffic speed, volume and occupancy for each lane.

The sensors and computer are made by General Railway Signal Company, which recently installed a similar system to monitor five miles of the Congress Street Expressway in Chicago.

This system has 34 ultrasonic detectors. Analog information is converted to digital data on punch-cards. Cards are processed on a general-purpose digital computer for traffic analysis studies. Operators can anticipate traffic interference far ahead of its occurrence. Minute-by-minute averages of traffic parameters can be computed.

**DIGITAL COMPUTER** — Last spring, four miles of Sunset Boulevard west from downtown Los Angeles went under control of a Thompson Ramo Wooldridge RW-300 digital computer.

The computer receives information on traffic volume and movement, by phone lines, from magnetic and pressure-type detectors buried in and around the controlled section. The computer uses this data and a stored analysis program continuously to determine the optimum duration of the green lights.

**PRESET TIMING** — Automatic-Signal division of Laboratory for



# Auto Traffic Controls

## WHAT PRICE AUTOMATION?

How much would it cost to automate the traffic controls in an American city?

Any driver who has done battle with the rush-hour traffic in downtown New York City knows that there are few cities that offer more room for improvement in traffic controls.

Starting late next year, New York plans to install new traffic light systems—and computers to control them—in the lower half of Manhattan, from 59th Street to the Battery.

Cost has been estimated at more than \$10 million. With other areas in Manhattan, Bronx, Brooklyn, Queens and Staten Island added, cost would be \$21 million.

New York is considering spending \$14 million over 18 months

Electronics makes a system in which an analog-type computer continuously monitors traffic density and volume with pressure, magnetic or radar detectors.

The system selects the optimum combination of any one of six manually preset cycle lengths and several other timing factors. Data from detectors and instructions to the local intersection controllers are transmitted by a 960-Mc Motorola radio system.

An Automatic Signal installation in Los Angeles uses pressure-sensitive detectors. Interrogated every 1½ seconds, the detectors report traffic counts to a control center in city hall. The system can handle up to 32 detectors at this speed.

A recently completed Seattle installation uses six radar vehicle detectors to control 22 traffic signals in a rural section and an industrial section. Both sections can be handled independently or synchronized, as traffic dictates.

Automatic Signal is also installing a system to control more than 65 intersections throughout Boston's Back Bay.

**PRETIMED SYSTEM** — Around Christmas, Tampa, Fla., will open a radio traffic control system. The radio portion, punched-tape programmer and coding device are made by Motorola. Traffic detectors, interrogators and special analog computer are made by Eagle Signal Company.

The Tampa system is being installed as a pretimed system, with a punched paper tape controlling a large number of predetermined cycle changes. The punched tape controls a 24-hour period. By using codes, various programs can be intermixed on one tape. Programs will automatically change for the different days of the week, or for such special situations as parades.

Planned expansion would make the system a "universal" type, by adding capability for actuated control. Various time cycles would be automatically activated as the number of vehicles passing a given intersection increased or decreased. The vehicle-count intersection controllers would also be supplied by Eagle Signal.

## Lunar Seismometers Will Now Check Ocean Bottom

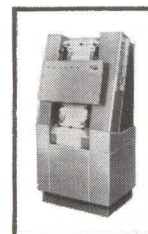
OCEAN-BOTTOM seismometers and recorders, for use at depths to 15,000 feet, have been designed by the United GeoMeasurements division of United Electro-Dynamics for Scripps Institute of Oceanography. They contain a modification of UGM's lunar seismometers. A digital programmer operates the recorder at desired time intervals and provides real-time correlation of data. Upon completion of the recording, the system rises to the surface for recovery and analysis.

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Samuel Johnson

These are the trademarks of some of our customers—each an important contributor to a dramatically growing industry. We at Potter pledge our diligence and skills to this growth through a constantly expanding program of research and development.

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**Model LP-1200  
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to modern computer systems. This high-performance, extremely reliable printer provides speeds of 1000 lines per minute with a maximum of 160 columns. An optional Format Control feature permits multi-page forms or books to be printed with completely flexible horizontal or vertical format and up to five carbons.

The Potter LP-1200 reflects the engineering-knowledge gained from extensive experience and research in high-speed printing. Solid-state modular electronics enhance reliability and sturdy, simple mechanical design readily adapts to meet customer requirements.

Three models are available: LP-1200-160 (160 columns), LP-1200-132 (132 columns) and LP-1200-80 (80 columns).

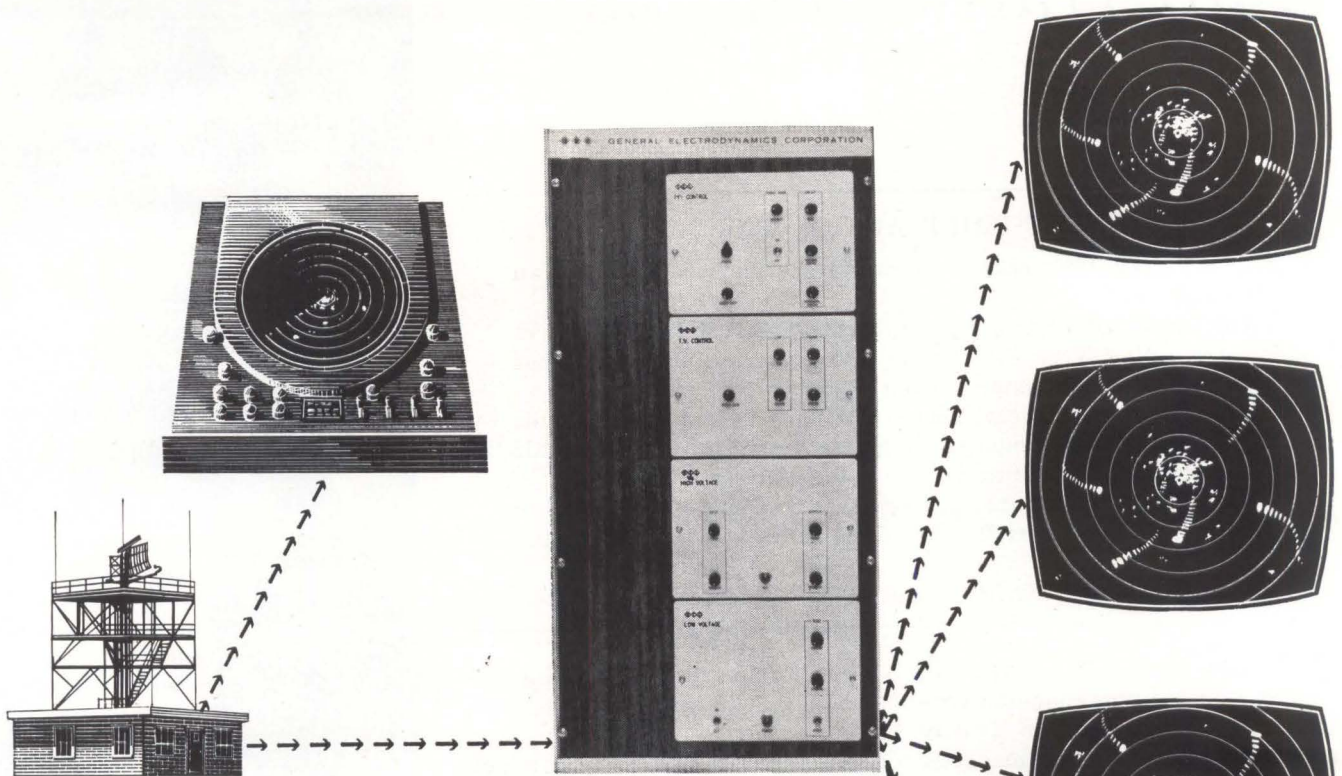
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## Now Multiple PPI Displays Under High Ambient Light Conditions... With G E C Scan Converter

With GEC's *transistorized* 6021 Scan Converter, it is no longer necessary to look at rapidly decaying PPI displays in dark surroundings. Any number of inexpensive TV monitors can be operated from one PPI source with controlled image storage time affording more reliable evaluation of displayed information.

Readily tailored to your specific requirements through its plug-in functional modules, the 6021 Scan Converter is capable of:

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◆◆◆ STORAGE and INTEGRATION of video information.

◆◆◆ TIME-COORDINATE TRANSFORMATION for expansion or reduction of bandwidth.

Contact GEC for more information about conversion of radar PPI to TV, TV standards conversion or conversion of slow scan narrow band TV to standard TV or vice versa.

Qualified electronic engineers are needed for work in the field of Scan Conversion. Address inquiries to Professional Placement Manager. An equal opportunity employer.

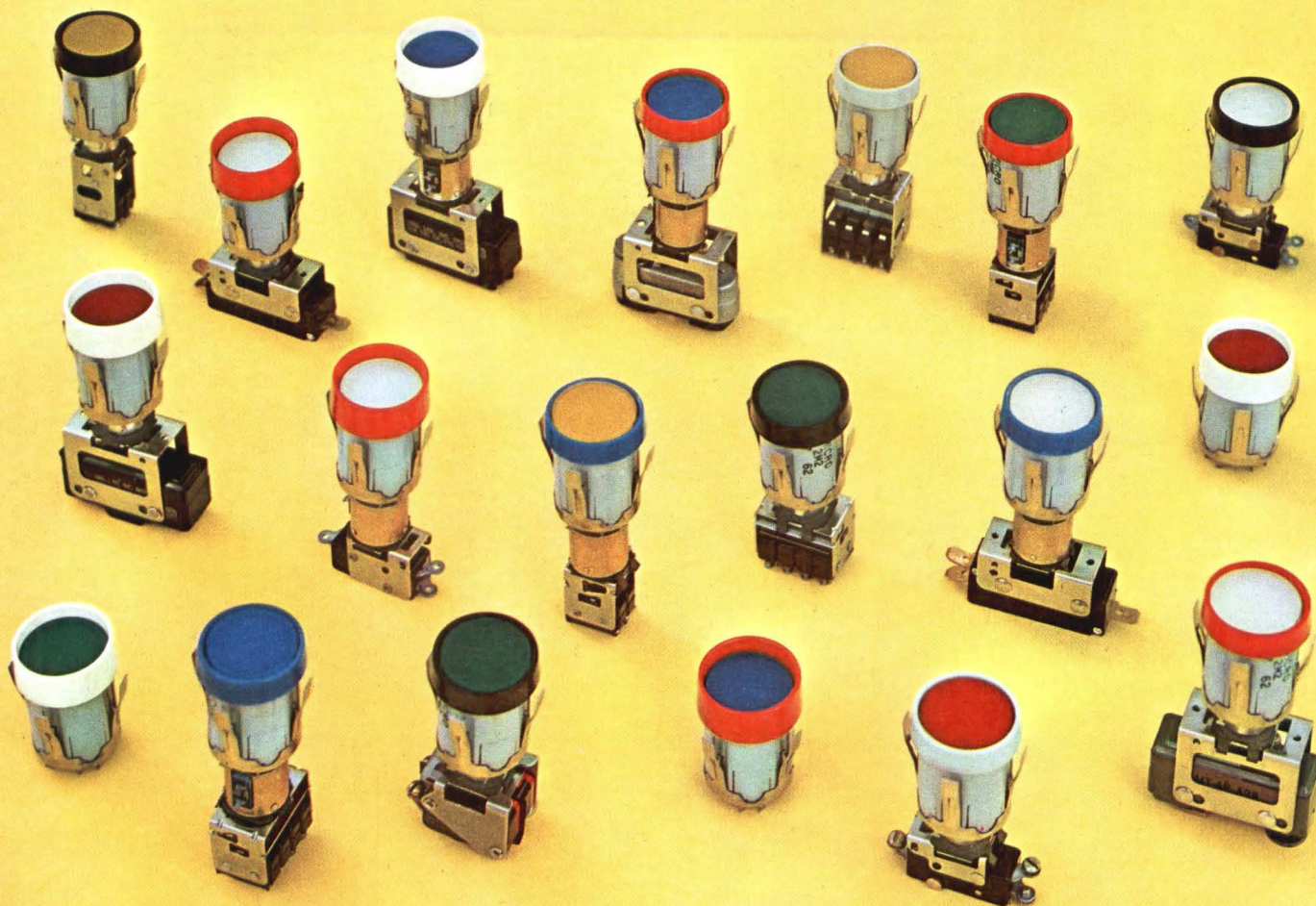
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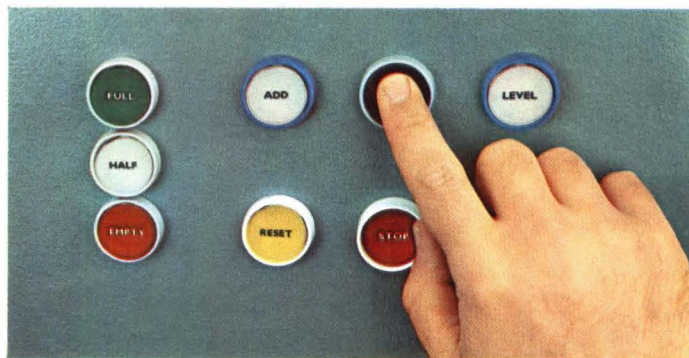


## New! Round Lighted Pushbutton Assemblies with four lamps under display screen

MICRO SWITCH Round "Series 2" lighted pushbutton switch assemblies add a new dimension to panel design.

- Modular construction...assemble interchangeable modules without tools.
- Choose from translucent color screens or translucent white screens with color filters over four separate lamps.
- Choice of 20 different switch units.

The new round form modules match the rectangular modules (see other side of page) in size, tactile "feel", screen colors and light output. They are available as indicators only, or as operator-indicators with switch units. Switching action can be momentary or maintained (push on, push off), and with or without magnetic detent coil. Color variations in display screens and guard rings enable panel designers to code control functions. Guard rings come in two heights. Contact a MICRO SWITCH application engineer (see Yellow Pages for Branch Office) or write for Data Sheet 199.



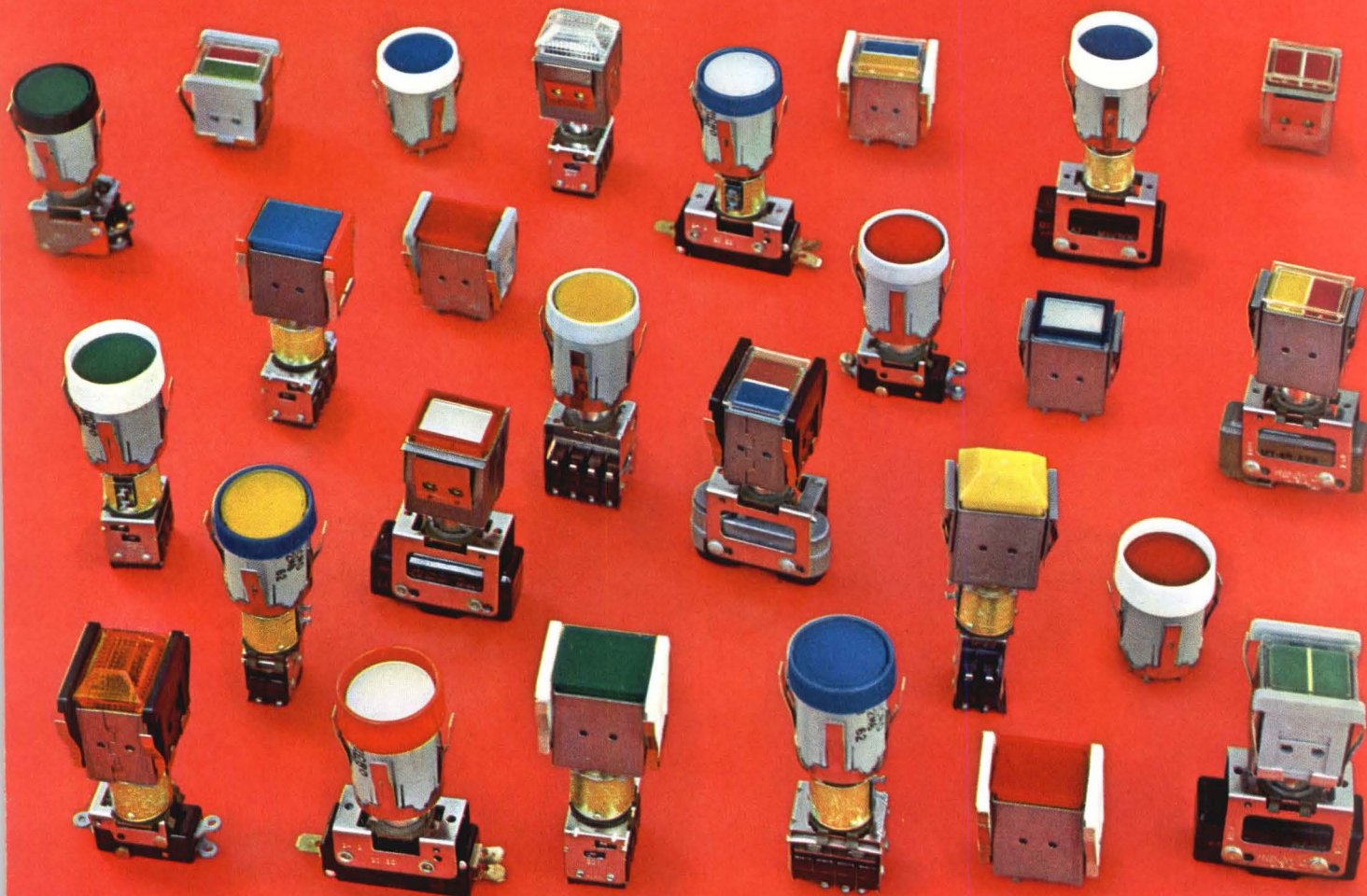
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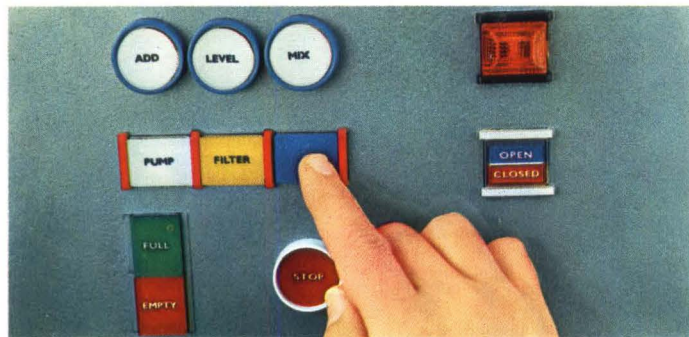
The new round shape display, together with the popular rectangular shape, gives the human factors engineer unlimited panel design possibilities for visual separation of multiple functions—both control and indication.

Under each display screen are four lamps, each lamp with separate termination. Up to four colors can be projected through each screen.

Choose from 20 different switch units—including hermetically sealed and subminiature assemblies. Circuitry and electrical ratings match your requirements! Each switch has the precision and reliability for which MICRO SWITCH is known.

For engineering assistance, call a MICRO SWITCH Branch Office. (See Yellow Pages.) Write for Catalog 67.

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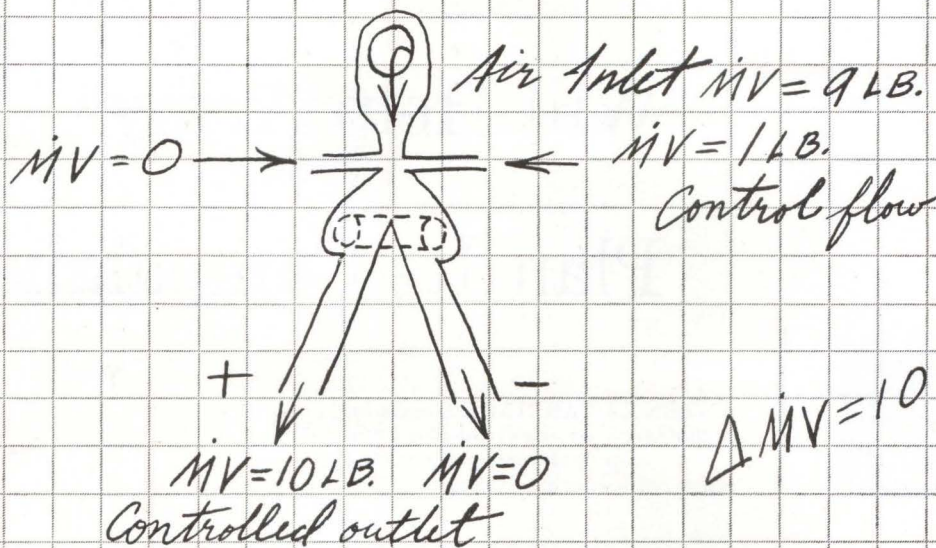
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Of interest to engineers and scientists



## PNEUMATIC CONTROL RESEARCH

...one of the more than 500 R&D programs under way at Douglas

This Douglas sponsored program seeks to provide the aerospace industry with an all pneumatic control system which has no moving parts.

Under investigation are pneumatic amplifiers, flip-flops, proportional flow devices and logic elements—the building blocks for digital computers. Experiments are being conducted in the Douglas Aerophysics Laboratory on advanced techniques in vortex control and the effects of scaling and Reynolds Number.

Important progress has been registered. Success in this field will provide simple, light weight, low cost control systems that will operate under extremes of temperature and radiation.

**Of career interest to engineers and scientists**  
Douglas has entered into a period of greatly expanded activities in programs (like the above)

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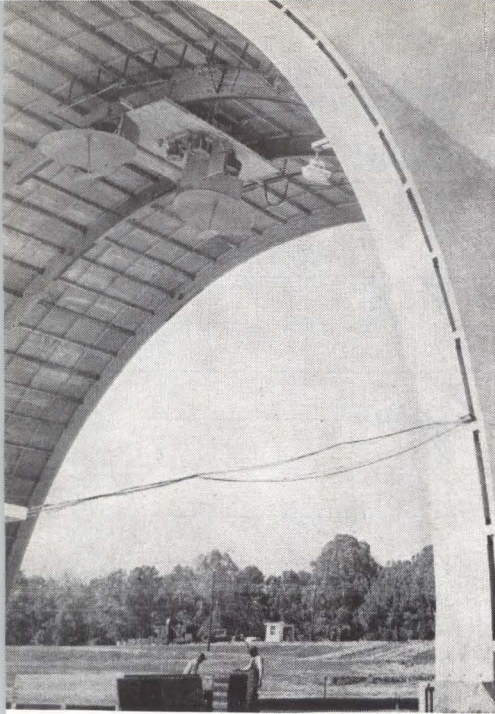
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# Airborne Soil Analyzers Will Help Army Plan Its Campaigns

ANTENNA CARRIAGE travels in a 60-degree arc inside 50-foot arch to determine best angle for measuring terrain characteristics

*Four-band radar now gathers soil signatures to aid system design*

By MARVIN REID  
McGraw-Hill World News

VICKSBURG, MISS. — During a military campaign, a field commander may turn to an aide and ask: "What's the trafficability of the terrain in the region 10 miles

beyond our right flank?"

What he means is: Is that ground mushy or hard? Can the enemy send tanks in? Will my antitank weapons get bogged down? What's the best road for my mobile missile launchers?

A new kind of radar laboratory, one that will guide the design of an airborne system to answer those questions quickly, went into operation a few weeks ago at the U.S. Army Engineer Waterways Experiment Station here.

The bistatic pulsed radar facility

is part of an overall study of terrain analysis. The station's Army Mobility Research Center (AMRC) is also studying infrared and other sensors.

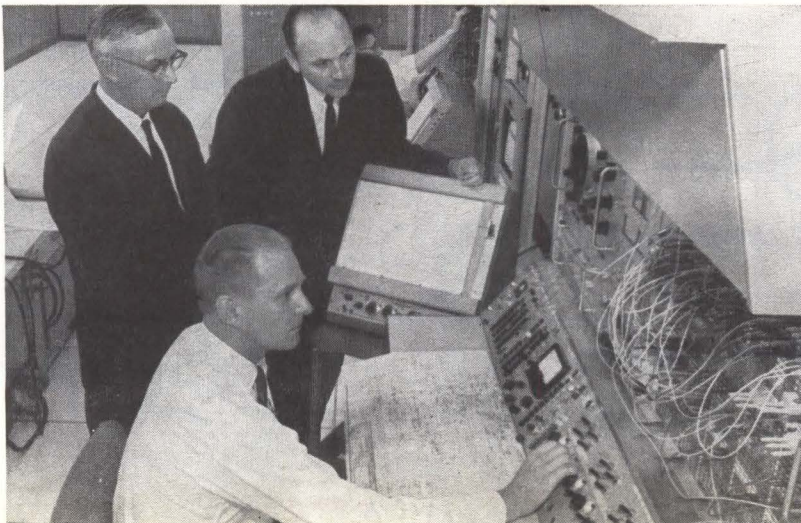
E. B. Lipscomb, chief of AMRC's Terrain Analyzer Section, visualizes eventually a multisensor system that can be put in an aircraft.

Such a system, Lipscomb says, could perceive, register and integrate data on the makeup of terrain, to give that military field commander the regional trafficability data he needs in a hurry.

---

## Digital and Analog Computers Combined

HYBRID COMPUTER CENTER, for analog-digital simulation and control of industrial processes, has been placed in operation by Minneapolis-Honeywell. Two EAI 231R analog units and a Honeywell 290 digital computer are combined, with special sections for high-speed linkage between the units. The new center will analyze and design process control systems, evaluate operating economics of plants, and simulate complete control programs



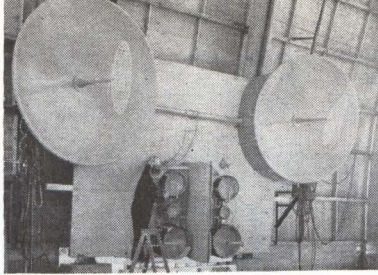
DUAL PROGRAM—Lipscomb says the project has two phases:

Primary goal of the first phase is to "fingerprint" terrain properties such as soil type, moisture content, density and other trafficability factors by examining "their electromagnetic characteristics in the ultraviolet-through-radar region of the spectrum."

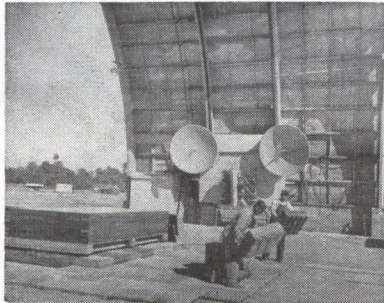
This phase is being conducted in the lab under controlled conditions with prepared soil samples of known characteristics. Here the effect of varying one particular parameter, such as grain size or moisture content, on the electromagnetic reflectance and emissivity properties of various materials can be determined.

The second phase will be determining the properties of materials under field conditions. Labora-





TRANSMITTING and receiving antennas of the four-band radar system are separated for bistatic studies



SPECIMENS covered with micro-wave absorbers provide a zero reference. Here, workmen remove absorbers to bare specimen for reflectivity tests

tory procedures and findings will be extrapolated for field use.

AMRC began infrared sensors studies in October, 1960. Start of the radar tests followed a feasibility study by the Science Services division of Texas Instruments.

In line with phase one, the facility measures and analyzes the effects on radar of soil samples. A catalogue of terrain signatures will be built up for matching with future airborne data.

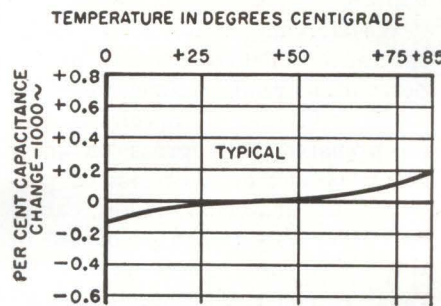
**RADAR SYSTEM** — The radar, called Westar (for Waterways Experiment Station Terrain Analyzer Radar), represents two major advances—reducing a complete P-band radar into a laboratory system, and making actual lab measurements with a C-band system.

TI designed and built the system to cover the K, X, C and P bands. The four-band combination was chosen because of Westar's needs.

Lipscomb's group wanted a system that would analyze soil conditions to a depth of at least 18 inches. TI's feasibility study showed that P-band gave deep penetration in wet soils, while the other three bands are useful for analyzing soils of low moisture content. Lipscomb

(Advertisement)

## New Film Dielectric Displays Unusual Stability



A new duplex plastic film dielectric developed and patented by the Sprague Electric Co. displays practically a zero temperature coefficient of capacitance over operating ranges up to +85 C. The retrace on return to room temperature is within  $\pm 0.10\%$ .

This new dielectric is currently being used in Sprague Electric's ISOFARAD Capacitors which are finding wide application in critical circuits of color TV receivers. The insulation resistance and dielectric absorption characteristics of these capacitors approach those of polystyrene film capacitors. ISOFARAD capacitors also are said to be superior to silvered mica capacitors in insulation resistance. Their tubular shape makes them more adaptable than silvered mica units for machine insertion on printed wiring boards. For practical purposes, their capacitance stability is equivalent to the more expensive silvered mica units.

Capacitor sections are of extended-foil design and are housed in pre-molded phenolic shells with plastic-resin end seals for protection against moisture and mechanical damage. Standard ISOFARAD Capacitors are rated at 500-volts d-c and are available with capacitance tolerances as close as  $\pm 5\%$ .

For complete technical data on ISOFARAD Capacitors (Type 145P), write for Engineering Bulletin 2073A to Technical Literature Section, Sprague Electric Company, 35 Marshall Street, North Adams, Massachusetts.

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# new!

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In order to suit various installation and packaging techniques, Type 45Z Pulse Transformers are available with standard length wire leads. Weldable or solderable leads can be furnished. Short pin-type leads for use with subminiature sockets are also available.

For complete technical information on Type 45Z Pulse Transformers, write for Engineering Data Sheet 40210 to Technical Literature Service, Sprague Electric Company, 35 Marshall Street, North Adams, Massachusetts.



48-441

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21



reports that early radar results bear out the feasibility report.

While no existing radar was suitable for both laboratory and airborne operations, TI found its existing radars and components in the  $K_u$ , X, C and P bands could be modified from AN/TPS-21 or AN/TPS-33 radar components.

**WOODEN ARCH** — The 50-foot arch is laminated wood. Microwave absorbants, a high level of signal-range gating and 100-db antenna isolation, help insure that radar recordings are purely from the terrain specimens, says Allen Feder, of TI's Science Services division.

Radar echo amplitudes could overlap, just as many object images on a black and white aerial photo could have the identical grey-scale level, Feder adds. Therefore, the best way to get valuable radar signatures appears to be as functions of signal amplitudes  $\gamma$  for the spread of aspect angles  $\theta$  from normal to grazing incidence.

To provide these  $\gamma$ - $\theta$  curves, the antennas are mounted on a carriage that travels from 30 to 90 degrees along the arc of 50-foot radius, centered on the upper surface center of the terrain material specimen.

Arc radius was set at 50 feet to insure that measurement would be made with far-field energy.

Terrain material is contained in a 12 × 6 × 2-foot cart.

The 6 × 12-foot specimen surface dimension encloses all of the radar beam cross section at all aspect angles involved for  $K_u$ , X, and C bands. The 2-foot specimen depth represents maximum C-band penetration in saturated soils.

Normal test procedure is to fill the cart with various types of soils

from different regions. Soil parameters are measured for various natural conditions. Before each test run, the specimen is covered with a microwave absorbant material to give a zero reference. Changes from the zero reference to exposed specimen run show the soil parameters.

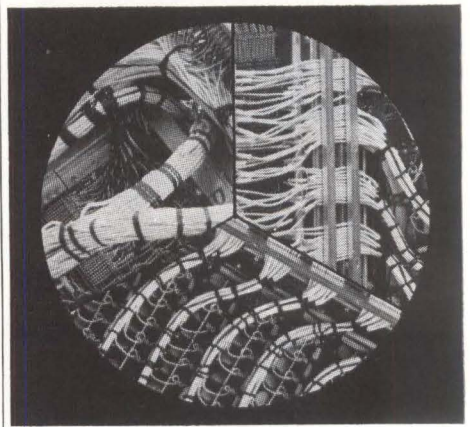
Westar can tell terrain material specimen moisture content to 0.1 percent and read specimen temperatures to 0.1 deg C. Specimens can be prepared with grass or snow cover, or can even consist of possible lunar materials. Mines, cables and other objects can be buried in the specimens to determine their radar response. Engineering structure models can be employed for simulation studies.

**AIRBORNE SYSTEM** — Another objective in designing the laboratory system was to select standard radar equipment that could be modified for later airborne use.

Westar's people expect to know by next July whether a modified version of the Vicksburg radar is feasible for airborne use. If the decision is made to go airborne, it would take another six months to a year to fabricate the system.

AMRC is thinking at this stage of an aircraft equipped with radar, infrared, visible photography, and other electromagnetic sensors.

AMRC is primarily interested in military needs for a system that reliably and rapidly analyzes the top 18 inches of a region's terrain. Other potential applications are highway right-of-way surveying, natural resource surveys and perhaps systems for mapping soils on the moon from a lunar orbiting vehicle.



The increased emphasis on reliability is in part the growth of our Electronic/Aerospace industries but made vital with the manned space flight era. Though the function of an electrical component is primarily electrical or electronic, final reliability lies in the mechanical performance. In wire and cable products, for example, failures due to cut-through, abrasion, and cold-flow have been numerous; these experiences should be a basic factor in design considerations.

Through techniques in applied radiation chemistry, research emphasis at Raychem has been on mechanical integrity. The resistance to abrasion as expressed by MIL-T-5438 and comparative deformation under load characteristics per ASTM D 621 are convincing tests which confirm mechanical toughness not existent in other high temperature insulation systems.

Though spacecraft reliability represents the extreme in mechanical/electrical design needs, this same reliability is a vital part of complex ground-based systems as well.

## TELEFEEL? WAIT ABOUT 10 YEARS

NEW YORK—Prototype equipment for the "feelies" of "Brave New World" fame is at least 10 years away.

It will take that long to solve the sensing and display problems associated with feeling at remote distances, indicated T. B. Sheridan, of MIT, at the Human Factors Society meeting.

A true display would reproduce in man the tactile sensation being experienced by remote equipment. Some preliminary experiments with air jets and servo-drive rods have been made, but results are not definitive.

Another technique, translating pressure or displacement into visual readout on an oscilloscope, appears to solve some handling problems and will probably be used in initial equipment



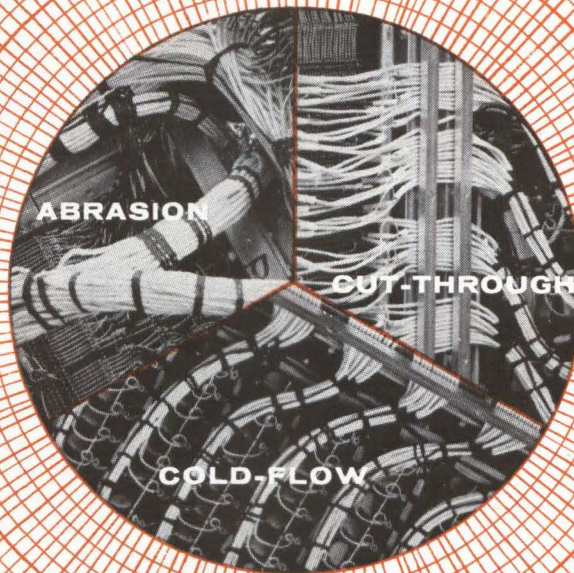
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**MECHANICAL TOUGHNESS...THE KEY TO RELIABILITY**

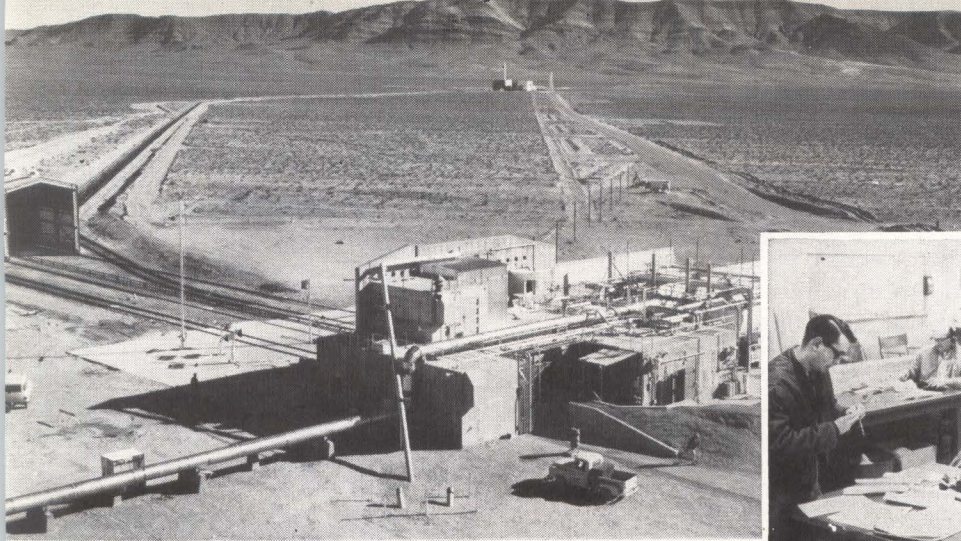
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TEST CELL where Nuclear Rocket Development Station has been trying out Kiwi reactors. Assembly building is 1½ miles away

CONTROL POINT for remote operation of Kiwi reactors during tests



## Project Rover's Long-Range Target:

*But funds squeeze may slow development of nuclear rockets*

By HAROLD C. HOOD  
Pacific Coast Editor

**MERCURY, NEV.** — Five days after the President's visit to the site, newsmen got their first glimpse of the Nuclear Rocket Development Station (NRDS) here. They got some eye-opening figures on Project Rover, the nation's program to develop nuclear propulsion systems

for lunar and planetary flights.

- A nuclear-propelled spacecraft for a manned Martian landing, for example, would weigh one-tenth as much as its chemically propelled counterpart.

- To create a thrust of 50,000 pounds the light-weight flying reactor must produce a million btu per second, or enough energy to boil away a ton of water every two seconds.

- Electronic equipment for one flight vehicle will cost easily \$1 million.

In simplified terms, a nuclear rocket engine consists of a reactor,

a nozzle, and a turbopump. Liquid hydrogen is pumped from the vehicle's tank through the reactor core where it is heated to over 5,000 F in a fraction of a second. Hydrogen gas is then accelerated through the jet nozzle at a specific impulse (thrust per pound of propellant) two or three times that attainable from a chemical combustion engine.

**THREE PROJECTS**—Rover consists primarily of three projects—Kiwi (a flightless bird), Nerva (Nuclear Engine for Rocket Vehicle Application), and Rift (Reactor-in-Flight Test).

Kiwi provides the basic reactor technology for the entire program. Six Kiwi ground test reactors have been tested, the first in July, 1959, and the most recent last month. (The tests have been successful, by and large. For example, in a test November 30, the cracking of a thermal insulator was the only hitch, according to a NASA spokesman in Washington. Remaining problems are chiefly mechanical and materials design.)

Other tests, including a simulated water entry and a "run-till-destruction" are scheduled over the next two years. Los Alamos Scientific Laboratory runs Kiwi.

### ROVER SLOWDOWN IS EXPECTED

The word from Washington last week coincided with the word from Mercury, Nev. Rover will probably get \$200 million in the fiscal 1964, about half of the project's request.

Key factor in the expectation was President Kennedy's statement on his return from Los Alamos:

"The nuclear rocket, even under the most favorable circumstances, would not play a role in any first lunar landing. This will not come into play until 1970 or '71. It would be useful for further trips to the moon or trips to Mars. But we have a good many areas competing for our available space dollars, and we have to try to channel it into those programs which will bring us a result first, on our moon landing, and then to consider Mars."

Rover has to prove itself by next July before a decision will be made on extra money, Kennedy said





KIWI REACTOR is prepared for testing. This one was tested November 30

## Man on Mars

Project Nerva is now in early stages of component development, and will yield a rocket engine suitable for flight in outer space.

The development program for the Nerva engine differs from those for other rocket engines primarily in that all disassembly, maintenance and reassembly must be done remotely and behind heavily shielded walls. (First test-stand firing is scheduled for 1964. As many as 30 or 40 Kiwi-type reactors may be used in tests leading up to a flight model.)

Prime contractor for Nerva is Aerojet-General, with Westinghouse Electric supplying the reactor, AMF responsible for engine assembly and remote disassembly, and Bendix developing control system actuation devices. Edgerton, Germeshausen & Grier is performing instrumentation and control.

**FLIGHT TESTS**—Lockheed Missiles and Space Co., prime contractor for Rift, is preparing Nerva's flight test vehicle. This will demonstrate nuclear propulsion in flight as a third stage of the C-5 Saturn.

In all, 10 Rift stages will be built. Five will be shipped to NRDS for static tests and four will go directly to Cape Canaveral for

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deep-water lob shots.

First flight, expected in 1967, will carry an inert Nerva engine. The next three trajectories will include nuclear operation of the Rift stage, coast, and nuclear restart. A regular Saturn booster stage will be used, with a dummy second stage. Above the Rift stage will be a special instrument unit.

In late Rift-Nerva phases, NASA will introduce a second family of reactors of enhanced power design, called Phoebus. Phoebus will be another Kiwi-type program of ground testing.

If the budget permits, some design considerations are coming up next year. Whether Phoebus gets under way, and, in fact, whether Nerva-Rift gets a full start, depends on considerations now under way in Bureau of the Budget.

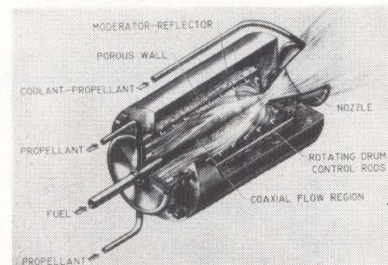
**FUNDS TRIMMED**—The Space Nuclear Propulsion Office (SNPO) hedges when asked how much it will spend on Kiwi, Nerva and Rift, but one spokesman referred to Rover as "a billion-dollar program." To date \$265 million has been spent. Some \$380 million has been requested for next fiscal year, but informed sources feel this will be trimmed to \$200 million. This will keep the program going at its present level, they say.

SNPO manages the three-pronged program. The office was established in August, 1961, by AEC-NASA agreement, and reports to both agencies.

**ELECTRONICS PROBLEMS** — In explaining some of the problems faced by his electronics designers, a Lockheed official underlines the fact that Rift must be able to operate satisfactorily in the radiation field set up by Nerva.

"Instrumentation used for conventional liquid hydrogen rockets in the past has been found to be completely unsuitable," he points out.

"Capacitance probes in liquid hydrogen tanks, for example, may be off by a factor of three in the presence of ionization produced by radiation. Another problem area is thermocouples. Since materials having significant density tend to generate heat in the presence of radiation, these may not be accurately indicating the temperature of their



CAVITY REACTOR concept being researched by NASA. Heat from core of fissioning plutonium gas would energize hydrogen propellant

surroundings. One answer is to keep the mass of components to a minimum.

"Ironically, the first time we've had no weight and size limits," he said, "we still have to miniaturize."

Signal noise introduced by radiation is a new problem for Lockheed's circuit designers. Avoiding high impedance loads has helped in some cases and regenerative feedback loops have been employed in others. The use of magnetic amplifiers, high-temperature amplifiers, and filamentless ceramic tubes is being investigated as a means of combatting the high-temperature environments anticipated. Welded module techniques are being used for most of Rift's electronics.

**Phased-Array Problem  
Supplying 2,000 Tubes**

BEDFORD, MASS.—Logistics presents one of the toughest problems in phased-array radar systems, said J. S. Cook, of Bell Telephone Labs, at an IRE meeting here. A phased-array system might have 2,000 transmitter power amplifier tubes.

Within 10 years, when phased arrays become competitive with other systems, high-volume production of tubes will be needed and their price will have to decrease by a factor of 100—down to \$50.

Commented one engineer: "Sounds like every phased-array system will have to have a tube factory built along with it."

There is great need for components designed specifically for phased array use, said N. F. Pribble, of Bendix Radio. Attempts to adapt other components result in prohibitive cost. Pribble is design group leader of the phased-array radar for Spadats (p 7, Oct. 19).



## MEETINGS AHEAD

MILLIMETER AND SUBMILLIMETER CONFERENCE, IRE; Orlando Section; Cherry Plaza Hotel, Orlando, Florida, Jan. 7-10.

RELIABILITY & QUALITY CONTROL SYMPOSIUM, IRE-PGRQC, AIEE, ASQC, EIA; Sheraton Palace Hotel, San Francisco, Calif., Jan. 21-24.

INSTITUTE OF ELECTRICAL & ELECTRONICS ENGINEERS WINTER GENERAL MEETING & EXPOSITION, IEEE; Statler and New Yorker Hotels, New York City, Jan. 27-Feb. 1.

MILITARY ELECTRONICS WINTER CONVENTION, IRE-PGMIL; Ambassador Hotel, Los Angeles, Calif., Jan. 30-Feb. 1.

QUANTUM ELECTRONICS INTERNATIONAL SYMPOSIUM, IRE, SFER, ONR, Unesco Building and Parc de Exposition, Paris, France, Feb. 11-15.

INFORMATION STORAGE AND RETRIEVAL SYMPOSIUM, American University; International Inn, Washington, D. C., Feb. 11-15.

ELECTRICAL & ELECTRONIC EQUIPMENT EXHIBIT, ERA, ERC; Denver Hilton Hotel, Denver, Colo., Feb. 18-19.

SOLID STATE CIRCUITS INTERNATIONAL CONFERENCE, IRE-PGCT, AIEE, University of Pennsylvania; Sheraton Hotel and U. of P., Philadelphia, Pa., Feb. 20-22.

PACIFIC COMPUTER CONFERENCE, AIEE; California Institute of Technology, Pasadena, Calif., March 15-16.

BIONICS SYMPOSIUM, United States Air Force; Biltmore Hotel, Dayton, Ohio, Mar. 18-21.

IEEE INTERNATIONAL CONVENTION, Institute of Electrical and Electronics Engineers; Coliseum and Waldorf-Astoria Hotel, New York, N. Y., March 25-28.

ENGINEERING ASPECTS OF MAGNETO-HYDRODYNAMICS SYMPOSIUM, IRE-PGNS, AIEE, IAS, University of California; UCLA, Beverly, Calif., April 10-11.

OHIO VALLEY INSTRUMENT-AUTOMATION SYMPOSIUM, ISA, et al; Cincinnati Gardens, Cincinnati, Ohio, April 16-17.

INTERNATIONAL NON-LINEAR MAGNETICS CONFERENCE, IRE-PGEC, PGIE, AIEE; Shoreham Hotel, Washington, D. C., April 17-19.

### ADVANCE REPORTS

INTERNATIONAL MEASUREMENTS CONFERENCE, ISA, et al; Stockholm, Sweden, June 1964. No specified deadline has been set for submitting papers, but in view of conference's international character, they should be submitted as soon as possible to: R. D. Douglas, Hydraulic Laboratory, Newport News Shipbuilding and Dry Dock Company, Newport News, Virginia. Subject titles include: general problems of electronics for measuring purposes; border questions on measurement and automation; instruments and methods for measuring electrical and magnetic quantities; radio-engineering measurement instruments and methods; radioactive-radiation measurement.

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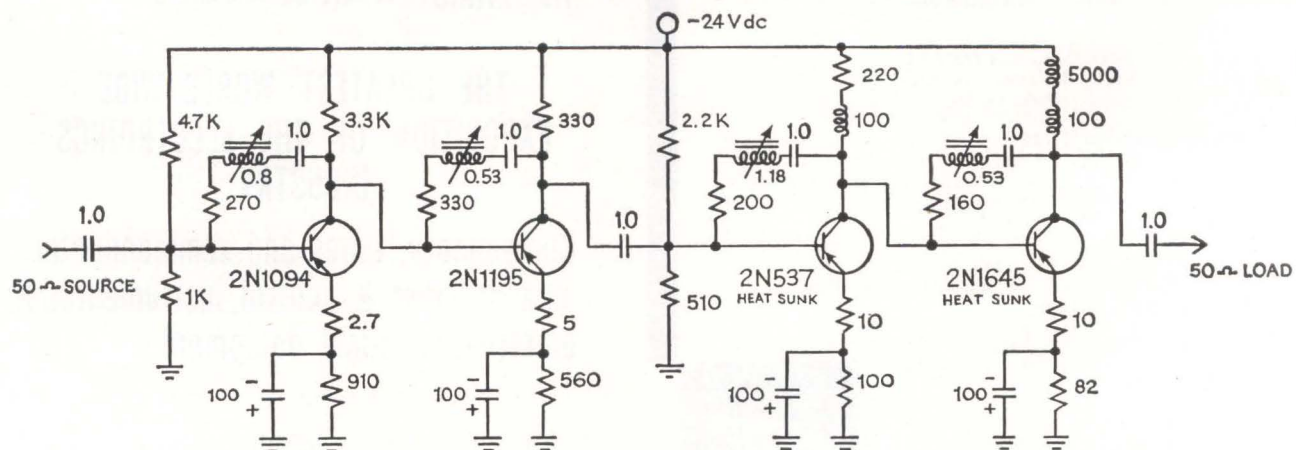


USA2N537



2N1645

## 2 kc—100 Mc Broad Band Linear Amplifier



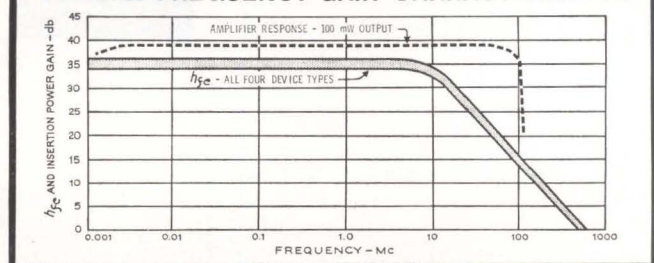
AMPLIFIER CHARACTERISTICS  
INSERTION POWER GAIN - 40db  
NOISE FIGURE - < 10db FROM 20-100 MC

ALL RESISTANCES IN OHMS  
ALL CAPACITANCES IN  $\mu\text{f}$   
ALL INDUCTANCES IN  $\mu\text{h}$

### DEVICE CHARACTERISTICS

|                             | USA<br>2N1094 | JAN<br>2N1195 | USA<br>2N537 | 2N1645 |
|-----------------------------|---------------|---------------|--------------|--------|
| $f_t$ (typical) Mc          | 650           | 550           | 600          | 600    |
| $RE_{ie}$ (typical) ohms    | 100           | 60            | 45           | 25     |
| $C_{cb}$ (dir) (typical) pf | 1.5           | 2.3           | 2.2          | 10     |
| $h_{fe}$ (typical)          | 50            | 45            | 25           | 65     |
| $BV_{CBO}$ min vdc          | -30           | -30           | -30          | -35    |

### TYPICAL FREQUENCY-GAIN CHARACTERISTICS



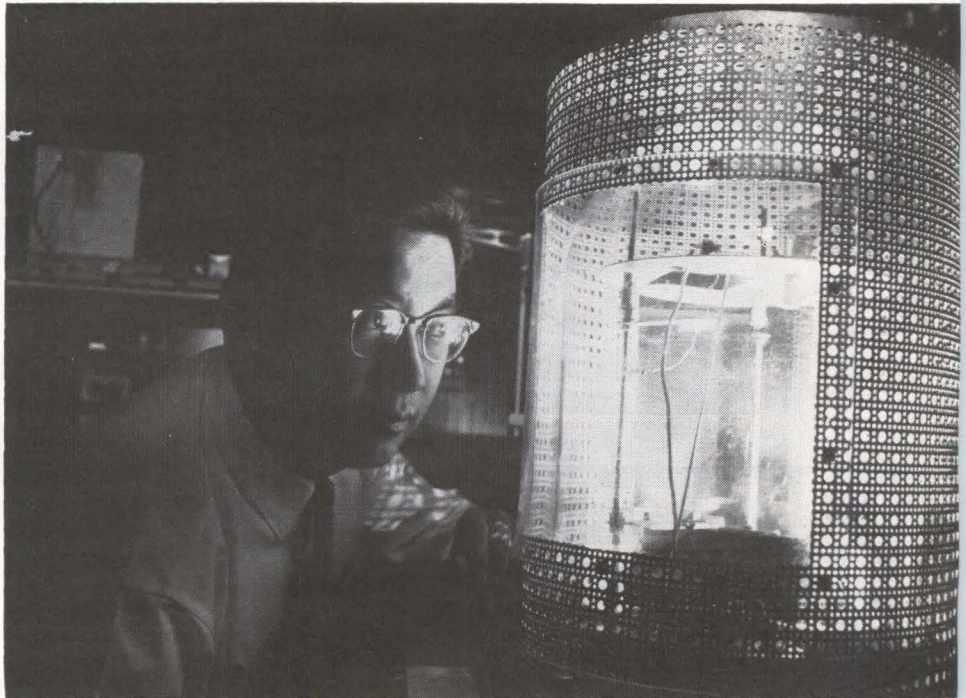
The four germanium transistors described above may be purchased in quantity from Western Electric's Laureldale Plant. For further technical information, price, and delivery, address your request to Contracting Department, Room 102, Western Electric Company, Incorporated, Laureldale, Pa. Telephone—Area Code 215—929-5811.

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**POLYMERIZATION** of silicon oil, used as an insulator for grid of hot-electron triode, is observed by author Tantraporn



## HOW GOOD ARE THIN-FILM TRIODES?

*Impact of active thin-film devices can be gaged from current progress. Comparisons are made of performance capabilities and of problems in fabrication and use*

By **W. TANTRAPORN**

Electronics Laboratory, General Electric Company, Syracuse, New York

**THIN-FILM TRIODES** may ultimately provide a variety of performance characteristics for use in microminiature electronic circuits. For example, the space-charge-limited type should provide the highest operating frequencies and be the least noisy of these devices. Comparable performance can be expected from field-effect triodes in thin-film form, and they should be

the easiest to fabricate and the most versatile. Although the hot-electron triode will be limited to operation at lower frequencies and will probably be the most temperature-dependent, it is expected to be better able to withstand radiation.

Much theoretical and experimental work with new triodes has been reported during the past two years.<sup>1-5</sup> Many of these triodes con-

tain semiconductor single crystals and are not amenable to present thin-film techniques. If those triodes that can be fabricated in thin-film form are logically classified, their expected performance capabilities can be compared.

Basically, a thin-film triode consists of three electrode terminals that are separated from each other by semi-insulating materials. Insulation requirements are dependent on the operating mechanisms. The mechanism by which the control electrode influences current between the other two electrodes can be used to classify thin-film triodes. On this basis, thin-film triodes can be placed in any of three classes: the space-charge-limited or analog triode and the hot-electron triode and field-effect triodes.

**SCL TRIODE**—A field must be established in the space-charge-lim-



ited triode between two electrodes in such a way that space-charge neutrality does not hold. This condition is possible in a wide band-gap insulator with the emitter electrode forming a low contact barrier

against the insulator. Such a space charge in the solid is thus similar to the space charge in the vacuum tube except for the different nature of the mobilities.

If a metallic line grid is then in-

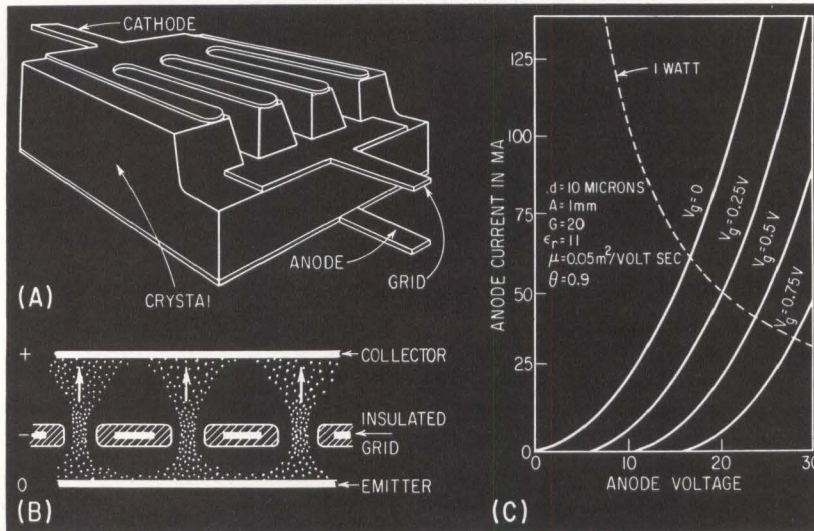
serted between the two electrodes to form a blocking contact with the insulator, the grid will function similarly to the grid in a vacuum tube. Since the spacing of the electrodes needed to achieve the space-charge condition is in the micron range, thin-film techniques can be used to fabricate the device. Grid fabrication is difficult, however, since the grid must be in the form of thin lines spaced about 1 micron apart within the insulator film and forming blocking contacts against the insulator.

A single-crystal type space-charge-limited triode<sup>2</sup> is shown in Fig. 1A. A space-charge-limited triode with single edge grid was demonstrated as early as 1959.<sup>1</sup> A present-day thin-film adaptation of the triode is shown in Fig. 1B with insulating layers replacing the blocking contacts. A blocking contact is difficult to achieve between a thin line and the semi-insulator, which is CdS.

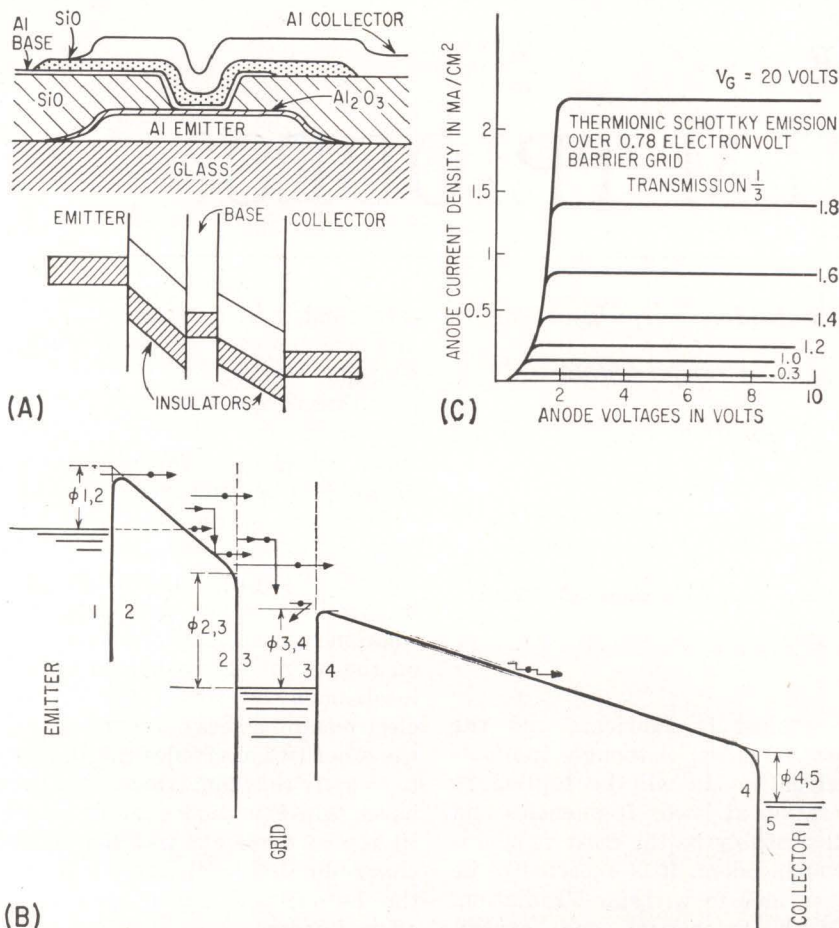
Theoretically, the triode characteristic is expected to be similar to that shown in Fig. 1C. However, the parameters used are optimistic even for the single crystal CdS. The more critical parameters are the mobility of 500 cm<sup>2</sup> per volt-second and the trap density of less than 10<sup>15</sup>/cm<sup>3</sup>, which cannot be obtained in the polycrystalline state. However, the space-charge condition can be established at small mobility and large trap density by increasing the electric field. Thus it should also be obtainable by decreasing the distance between the electrodes. Space-charge-limited current has been observed in some carefully prepared CdS thin films a few microns thick.

**SCL PERFORMANCE**—Although the space-charge effect cannot be easily calculated, it is regarded as beneficial in reducing noise within the device compared with other devices operating at the same temperature.<sup>9</sup> Since it is a majority-carrier device, temperature dependence should be small.<sup>10</sup>

Voltage gain in a thin-film SCL triode will probably be about 10. Current gain should be large because of the small grid current. Power gain of about 10<sup>6</sup> is not unlikely, although actual power level may be small if trap density of the material (CdS) is large. For high



SINGLE-CRYSTAL type space-charge-limited triode (A) has been adapted to thin-film form (B). Triode characteristics (C) have been predicted theoretically—Fig. 1



HOT-ELECTRON triode (A) is shown as originally conceived. Energy diagram (B) is for hot-electron triode for which theoretical characteristics (C) are expected—Fig. 2



density of shallow traps, however, the SCL triode is expected to have better frequency characteristics. Triode performance is limited by trapping relaxation time at lower frequencies but becomes better at higher frequencies as the signal modulates only the untrapped charges. Finally, frequency is limited by transition time. Gain-bandwidth product is thus given by the reciprocal of transition time and is about  $10^9$  cps if anode voltage is 100 volts, spacing is 5 microns and mobility is  $3 \text{ cm}^2$  per volt-second.

**HOT ELECTRON TRIODE**—Considerable interest was first aroused by the hot-electron triode, followed by confusion and finally disappointment. The device as originally proposed<sup>3</sup> is shown in Fig. 2A. It was first assumed that electrons left the emitter and entered the grid by a quantum tunneling mechanism.

Another hot-electron triode was reported<sup>4</sup> that was assumed to work on the same emission mechanism but with the collector portion replaced by a germanium single crystal and an ohmic electrode. It was later pointed out<sup>5</sup> that current emission was more likely the result of the Schottky thermionic process than of quantum tunneling. Finally it was proved that operation of the triode must depend on another mechanism that is facilitated by the presence of pinholes. This mechanism is now being investigated by the originators of the triode, which is now called the metal interface amplifier. This triode, which is not a hot-electron triode but a field-effect triode, does not fit into the classifications established in this article. It uses a semiconductor single crystal and is not a thin-film device as it is here defined.

An energy diagram of the hot-electron triode is shown in Fig. 2B, which also shows relevant processes. Best operation of this device is achieved under the following conditions: For high emission and to reduce temperature dependence,  $\phi_{1,3}$  should be approximately equal to zero. For hot electron transfer through the grid layer,  $\phi_{2,3}$  should be about 1 electron volt and should be greater than  $\phi_{3,4}$ . Thickness of layer 3 should be about 100 angstroms (continuous film). Finally,  $\phi_{3,4}$  should be greater than  $\phi_{4,5}$ ,

which should be approximately zero for best collector efficiency.

Experimental evidence was recently reported<sup>7</sup> of hot-electron transfer across a thin metal film. Unfortunately, a semiconductor (germanium) collector was used in these experiments, although the

same function could be accomplished in principle with a thin insulator layer with a strong bias. The state of the art of the hot-electron triode is thus represented by hot-electron transfer into the semiconductor crystal, and the problem in the future will be to fabri-

STATE OF THE ART IN THIN-FILM TRIODES—TABLE I

| Triodes              | Field Effect                                                                 | Space-Charge Limited                                                                                       | Hot Electron                                                                                                                                                                             |
|----------------------|------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| Structures           | Semiconductor film of micron thickness. Electrodes on semiconductor surfaces | Semiconductor film of micron thickness between anode and cathode. Fine-line grid embedded in space between | Consecutive layers of emitter metal, emitter insulator, grid metal, collector insulator, collector metal. First two, last two or both may be replaced by semiconductor and ohmic contact |
| Feasibility          | Proven experimentally                                                        | Predicted theoretically with preliminary experimental support                                              | Predicted theoretically with experimental proofs for some triode parts                                                                                                                   |
| Achievement Dates    | 1961                                                                         | 1962-63                                                                                                    | Late 1963                                                                                                                                                                                |
| Anticipated Problems | Optimizing dimensions, developmental improvements                            | Isolated fine-line grid with spacings about 1 micron                                                       | Electron transfer across grid layer difficult in complete structure                                                                                                                      |

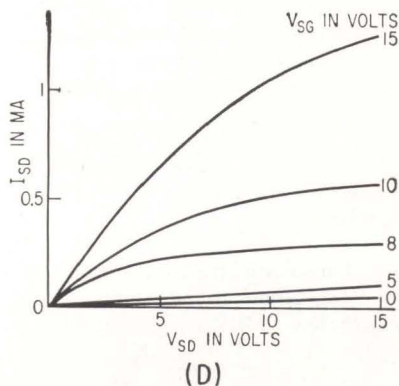
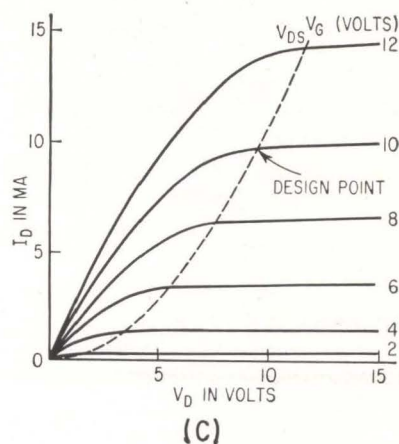
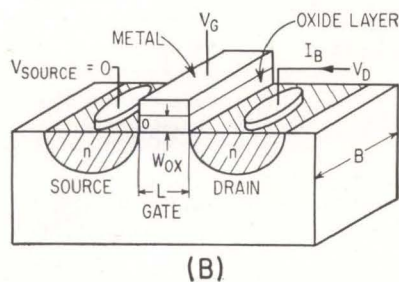
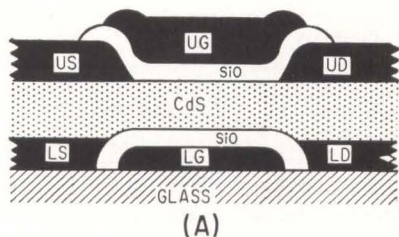
EXPECTED THIN-FILM TRIODE PERFORMANCE—TABLE II

| Triode            | Field Effect                                                                   | Space-Charge Limited                                                           | Hot Electron                                                                                  |
|-------------------|--------------------------------------------------------------------------------|--------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------|
| Mode of Operation | Voltage controlled, best with positive grid bias. Input resistance $10^6$ ohms | Voltage controlled, best with negative grid bias. Input resistance $10^6$ ohms | Current controlled, positive grid bias required. Input resistance 1-100 ohms                  |
| Frequency Limit   | About $10^8$ cps (limited by transition time)                                  | $10^8$ - $10^9$ cps (optimized capacitance versus transition time)             | $10^6$ - $10^7$ cps (limited by input shunt capacitance)                                      |
| Main Features     | Ease of fabrication, high gain-bandwidth product, versatility (- or + gate)    | High gain-bandwidth product, temperature insensitivity, low noise              | High tolerance to radiation                                                                   |
| Limitations       | Reproducibility difficult because of critically small spacings                 | Grid structure fabrication difficult                                           | Operation limited to low frequencies, temperature dependent, noisy (noise figure about 15 db) |



cate a thin-film structure that has and can maintain the barrier heights prescribed.

**CHARACTERISTICS** — Operation of hot-electron triodes having insulator films of 20 to 1,000 angstroms will necessarily be near the



FIELD-EFFECT triode has general configuration at (A). Charge redistribution process was assumed for suggested triode (B) with predicted performance (C), which is similar to results (D) at this laboratory—Fig. 3

breakdown condition and will have to be current-controlled. Current gain is less than unity because of absorption of the hot electrons by the grid layer. The power gain that is possible is therefore the result of voltage gain, which is not expected to be large. Power gain of about 100 is considered high if transfer of hot electrons is about  $10^{-1}$ . Theoretical characteristics for likely parameters are shown in Fig. 2C.

Because of the extreme nonlinearity in the current-voltage relationship of the emitter-grid section, input resistance at the operating point will probably be about 100 ohms or an order of magnitude either way and will be shunted by the input capacitance. For an alumina film 20 angstroms thick, capacitance is about  $10^{-8}$  farad per  $\text{mm}^2$ . The input section thus limits operation to an upper frequency limit of about  $10^6$  to  $10^7$  cps. Although frequency capabilities are lower in the hot-electron triode, this limitation is compensated by its greater resistance to radiation. The thin film becomes essentially a massless absorber of radiation. Tests indicated that thin films are not affected by radiation corresponding to the stronger Van Allen belt.

Temperature dependence of the hot-electron triode will be dominated by emission  $e \exp(-\phi_s/kT)$ . Noise figure is expected to be high, represented by a hot-electron equivalent temperature about 40 times room temperature. These disadvantages of the hot-electron triode contrast with the SCL triode.

**FIELD-EFFECT TRIODE** — The only thin-film triode in the three classes that is presently operational is the field-effect triode.<sup>8</sup> In this device, the control electrode affects the number of free carriers in the space between the other two electrodes. The predominant mechanism operating in this type triode is not presently clear. The effect may be on emission efficiency, the relocation of free charges from an irrelevant to the relevant region or the freeing of trapped charges in the semi-insulator thin film. The mechanism is now being studied in experiments at this laboratory with the aim of controlling or improving it.

The general configuration of the

field-effect triode is shown in Fig. 3A. The charge-redistribution process was assumed for one triode having the suggested configuration shown in Fig. 3B and the predicted performance shown in Fig. 3C. In the Weimer triode, the gate electrode was on the opposite surface from the source and drain electrode.

The results of one phase of the work at this laboratory is shown in Fig. 3D, which indicates the close similarity to the reported results of Weimer and the predicted curve of Ihantola. The results also indicate a trap-emptying mechanism.

Without a definite model, the limits of field-effect triode performance cannot be predicted. However, anticipated performance capabilities based on the reported experimental results should be comparable to those of the SCL triode.

Fabrication is relatively simple. However, producing identical samples may be difficult because of the critically small spacings (microns).

An attractive feature of the field-effect triode is its flexibility. It lends itself to various combinations of electrode positions, dimensions, electrode materials and large ranges of current and voltage, and various electrical configurations.

The state of the art in thin-film triodes is summarized in Table I. Expected performance is provided in Table II.

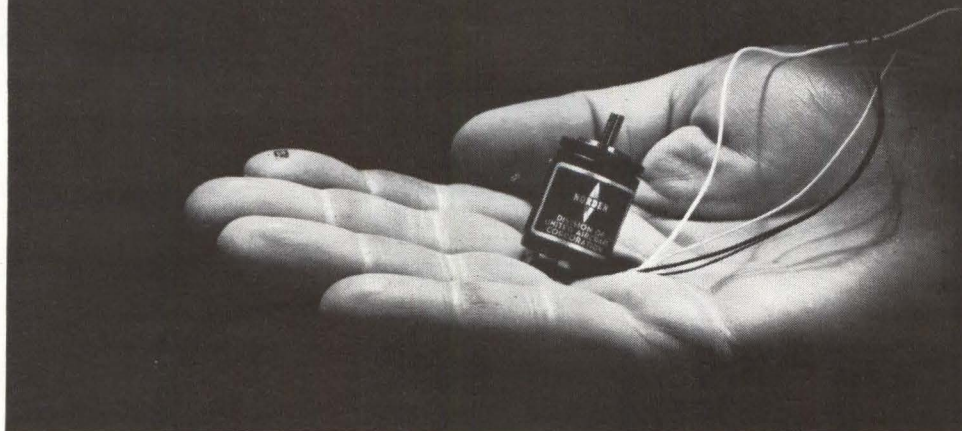
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- (10) A. M. Conning, A. A. Kayali and G. T. Wright, Space-Charge-Limited Dielectric Diodes, *J Inst EE*, 5, p 595, 1959.
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- (12) H. K. J. Ihantola, Tech Rep 1661-1, Solid State Electronics Laboratory, Stanford Univ, August 17, 1961.



# Putting a Servo Amplifier on a Small Silicon Wafer

MOLECULAR  
SERVO amplifier,  
on fingertip, packs  
enough power to  
drive a size 8  
servo motor



*Inside-out transistors are key to high-power  
output of a molecular servo amplifier*

By M. W. AARONS, Norden Division, United Aircraft Corp., Norwalk, Conn.

MOLECULAR SERVO amplifiers with enough power to drive a servomotor are diffused into a thin silicon wafer only  $\frac{3}{8}$ -inch diameter. These analog units are the result of several new molecular electronic techniques developed to simplify fabrication and to enable the output stage to deliver a sizable amount of power. An important result is the topological inversion of the transistor structure to achieve extremely low saturation resistance. The geometry of conventional transistor structures was altered by turning the transistor inside-out. It is difficult to use conventional geometry, with all contacts in the same plane and extract the power required.

The amplifier is direct-coupled, class A and contains almost four dozen components. Rated power output is 1.5 watts. All circuit connections are deposited on a passivated surface. The transistors can

sustain 75 volts and deliver up to 200 ma into size 11 and size 8 servo motors.

**CIRCUIT**—In Fig. 1A, transistors  $Q_1$  through  $Q_4$  form a differential high impedance voltage preamplifier. Transistors  $Q_5$  and  $Q_6$  are emitter follower driver stages, which are zener diode coupled to the push-pull power output stages  $Q_7$  and  $Q_8$ . Re-

## NEW APPLICATION OF MOLECULAR ELECTRONICS

To date, most molecular electronic devices have been digital. And they handle relatively low power. This unit is an analog device and can provide enough power to drive standard size servo motors. In fact, the amplifier has driven 3-watt motors

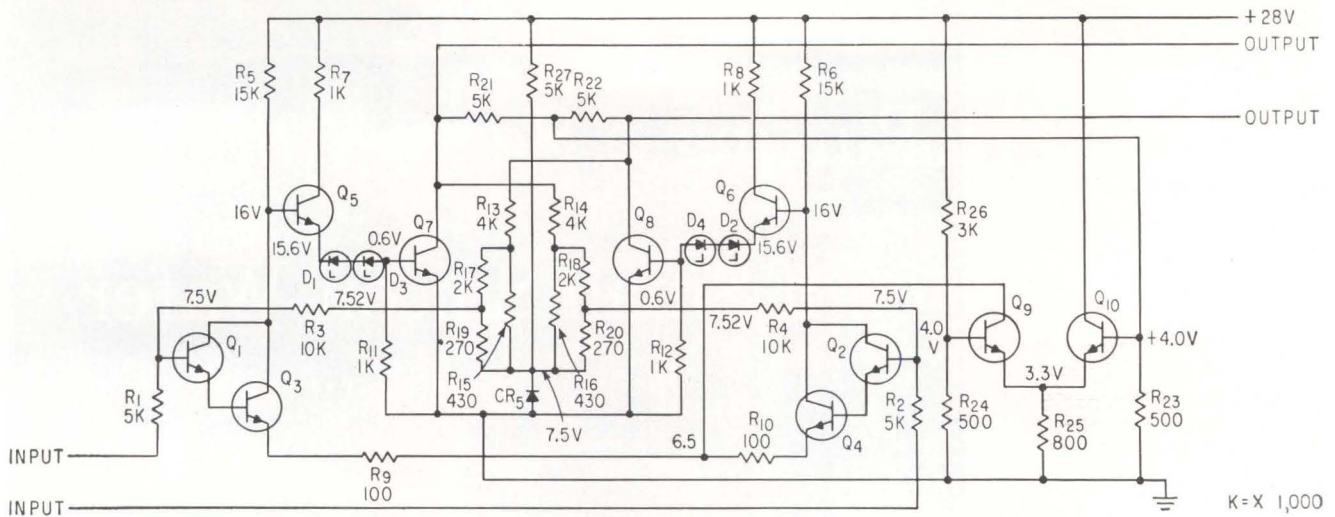
sistors  $R_{11}$  and  $R_{12}$  provide thermal stabilization for the power stage and guarantee that the zeners are broken down.

Open-loop gain of the differential forward amplifier  $Q_1$  through  $Q_4$  is greater than 2,000. The closed-loop gain, however, is determined by resistor ratios in the differential feedback network:  $R_1$  through  $R_4$  and  $R_{13}$  through  $R_{20}$ . The overall gain is precisely specified to be 200 by this technique.

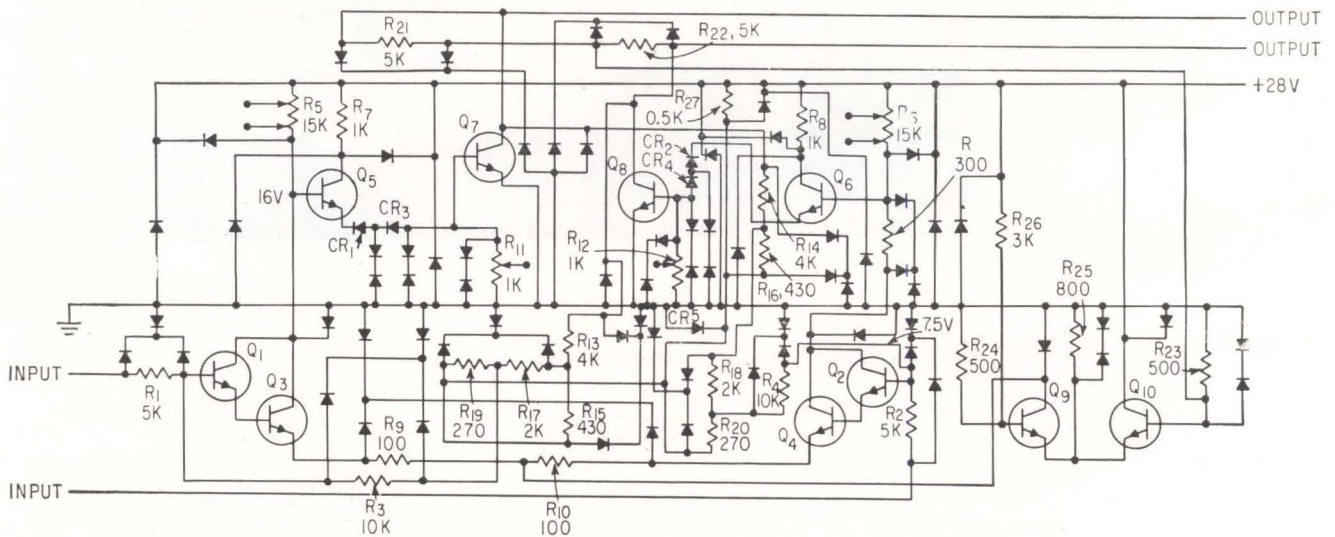
Direct-current operating points are stabilized by the common-mode feedback amplifier consisting of  $Q_9$  and  $Q_{10}$  with resistors  $R_{21}$  through  $R_{26}$ . The signal across the output is differentially summed by  $R_{21}$  and  $R_{22}$  cancelling the a-c components. The d-c component is then amplified and applied to the emitters of the differential input Darlington pair.

The method of isolation, which consists of back-to-back junction surfaces, alters the actual circuit





(A)



(B)

**BEFORE AND AFTER.** Schematic (A) is the original circuit of the servo amplifier. When it is fabricated on the silicon wafer, circuit (B) results because of distributed diode planes introduced by the substrate—Fig. 1

operation by inserting distributed diodes in a complicated manner within the circuit, Fig. 1B.

**TRANSISTOR DESIGN** — Since the circuit must deliver sizable amounts of power, the output stage received a great deal of attention. In conventional power transistors the bulk of the collector body is of low resistivity. Modern  $n$  on  $n^+$  epitaxial planar diffused devices are examples of this geometry. In crystal circuits it is difficult to achieve this result and maintain a collector breakdown of 120 volts. The motor that the circuit drives requires 94 volts peak-to-peak and 120 milliamperes peak current.

To solve the problem of low collector resistivity, 200 to 1 scale models of planar power transistors

were constructed. Emitters and collectors were made of aluminum foil using tape to mask surfaces between collector pads. Solutions of NaOH were mixed in different concentrations to simulate substrate material of 1, 2, 3 and 4 ohm-cm bulk resistivity. The depth of the solution was varied in 0.1-inch increments, simulating 0.5-mil variations in the depth of the collector region. The models were also modified to vary the length of emitter and collector junctions, and the separation of these junctions. A successful topological inversion of the power transistor structure was achieved as a result of data obtained from these models.

**INTERCONNECTIONS** — A set of rules was developed so that the

complex circuit could be translated into the best arrangement of the elements within the crystal. These rules eliminate interconnection crossovers and require that elements with critical interconnection lengths be close together.

Because the program involved placing an entire electronic system in one crystal of silicon, it was necessary to determine whether process technology was sufficiently advanced to enable initial good yields. Therefore, a layout that dissected the amplifier by symmetry into four distinct circuits, Fig. 2, was chosen. An interconnection scheme was developed that allows a choice of assembly methods depending upon test results of the individual wafers.

The first choice was to intercon-



nect within each independent circuit then dice the wafer to pick and choose the best circuit of each category, Fig. 3. The four 100-mil square chips are then mounted on the same header. Ball-bonded wire connections between chips complete the amplifier.

The second choice was to interconnect within and between four adjacent circuits by deposited aluminum and dice the wafer into complete amplifier chips, Fig. 4. The decision of which way to go is made by electrical tests after ohmic contacts are alloyed to the crystal.

**FABRICATION**—Circuits are produced from two types of material. The first type consists of a 20 ohm-cm *p*-type crystal upon which is grown a 1-mil 2.5-ohm-cm *n*-type epitaxial layer. The second type is a bulk 2.5-ohm-cm *n* wafer. Processing of the second type is described since the steps are typical of both.

The wafer is lapped and polished to a 4.5-mil thickness. Then a 25,000 angstrom thickness of steam oxide is grown and subsequently etched away. This step removes work damaged crystal layers and yields a smoother surface than mechanical polishing. A 10,000 angstrom thickness oxide is now grown and photoresisted to produce isolation moat contours. Boron from a tribromide source is deposited ( $C_1$ , approximately  $10^{21}$  atoms per  $cm^3$ ) and simultaneously diffused from top and bottom, thus creating *n* regions that are isolated by back-to-back junction planes. The bases of the transistors, the *p* part of diodes, and all resistor networks are diffused from a boric-acid source. The predeposition is controlled so that a sheet resistivity of 250 ohms per square is maintained. The next step is to diffuse all emitters, make *n*<sup>+</sup> contact areas in the collector regions, and complete the zeners. A phosphorus pentoxide process is employed for *n*<sup>+</sup> deposition.

Holes are then etched into the oxide where contact to the crystal is desired. Aluminum is evaporated over the entire wafer and subsequently etched completely off the oxide. The aluminum is spike-alloyed into the crystal. Regrowth of *p* material in the collector regions are prevented by the *n*<sup>+</sup> diffusion. Interconnection of elements is ac-

complished by a similar procedure of deposition and removal. The aluminum leads are vacuum baked at 500 C to alloy the aluminum into the surface of the oxide layers.

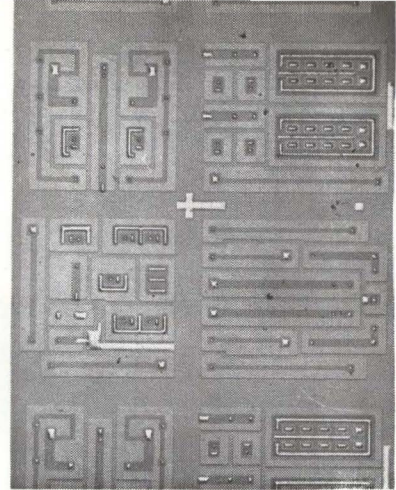
Careful attention to the porosity of the photoresist is maintained throughout to prevent development of pinholes in the oxide. The KPR (Kodak photoresist) is monitored in a crossed Nicol prism arrangement, for small particles and filaments. Impurities reveal themselves by depolarizing light that they scatter. Oxides are routinely checked by exposure to chlorine gas at 950 C. Pinhole counts range between 0 and 10 per wafer.

After dicing, mounting and lead attachment, the circuit is electrically evaluated. The good units are cleaned in deionized water and vacuum baked for 1 hour at 300 C. Hermetic sealing is accomplished by electron-beam welding.

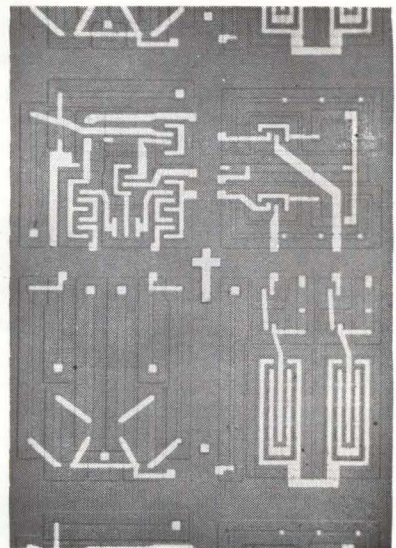
**TESTING**—To evaluate the servo amplifier functionally, a controlled 400-cps input signal is coupled to the amplifier through a ratio transformer. The input signal is measured both rms and peak to peak. Output of the amplifier is fed into a tuned servo motor, whose primary is open so that the load simulates stalled conditions. The rms output from either  $Q_1$  or  $Q_2$  to ground is then measured. Peak-to-peak output voltage is measured across the motor windings.

Transfer characteristics of the amplifier are determined by adjusting the ratio transformer and reading input and corresponding output voltages. The rms output is only read across half of the output; however, the two halves are 180 deg. out of phase so that they can be added linearly to obtain the total rms output. Quiescent current is approximately 60 ma per power transistor with an additional 10 ma in the B+ circuit. The current swings between 0 and 120 ma, while the rms into the motor winding is 36 volts for a 28-volt supply.

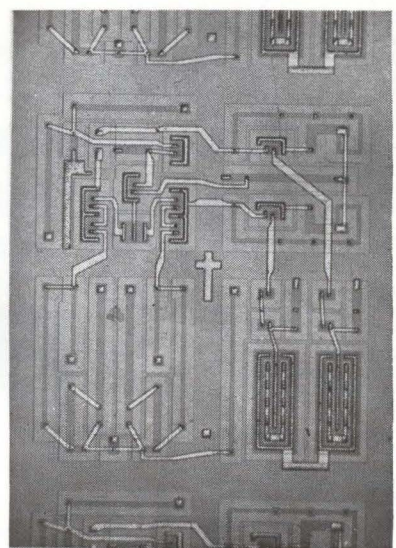
This paper represents the work of a team of scientists and engineers at Norden, who have been supported by United Aircraft Corp. and the Navy Bureau of Weapons. The work was sponsored by the Bureau of Naval Weapons under contract NOW-61-1053-C.



FOUR CIRCUITS comprise the complete amplifier. Here they are shown without interconnections—Fig. 2



CONNECTIONS within each individual circuit are made first. Then the circuits are tested to determine the next step in fabrication—Fig. 3



COMPLETED servo amplifier with all interconnections—Fig. 4



# New Design Concept Reduces

*High-power klystron tube uses electrostatic focusing of electron beam instead of conventional solenoid or permanent magnet. First model of an S-band klystron produces 15.5 Kw peak power with an efficiency of 25 percent. Multimegawatt tubes at L-band are contemplated*

By S. R. MECHTEL and A. MIZUHARA

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**THE CONVENTIONAL** klystron amplifier is valuable for amplification of r-f signals at uhf and microwave frequencies. It is used widely in radar, communication, navigation and guidance, particle accelerators and television transmission. It is the only device that offers the combination of high gain, high power, good efficiency and long life at these frequencies. Klystrons are relatively insensitive to load changes and retain high efficiency and gain over a wide range of voltages. Other features of klystrons are their simplicity, ruggedness and suitability for mass production.

One of the disadvantages of high-power klystrons is that they require a strong magnetic field in the axial direction for focusing the electron beam. This field is usually generated by an electromagnet, and less frequently by a permanent magnet.

Either way the weight and volume of the magnets is many times that of the tube itself. The permanent magnet also produces a stray magnetic field, which may interfere with other equipment and the solenoid requires a power supply that is inherently heavy and bulky and reduces the overall efficiency. Both the electromagnet and the permanent magnet add to the initial cost.

Elimination of focusing magnets would be highly desirable, especially in mobile, airborne and space systems where space and available power are at a premium, and weight must be kept at an absolute minimum. The application of a conventional klystron is also limited by its focusing magnets in phased-array radar, in which the tubes must be packed densely.

It has been known for a long time that electron beams can also

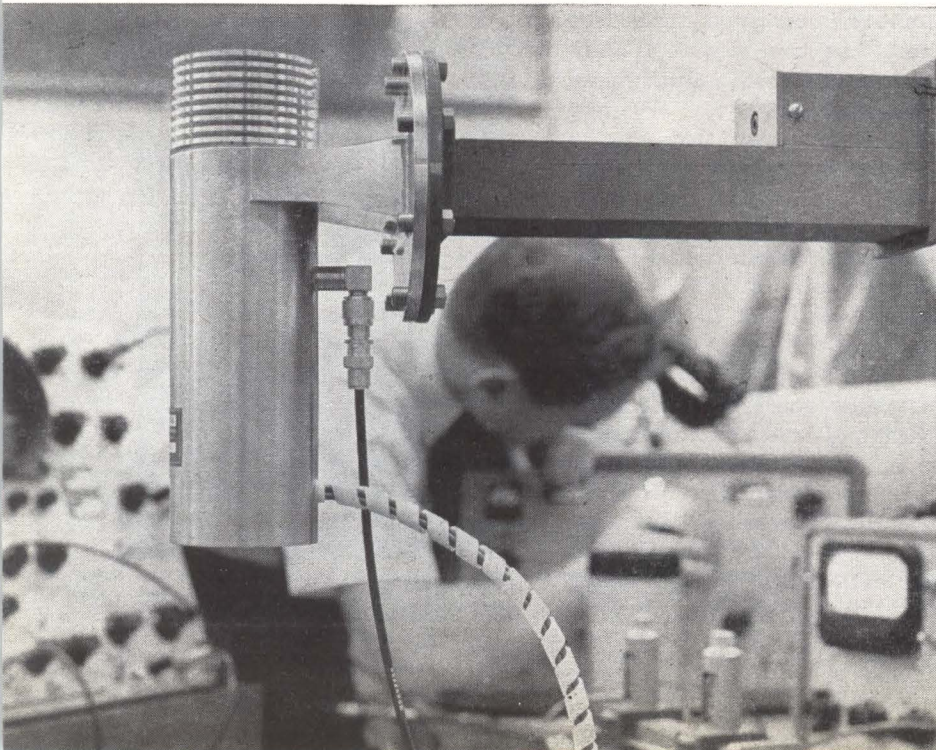
be focused by electrostatic fields. This is done successfully in cathode-ray tubes and electron microscopes. However, in attempting to use the same principle in a klystron amplifier, the problems encountered are incomparably more difficult. This is due to the high current densities within the beam of a klystron.

**FOCUSING**—The focusing scheme of the newly developed electrostatic klystron incorporates Einzel lenses. Figure 1 shows an electrostatically focused klystron. The dimensions of the lens system were chosen so that optimum operating performance is achieved with the lens voltage equal to the cathode voltage. This allows the lens electrode to be internally connected to the cathode; therefore, no extra power supply for the lens is required; that is, single voltage operation of the tube is possible. Such an electrostatic klystron retains all the favorable characteristics of a conventional, magnetically focused klystron without the handicap of the magnets.

Figure 2A shows the r-f output of the tube plotted against r-f drive power at a beam voltage of 20 Kv. In Fig. 2B, the saturated r-f output power is given as a function of the beam voltage. Finally, Fig. 2C illustrates the variation of efficiency with the beam voltage. As the curves of Fig. 2 show, the behavior of the tube is the same as that of a conventional klystron.

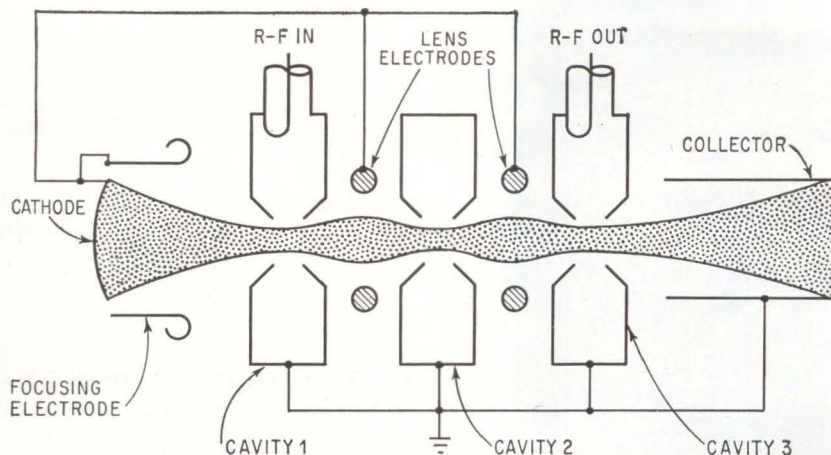
**POWER**—The average power of 850 watts, given in the table, was

*KLYSTRON weighs only five pounds, which is about 3 percent of the weight of a conventional klystron with magnets*





# KLYSTRON WEIGHT



ELECTROSTATICALLY focused klystron, with lens electrodes connected internally to cathode, eliminating extra power supply for lens—Fig. 1

measured when the body of the tube was cooled by a small air blower. With liquid cooling, a much higher average power should be achievable. Furthermore, it is hoped that by improving the electron optics of the tube, its efficiency can be raised to 35 to 40 percent.

The weight of the first experimental klystron was fifteen pounds. The photo shows the latest, fixed-tuned version of the tube, which weighs only five pounds. The weight of the electrostatically focused klystron is only about three percent that of a comparable conventional

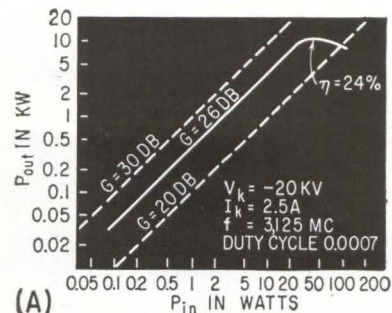
klystron with its magnets.

Considerably higher power than the 15 Kw obtained from the experimental model is possible. By scaling the present tube to a beam voltage of 100 Kv, an r-f output power of nearly 1 Mw can be expected at S-band. At lower frequencies, such as L-band, a multimewatt electrostatically focused klystron seems feasible. Higher gain can be achieved by simply increasing the number of cavities.

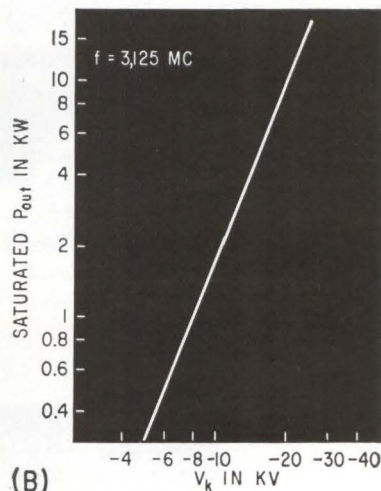
**USES**—The new type of klystron amplifier seems especially suitable and important where weight and volume of the tube must be kept at a minimum and stray magnetic fields cannot be tolerated. Applications include radar and communication systems in airborne and mobile applications. The klystron should also prove useful in future satellite and space vehicles, with the advent of nuclear power supplies that are now under development.

One feature of the klystron that can be exploited in certain applications is its ability to be self-supporting on its output waveguide flange. This can be used advantageously where the klystron is mounted directly at the focal point of the antenna; for example, in radar, communications, navigation-guidance, active radio astronomy and telemetry systems.

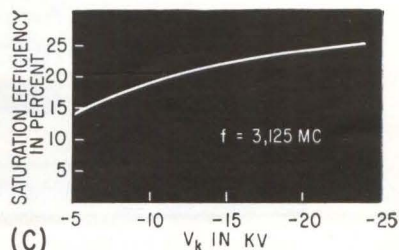
Perhaps one of the most important applications for the electrostatically focused klystron is in



(A)



(B)



(C)

PERFORMANCE CURVES: power output and beam transmission versus r-f power input (A); saturated power output versus cathode voltage (B); efficiency versus cathode voltage (C)—Fig. 2

## RESULTS

This new concept drastically reduces the weight and volume of the high-power klystron, and will be of interest to the military equipment designer.

The first tube made of this type was a 3-cavity klystron for moderately high power levels at S-band. The results achieved are

|                               |               |
|-------------------------------|---------------|
| Frequency                     | 3,125 Mc      |
| Beam Voltage                  | 22.5 Kv       |
| Beam Current                  | 2.8 amp       |
| R-F Output                    | 15.5 Kw peak  |
| Power                         | 850 W average |
| Small Signal                  |               |
| Gain (non-synchronous tuning) |               |
| Saturated                     |               |
| Gain                          | 23.5 db       |
| Efficiency                    | 25 percent    |

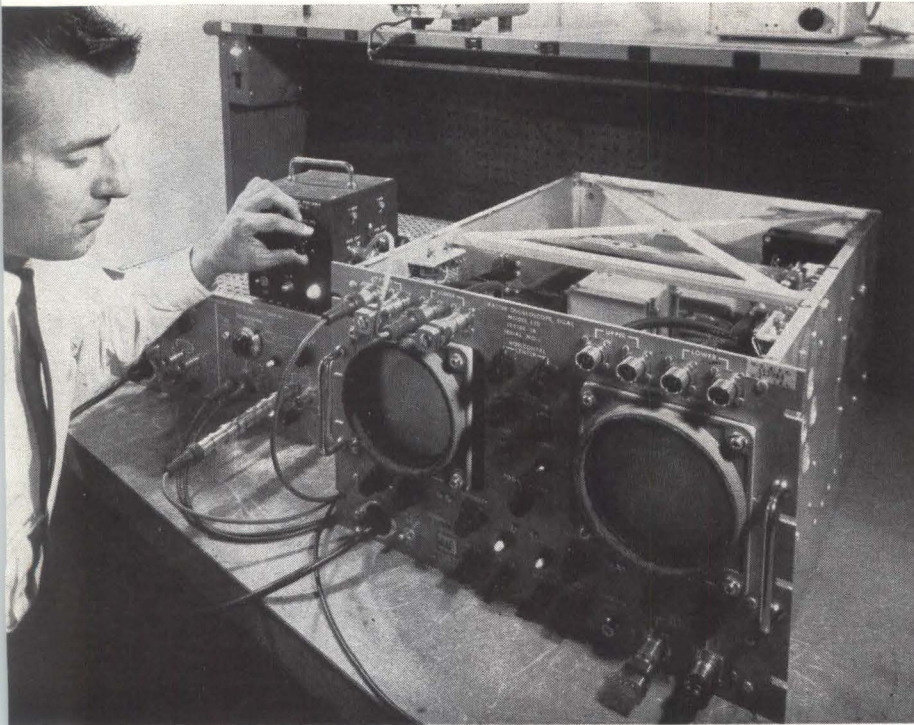
phased-array radar systems. Because the klystrons are compact and have no magnetic fields, they can be placed side by side with no interaction between tubes. Since the klystron is simple in design and suitable for mass production, the initial cost of such a phased array radar system should prove to be economically practical.

The authors acknowledge the support given by the U. S. Naval Ordnance Test Station, China Lake, California, during the first phase of the work.



# Use RASTER

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RASTER oscilloscope such as this can be used in any application where the time intervals between various events is required.

RASTER OSCILLOSCOPES have been used to measure detonation velocities in high explosives and a basic design has been developed.<sup>1</sup> The design incorporates into a compact package all the circuits and hardware to generate the raster display. It uses transistors. The power consumption is only 100 watts, a considerable advantage over designs using vacuum tubes as active elements.

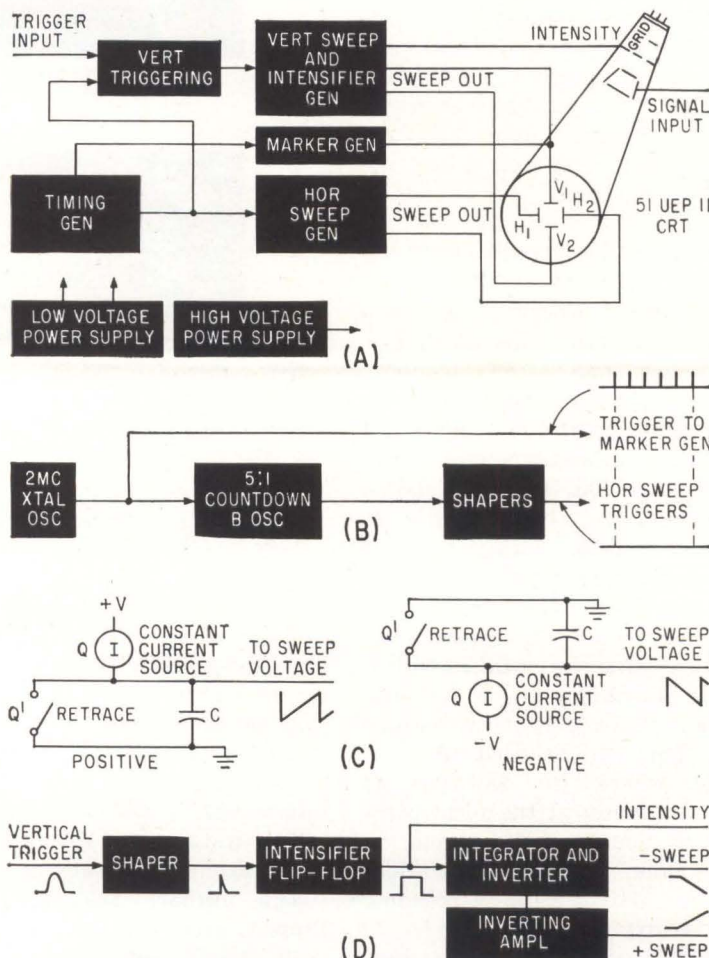
The design reliability, proved by life tests of over 5,000 hours, shows that silicon transistors can be safely operated at the high voltages needed in cathode-ray-tube deflection systems. The oscilloscope is shown in the photo.

DESIGN—In measuring time intervals, the end points are represented by pulses that could trigger digital time-measuring equipment. However, the amplitude and shape of the pulses may not be accurately known and an analog system such as the raster scope is needed. The design covers time intervals from 0.5 to 100 microseconds, and has a time resolution of 0.05 microsecond.

Complete use of transistors provides reliability, low power consumption, and small size. Good performance is obtained because the subassemblies can be mounted physically near the crt, thus reducing critical lead lengths. Because the design imposed by the crt requires that high voltages be handled by the transistor circuits, silicon mesa transistors are used throughout.

In many of the circuits the transistors operate in the avalanche mode, enabling them to handle reliably high voltages and generate high speed pulses.<sup>2</sup>

Batteries provide a stable source



RASTER SYSTEM for new compact oscilloscope (A); and details on timing generator (B), horizontal sweep generator (C), and vertical sweep and intensifier (D)—Fig. 1



# OSCILLOSCOPES

## for Faster Time Measurements

*Test oscilloscopes using tv-type scanning make optimum use of the crt face in displaying high-resolution time-interval measurements. This compact oscilloscope uses transistors, diodes and tunnel diodes for all stages*

for the sweep-circuit power supply and are isolated from ground.

**DISPLAY**—Usually a raster oscilloscope requires a crt with 3 sets of deflection plates, 2 sets presenting the raster display, with the timed pulses applied to the third set. This third set of plates makes the crt versatile since there is isolation between raster scanning and pulse display. The raster system is outlined in Fig. 1A.

The basic horizontal scanning rate for this design is 400 Kc, controlled by a 2-Mc crystal oscillator. The 2-Mc oscillator output triggers a blocking oscillator, which counts down by five to produce the 400-Kc timing pulses for the horizontal sweep (Fig. 1B).

The 2-Mc oscillator output triggers the marker generator which generates time-mark pulses used to time the display accurately. These time-mark pulses are applied to the vertical plate and their rise time, width and fall time are short so that there is minimum interference between the timing pulse and the pulses being timed.

The horizontal sweep generates a push-pull ramp voltage to produce the horizontal scan. The voltage swing is  $\pm 130$  v and special silicon mesa transistors are used. To provide the horizontal sweep a capacitor is charged with a constant current (Fig. 1C). Transistor *Q* operates in the common-base mode and provides a constant charging current for sweep capacitor *C*.

Transistor *Q'* discharges *C* to provide the sweep retrace; *Q'* is driven at a 400-Kc rate by a continuous pulse train from the timing unit.

The vertical sweep circuit pro-

vides the scanning voltage to deflect the beam vertically. A push-pull 130-v sweep voltage is required. The crt is biased to cutoff except during the vertical sweep interval. An intensifier pulse turns on the beam when the vertical sweep starts. Vertical sweep is combined with the intensifier gate generator (see Fig. 1D). The shaper provides a latching function that prevents double pulsing of the vertical sweep. The input trigger pulse is shaped and triggers a monostable multivibrator. The on time of the multi determines the time the display is intensified. On time is variable, covering a range of 25 to 100  $\mu$ sec. Amplitude of the intensifier pulse is approximately 100 v. The intensifier pulse is integrated to provide the negative ramp voltage for the vertical sweep.

A gain-of-1 inverter provides the positive ramp voltage for the push-pull deflection system.

The intensifier multivibrator uses an avalanche triggering system to

improve the turn-on time of the intensifier pulse.

Trigger input to the vertical sweep circuit is provided by an amplitude discriminator. The circuit also synchronizes the vertical trigger pulse to the horizontal trigger pulse so that the display on the face of the tube will be stationary, making it easier to focus the display.

If a pulse to be timed occurs during the retrace time of the horizontal sweep, it is difficult to measure. To overcome this problem, another indicator is used, whose horizontal sweep is delayed in time. This other indicator called a slave, has all of its functions in parallel with the master except the horizontal sweep.

The timing generator provides a delayed sweep trigger for the slave horizontal sweep. A block diagram of the timing of the horizontal sweeps is shown in Fig. 2.

**CIRCUITS**—To facilitate maintenance, most of the electronic func-

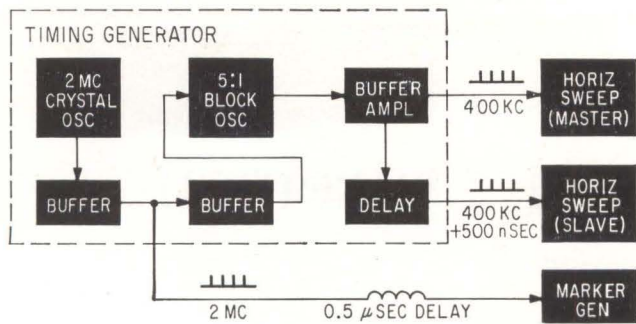
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### WHY A RASTER SCOPE?

Conventional oscilloscopes measure rise times and pulse widths precisely and easily. However, for measuring time intervals between pulses, sweep linearity imposes a basic limitation. If better than 3-percent measurements are required, a raster type scan has an advantage in that it increases time resolution capabilities by the number of total scanning lines in the raster. This article describes a transistor raster oscilloscope for making such high-resolution time-interval measurements

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**TIMING GENERATOR**  
provides a delayed sweep trigger for the slave horizontal sweep—Fig. 2

tions are performed with circuits fabricated on printed-circuit assemblies. Major circuit functions may be replaced as a unit.

The timing generator is shown in Fig. 2 and in Fig. 3. Transistor  $Q_1$  is a crystal-controlled blocking oscillator and generates a highly nonsinusoidal voltage across the emitter resistor,  $R_1$  (Fig. 3);  $C_1$  varies the amplitude of the fast-rising part of the emitter voltage and has minimum effect on the repetition rate of the blocking oscillator;  $C_2$  and  $R_2$  differentiate the pulse and the emitter follower,  $Q_2$ , drives the marker timing delay line at point B. Transistor  $Q_3$  is a limiter whose input is differentiated by  $C_3$  and  $R_3$  in parallel with  $R_1$ . The output of  $Q_3$  synchronizes the 5:1 countdown stage,  $Q_4$ , which operates as a blocking oscillator whose recovery time is controlled by  $C_4$ . The synchronizing pulses at the

base are such that the stage will not trigger until the collector voltage has recovered to a certain level.

The 400-Kc pulses across  $R_5$  are reduced in level by the forward voltage drop of  $FD_{101}$  diode before being applied to the base of  $Q_5$ . Transistor  $Q_5$  operates in the avalanche mode and its output at D provides the drive pulse for triggering the master horizontal sweep. After being triggered, the collector of  $Q_5$  remains near ground. When the next 2-Mc pulse feeds through  $T_1$   $Q_5$  turns off and  $C_5$  charges toward 50 v. This voltage rise is coupled through  $C_6$  and triggers  $Q_6$ . When  $Q_6$  avalanches, it provides an output pulse at point F to trigger the slave horizontal sweep. This output is delayed 500 nsec from the pulse at point D.

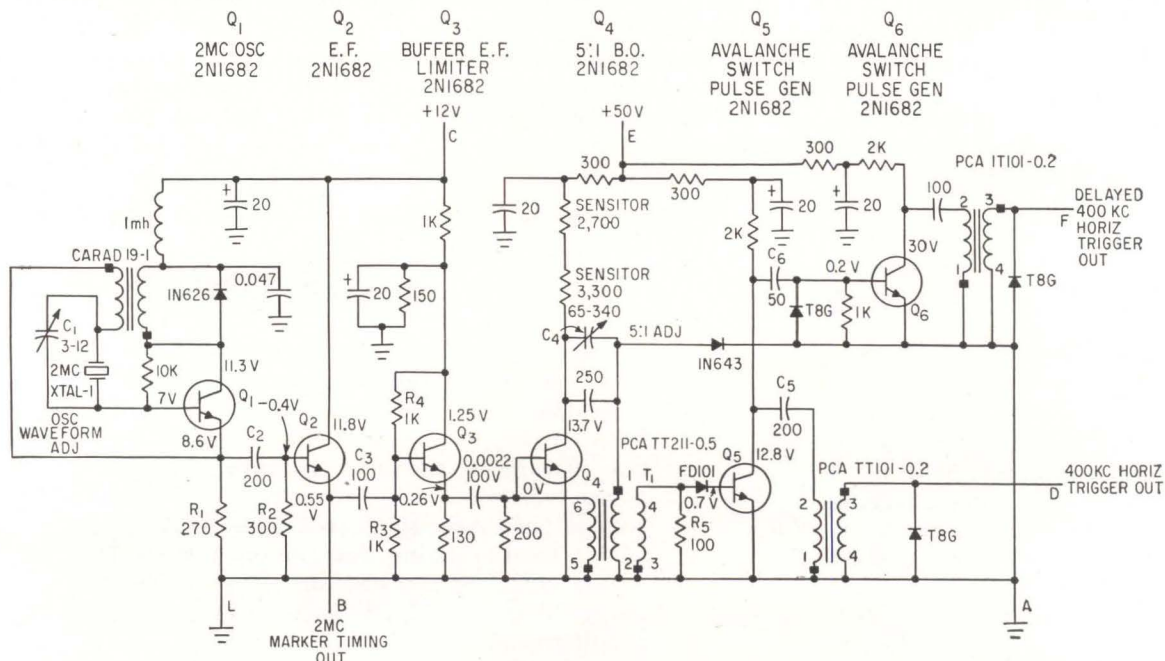
**HORIZONTAL SWEEP**—Circuits to generate the horizontal sweep

are shown in Fig. 4. In the positive sweep, the value of  $Q_3$  collector current is determined by the battery through the + SWEEP AMP control. This constant current charges  $C_3$  to provide a linear sawtooth of voltage to sweep the crt beam. After  $C_3$  is charged toward 150 v,  $Q_4$  will be operating at a point in its avalanche switching region;  $Q_4$  is triggered by the 400-Kc pulse from  $Q_2$  through  $T_1$  and discharges  $C_3$  to provide the sweep retrace.

The important characteristic of  $Q_3$  is its ability to provide a constant current source, which it does over a 150-v collector-voltage range. The important characteristic of  $Q_4$  is that its collector breakdown rating is greater than 150 v.

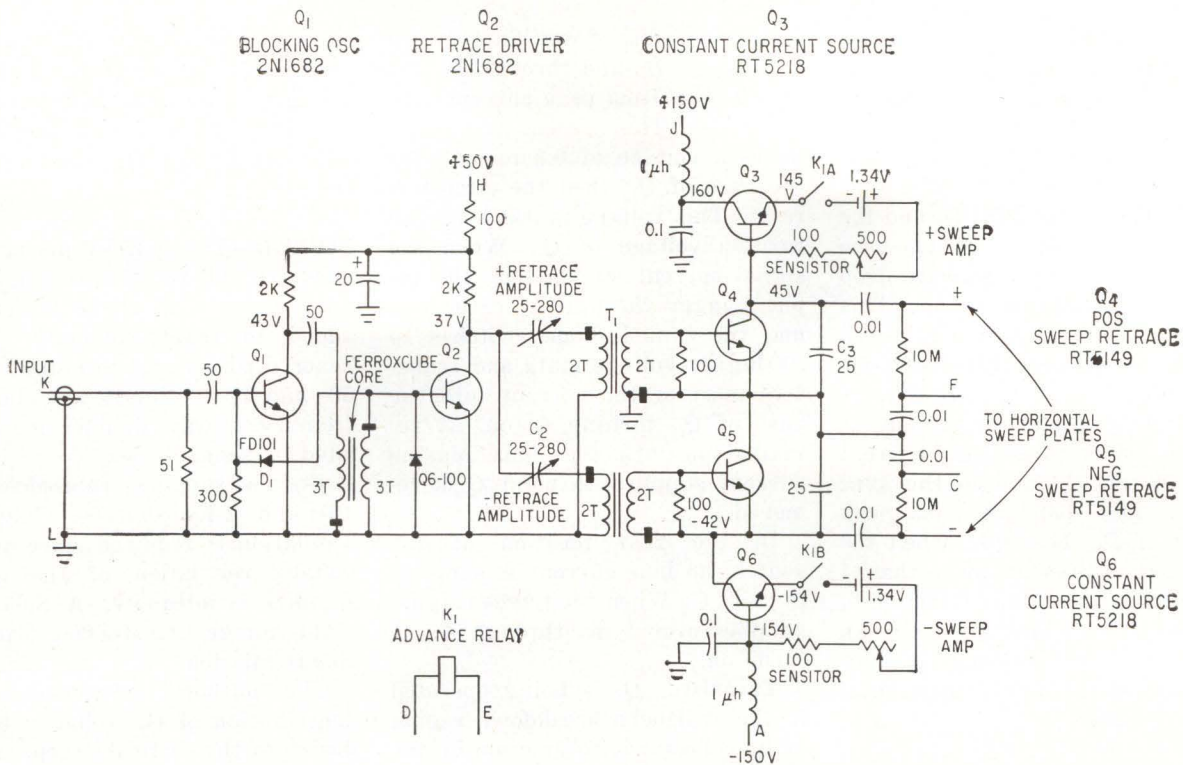
Negative sweep is similar to the positive sweep except that the capacitor is charged from the minus 150-v bus. This requires the emitter of  $Q_3$  to follow the sweep voltage and requires a special low capacitance pulse transformer. This transformer is constructed by winding miniature coaxial cable around a toroidal ferrite core; the same for  $T_1$ .

The input signal to the horizontal sweep circuit triggers two stages  $Q_1$  and  $Q_2$ , which reshape the timing pulses and retrace the horizontal sweep. Transistor  $Q_1$  is an avalanche-mode blocking oscillator

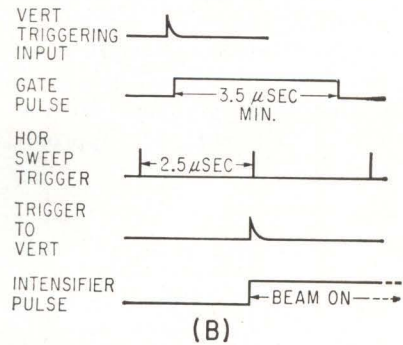
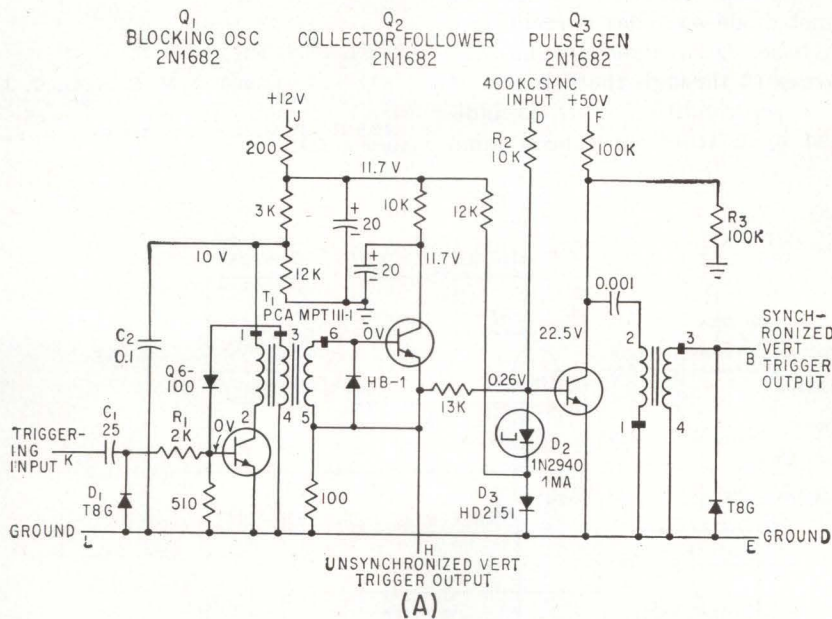


IN TIMING SYSTEM for horizontal sweep, output pulse at point F, which triggers slave, is delayed 500 nsec from pulse at point D—Fig. 3





HORIZONTAL SWEEP generator employs similar positive and negative sweeps except for method of charging—Fig. 4



VERTICAL triggering generator (A) and waveform diagram of vertical triggering (B)—Fig. 5

with feedback applied through  $D_3$ ;  $Q_2$  is switched by the output of  $Q_1$  and discharges the two 25-280 capacitors through the primaries of the two transformers following. The retrace drive pulses to the negative and positive sweeps are separately variable to compensate for differences in  $Q_4$  and  $Q_5$  characteristics. Relay  $K_1$  turns off the batteries when the scope is turned off. At a normal 3-ma battery drain, the battery life should be at least 500

hours.

Figure 5A shows the vertical triggering circuit. The voltage appearing at the vertical trigger input is discriminated against by a reverse bias. This bias is set by the trigger level control,  $R_3$ . The input trigger signal must overcome this bias before the vertical triggering circuit will operate. Figure 5B shows a waveform diagram of the vertical triggering. The vertical trigger input (Fig. 5) is differenti-

ated by  $C_1$ , and the input impedance of the stage  $Q_1$ . Diode  $D_1$  prevents negative input signals from affecting circuit operation;  $R_1$  attenuates the vertical trigger input applied to  $Q_1$ .

Transistor  $Q_1$  is a blocking oscillator whose output pulse width is greater than 3.5  $\mu$ sec, determined by  $T_1$  and  $C_2$ . This gate pulse is coupled to point  $H$  through  $Q_2$ . When a fire-test switch (not shown) is in the FIRE position this output



triggers the intensifier and vertical sweep circuits. This gate pulse is also coupled into the base of  $Q_3$ .

A 1-ma tunnel diode,  $D_2$ , is used with  $Q_3$  as a coincidence gate;  $Q_3$  generates an output only if a sync pulse is present at point  $D$ , and the gate pulse is present at  $H$ . The base of  $Q_3$  is biased by the forward drop of  $D_2$ , a germanium diode. This voltage level is below that required to turn on silicon transistor,  $Q_3$ . When a sync pulse from  $D$  is present and no gate pulse is present,  $Q_3$  remains off because the current flow through  $R_2$ , due to the sync pulse, is less than the 1-ma peak current of  $D_2$ . However, when the gate pulse is present, more than 1 ma flows through  $D_2$  and it switches, turning  $Q_3$  on. This produces an output pulse at  $B$  which is synchronized to the 400-Kc horizontal trigger pulses.

**VERTICAL SWEEP**—The vertical sweep and intensifier circuits are shown in Fig. 1D and Fig. 6. In the shaper,  $Q_1$  (Fig. 6) triggers the intensifier pulse. It operates in two different modes determined by the position of a fire-test switch.

In the FIRE position of the switch, a current of approxi-

mately  $\frac{1}{2}$  ma flows into point  $C$ , through  $R_2$ , and through  $D_7$  and  $D_1$  ( $D_7$  is a 1-ma peak current tunnel diode). This current flow establishes a voltage of 0.3 to 0.4 v at the base of  $Q_1$  when the circuit is reset. This voltage is less than the turn-on voltage of  $Q_1$ . When the signal current supplied by the input trigger through  $R_1$  exceeds  $\frac{1}{2}$  ma, the tunnel diode switches to its higher voltage state and transfers most of the current into the base of  $Q_1$ , turning  $Q_1$  on. It remains on until the  $\frac{1}{2}$ -ma biasing current supplied to point  $C$  is removed.

In the TEST position of the switch, no bias current is supplied to point  $C$ . When the trigger signal supplies over 1 ma through  $R_1$ ,  $Q_1$  turns on.

Transistor  $Q_1$  is being operated in the avalanche breakdown region of its collector-base junction by the current supplied through  $R_3$ . Its collector voltage is then equal to the breakdown voltage ( $BV_{CES}$ ) of the collector-base junction. When the tunnel diode switches current into the base,  $Q_1$  avalanches and discharges  $C_1$  through the primary of  $T_1$ . Reset condition of  $Q_1$  is indicated by a front-panel neon lamp

connected to point  $D$ . This lamp is on when  $Q_1$  is off;  $D_2$  equalizes the voltage swing and maintains the collector voltage of  $Q_1$  at the breakdown level when the reset lamp is on.

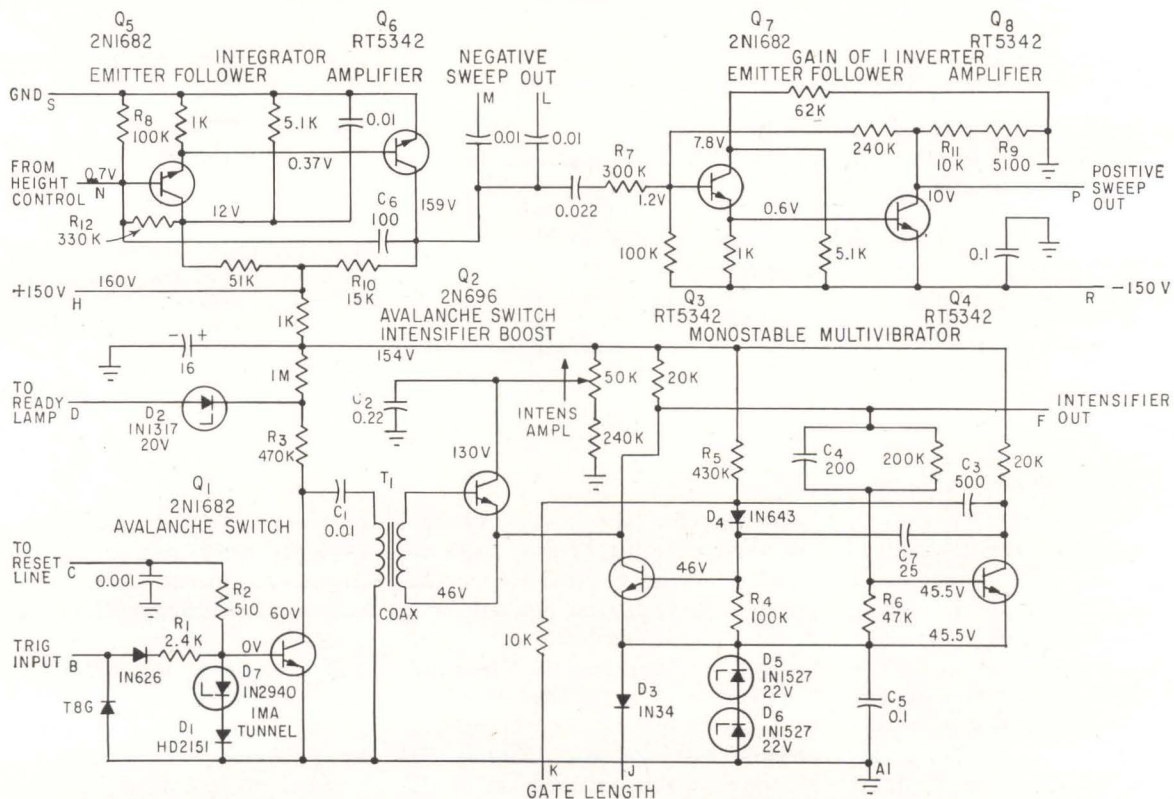
**POWER**—The  $\pm 150$ -v power supplies are half-wave capacitor input filter types with choke smoothing added to reduce 60-cycle ripple. Zener diodes regulate output. The 50- and 12-v voltages are obtained from a half-wave doubler and regulated by zener diodes.

Modular supplies are used for the 10- and 2-Kv sources. Only line regulation is required since output voltage regulation of the power supplies is adequate. A Sola constant-voltage transformer provides line regulation.

The authors acknowledge the contribution of G. Holladay to the design of the vertical sweep circuit. This work was performed under the auspices of the U. S. Atomic Energy Commission.

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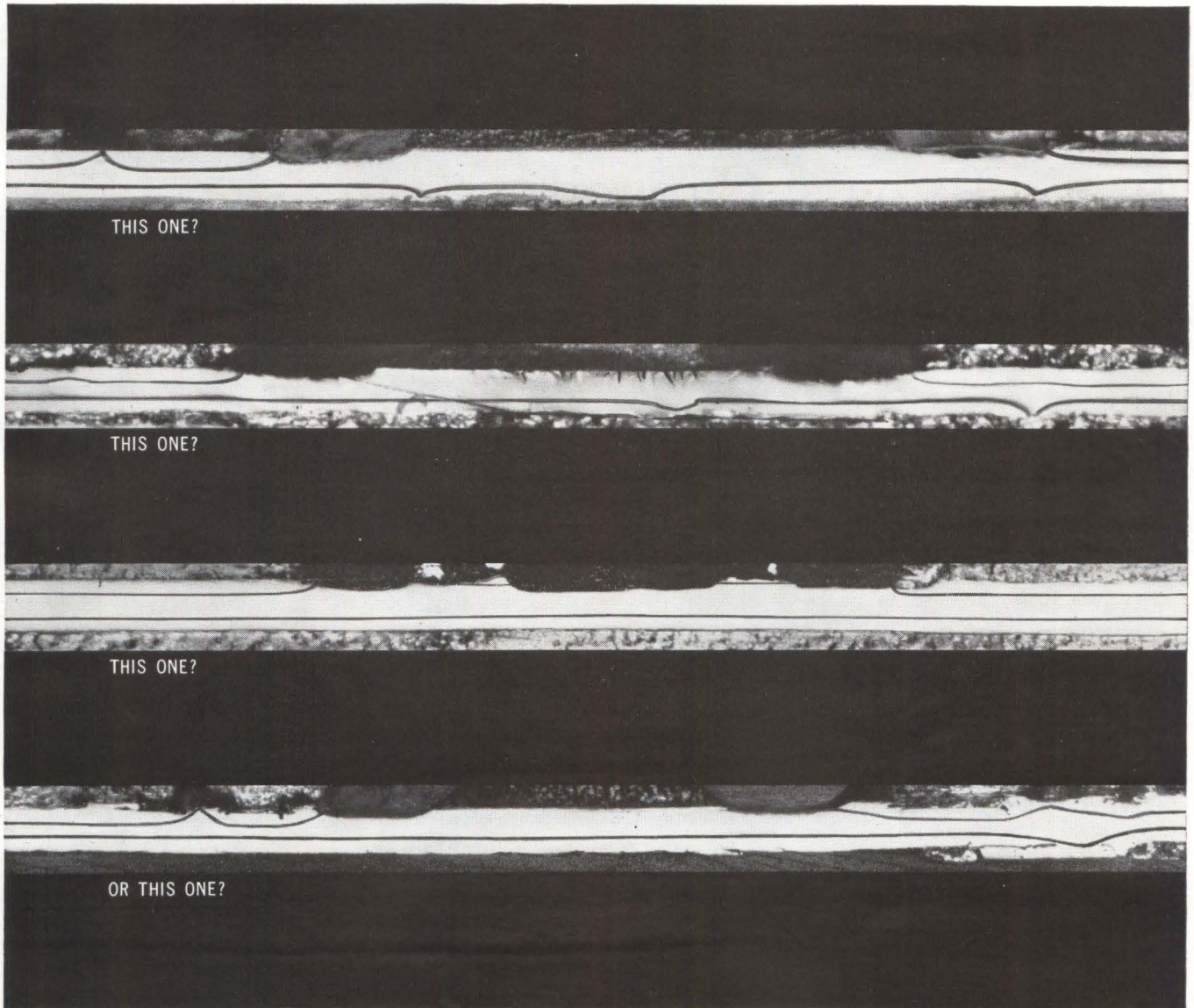


**VERTICAL SWEEP and intensifier.** In this circuit,  $Q_1$ , which triggers the intensifier pulse, operates in two different modes determined by a fire-test switch (not shown) that feeds into point  $C$ —Fig. 6

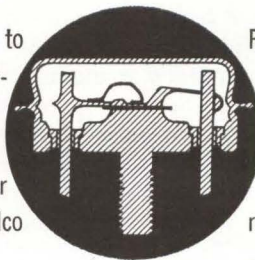


# Which power transistor junction would make your product perform best?

These are cross-sectional photomicrographs of emitter and collector junctions from power transistors produced by four different manufacturers. Which junction would provide better distribution of heat and current? Which junction is stronger, will last longer?



Answer: First, second and fourth samples, top to bottom, are non-planar junctions. Their imperfections allow concentration of current, lead to hot spots and eventual junction failure. Third sample is a planar junction, unique in power transistor fabrication and the result of Delco



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# Rapid Selection of VHF Bypass Capacitors

By LAWRENCE E. LEE  
Ball Brothers Research Corp., Boulder, Colo.

**SELECTION** of bypass capacitors is usually based on the relation

$$C > \frac{5 \text{ to } 10}{2\pi fR} \quad (1)$$

where  $R$  is the load to be bypassed and  $f$  is the lowest frequency that will be effectively bypassed.

This relation suggests that the larger the capacitance,  $C$ , the better the bypassing action will be. This is true for high values of  $R$  or low frequencies. However, for low values of  $R$  or very high frequencies, the inductance of the capacitor leads and plates must be considered.

The inductive reactance of the leads at frequencies near 100 Mc becomes so significant that the

bypassing values obtained from Eq. 1 are no longer valid.

### CAPACITOR INDUCTANCE—

Figures 1A and 1B illustrate a capacitor and its equivalent circuit. In general, the dielectric and lead losses,  $r$ , of r-f capacitors<sup>1</sup> are small and can be neglected when compared to the inductive reactances. Inductance  $L$  is the sum of the inductance of the leads,  $L_s$ , and capacitor plates  $l_p$ . At frequencies near 100 Mc the inductive reactance  $\omega l_p$  of the capacitor itself is small, and only the reactance  $\omega L_s$  of the leads is significant.

The inductance of a straight nonmagnetic wire with a length much greater than its diameter can be obtained approximately from<sup>2</sup>

$$L = 0.005l(2.3 \log_{10} (4l/d - 0.75)) \quad (2)$$

where  $L$  = inductance in microhenries,  $l$  = length of wire in inches, and  $d$  = diameter of wire in inches.

The variation of inductance as a function of length for No. 22 Awg wire is shown in Fig. 1C. This inductance can be appreciable; for example, at 100 Mc a wire one inch long has an impedance of nearly 16 ohms.

**BYPASS SELECTION**—At resonance, a series RLC circuit has

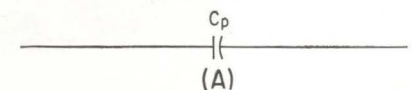
### HIDDEN PARAMETERS

Usually, capacitors are thought of as having only capacitance, inductors only inductance and resistors only resistance. But capacitors also have small amounts of inductance and resistance. Because these parameters are so small they remain hidden. In low-frequency work they are usually disregarded.

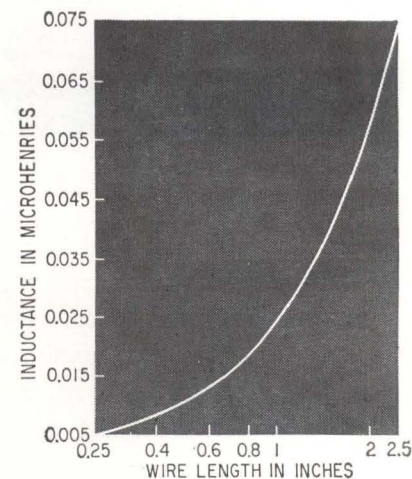
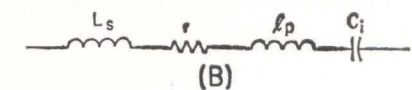
At very high frequencies, the hidden parameters suddenly become so important that, if they are neglected, the calculation of bypass capacitance can result in an error of one order of magnitude

nearly zero impedance. By choosing a capacitance that will pro-

(continued on p 46)



- $l_p$  = INDUCTANCE OF PLATES
- $L_s$  = INDUCTANCE OF LEADS
- $r$  = DIELECTRIC AND LEAD LOSSES
- $C_i$  = IDEAL CAPACITOR
- $C_p$  = ACTUAL CAPACITOR



IDEAL CAPACITOR (A) and its equivalent circuit (B). Lead inductance for No. 22 Awg wire as a function of length (C)—Fig. 1

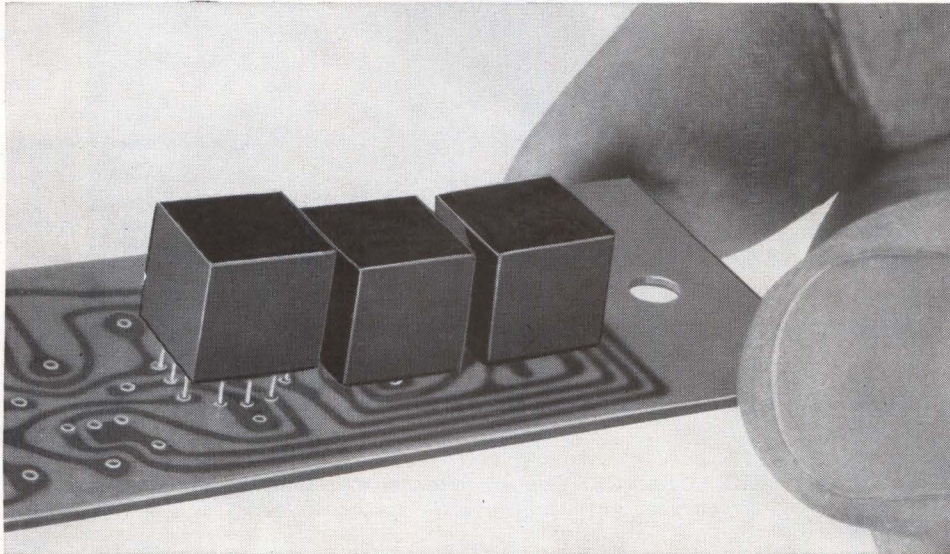
TABLE I—Resonant Frequencies of Capacitors With 1/2-Inch Leads

| Frequency<br>Capacitance<br>C | Frequency<br>Calculated<br>From Fig. 2<br>f<br>(Mc) | Frequency<br>Determined<br>Experimentally<br>f<br>(Mc) |
|-------------------------------|-----------------------------------------------------|--------------------------------------------------------|
| 50 pf                         | 145                                                 | 150                                                    |
| 100 pf                        | 100                                                 | 105                                                    |
| 500 pf                        | 45                                                  | 44                                                     |
| 0.001 μf                      | 32                                                  | 33                                                     |
| 0.005 μf                      | 14                                                  | 14.2                                                   |
| 0.01 μf                       | 10                                                  | 10.1                                                   |
| 0.05 μf                       | 4.5                                                 | 3.9                                                    |
| 0.1 μf                        | 3.2                                                 | 3.7                                                    |



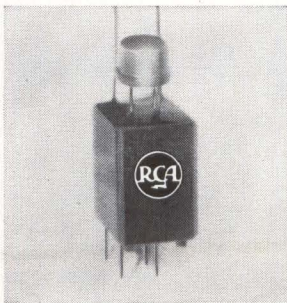
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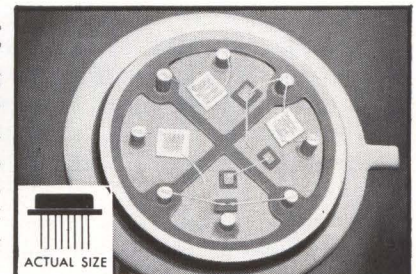
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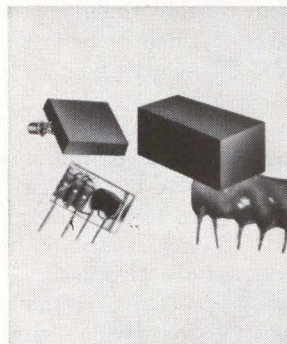
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TABLE II—Inductance Of Various Lead Gages

| Lead Size (Awg) | Inductance in Microhenries |               |                 |
|-----------------|----------------------------|---------------|-----------------|
|                 | 0.5 inch length            | 1 inch length | 1.5 inch length |
| No. 18          | 0.0098                     | 0.023         | 0.0375          |
| No. 20          | 0.0103                     | 0.0241        | 0.0392          |
| No. 22          | 0.0109                     | 0.0253        | 0.0409          |
| No. 24          | 0.0115                     | 0.0264        | 0.0425          |

TABLE III—Deviation Of Inductance For No. 22 Awg Wire

| Lead Length (inches) | Inductance in Microhenries for #22 Awg wire |         |             |
|----------------------|---------------------------------------------|---------|-------------|
|                      | -10 percent                                 | Nominal | +10 percent |
| 0.5                  | 0.0098                                      | 0.0109  | 0.0120      |
| 1.0                  | 0.0228                                      | 0.0253  | 0.0278      |
| 1.5                  | 0.0368                                      | 0.0409  | 0.0450      |

duce series resonance with the inductance of its leads, the lead inductance is effectively cancelled. This idea is used to construct the graph of Fig. 2. The reactance as a function of frequency for various capacitors and for 0.5, 1, 1.5 and 2-inch total lead lengths of No. 22 Awg wire is shown. This gage wire was selected because it approximates the wire size used in various capacitors.

Each crossing of an inductive reactance line by a capacitive reactance line indicates the frequency at which the corresponding capacitor is in series resonance with its leads. The optimum bypassing at a particular frequency occurs at these crossing points.

As an example of the lack of effectiveness of capacitance selection using Eq. 1, consider bypassing a 50-ohm load resistance at 100 Mc. A 500-pf capacitor, or even better, a 1,000-pf capacitor would have been chosen. However, from Fig. 2 at 100 Mc, 0.5-inch leads (1-inch total length), have an inductive reactance of nearly 16 ohms. The net reactance bypassing the 50-ohm load would then be:  $(16 - 1.6)$

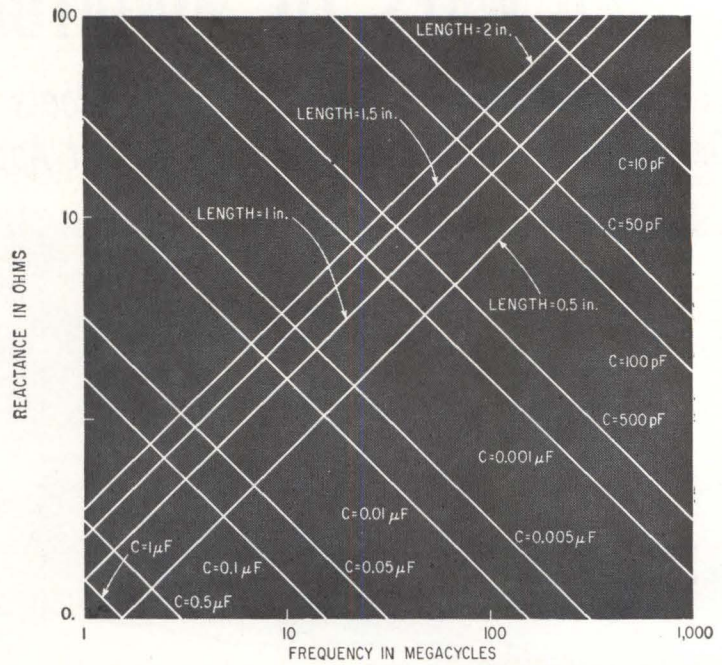
or 14.4 ohms for the 1,000-pf capacitor and  $(16 - 3.2)$  or 12.8 ohms for the 500-pf capacitor. The bypassing is inefficient. Figure 2 indicates that at 100 Mc, 100 pf is the optimum value.

Measurements were made of the resonant frequencies of various types and sizes of capacitors, to verify the theoretical data of Fig. 2. The average experimental values obtained for the various capacitors are indicated in Table I. The results indicate that the graph of Fig. 2 can confidently be used as a guide for selecting r-f bypass capacitors.

**LEAD SIZES**—Although No. 22 Awg is the most common lead size used in capacitors in the 10 to 1,000-pf range, lead sizes ranging from No. 18 to No. 24 Awg are also used.

Table II shows the inductance for various lengths of lead sizes. Table III shows the 10-percent deviation for No. 22 Awg. Comparing Tables II and III, the inductance for the various wire gages is within the  $\pm 10$  percent of No. 22 Awg.

The change in resonant frequency of the capacitors due to the change in inductance is<sup>3</sup>



REACTANCES of capacitances and leads as functions of frequency; various lead sizes are shown—Fig. 2

$$f_1 = \frac{1}{2\pi(LC)^{1/2}}$$

$$f_2 = \frac{1}{2\pi(LC)^{1/2}(1 \pm X)^{1/2}}$$

$$f_2 = f_1 \frac{1}{(1 \pm X)^{1/2}}$$

$$f_2 = f_1 \left[ 1 \mp nX + \frac{n(n+1)X^2}{2!} \mp \frac{n(n+1)(n+2)X^3}{3!} + \dots \right]$$

$$f_2 = f_1(1 \mp 0.5X + 0.375X^2 \mp 0.3125X^3 + \dots)$$

$$f_2 = f_1(1 \mp 0.5X) \text{ for } X \ll 1$$

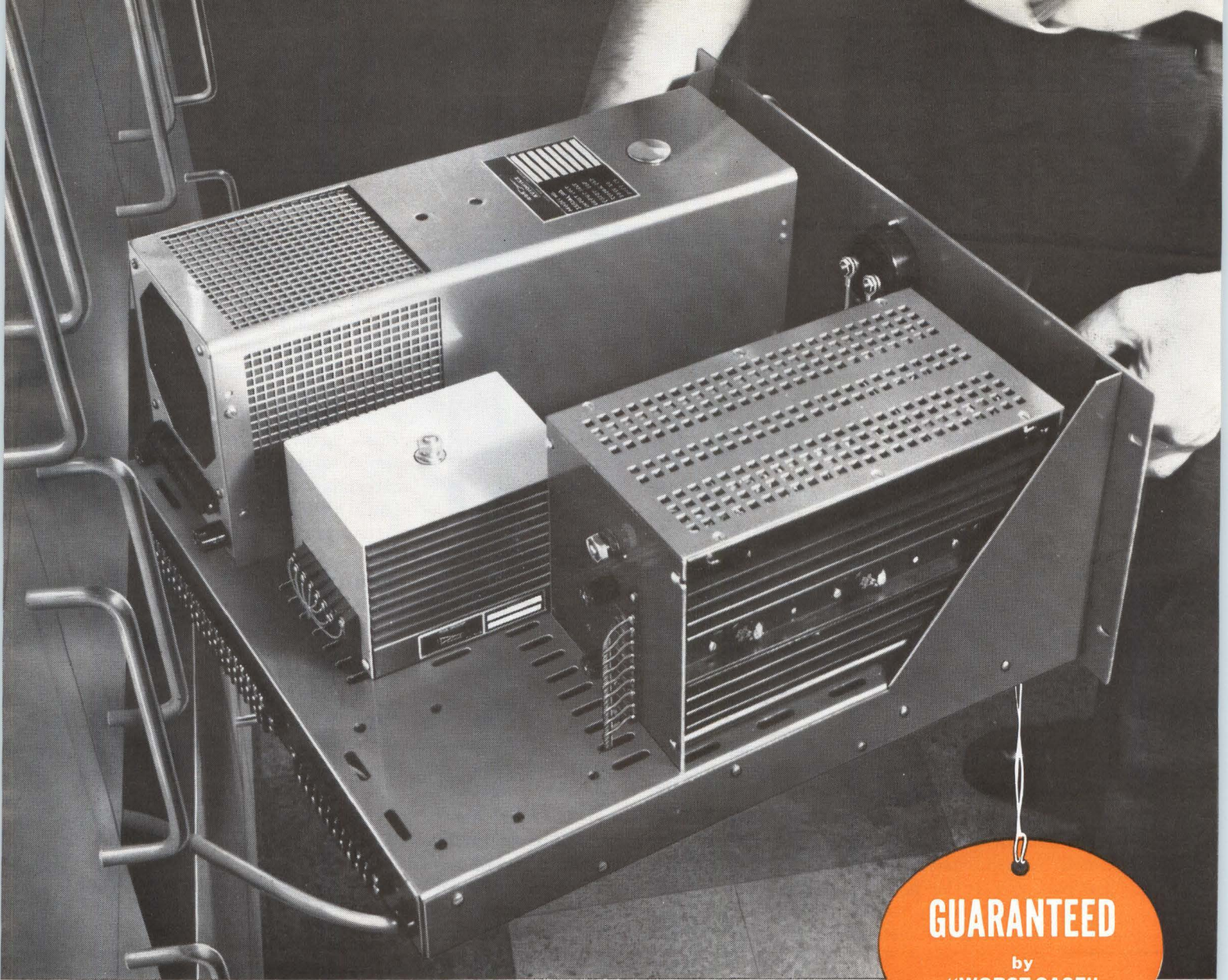
where  $f_1$  = resonant frequency,  $L$  = lead inductance,  $C$  = capacitance and  $X$  = change in inductance.

Therefore, a 10-percent change in  $L$  produces a 5-percent change in the resonant frequency. This represents a 500 Kc change at 10 Mc and a 5 Mc change at 100 Mc. Thus Fig. 1C is valid as an engineering design chart for wire sizes from No. 18 to No. 24 Awg.

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- (1) F. E. Terman, "Electronic and Radio Engineering", McGraw-Hill Book Co., 3rd Ed., p 24-26.
- (2) F. Langford-Smith, "Radiotron Designer's Handbook", Wireless Press, Australia, 4th Ed., p 1287.
- (3) C. R. C. "Standard Mathematical Tables", Chemical Rubber Publishing Corp., 11th Ed., p 349.





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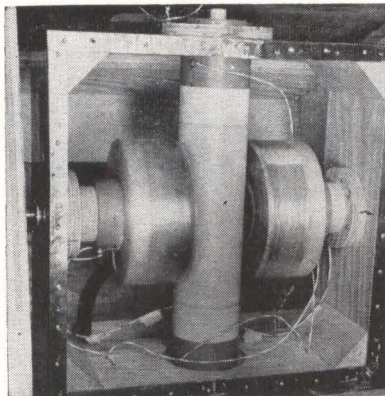
# Solid-State Nuclear Gyro Reported Feasible

*Gyro designer's goal nears:  
space vehicle guidance  
without moving parts*

By MICHAEL F. WOLFF  
Senior Associate Editor

**DEMONSTRATION** by Arma of the feasibility of a solid-state nuclear gyro represents a significant step toward the goal of many guidance system engineers—a gyro without moving parts. The claim is based upon Arma's report that they were able to align protons in an experimental directional gyro and then sense this alignment (ELECTRONICS p 8, Dec. 14).

The nuclear gyro belongs to a class of gyros that would use the angular momentum of atomic nuclei and electrons rather than the conventional rotor momentum as a directional reference (ELECTRONICS, p 20, Feb. 16). Because such gyros would have no moving parts they are expected to be more accurate and reliable than present gyros. They would also require less power



FIRST PUBLISHED closeup of nuclear gyro model shows polarizing and sensing coils. The sample of material is placed inside vertical coil

and produce minimum inertial reaction on a spacecraft.

**HOW IT WORKS**—There are many possible techniques for orienting and sensing the orientation of nuclear gyro particles. Arma uses nuclear magnetic resonance techniques. Here proton spin vectors

are aligned by simultaneously applying a pulsed d-c magnetic field and a pulsed r-f field. Purpose of the r-f field is to augment the proton alignment process by aligning electrons. These electrons then interact with the protons in such a way as to cause additional protons to be aligned. This phenomenon, cross-relaxation, can increase the number of aligned protons in some materials by a factor of three.

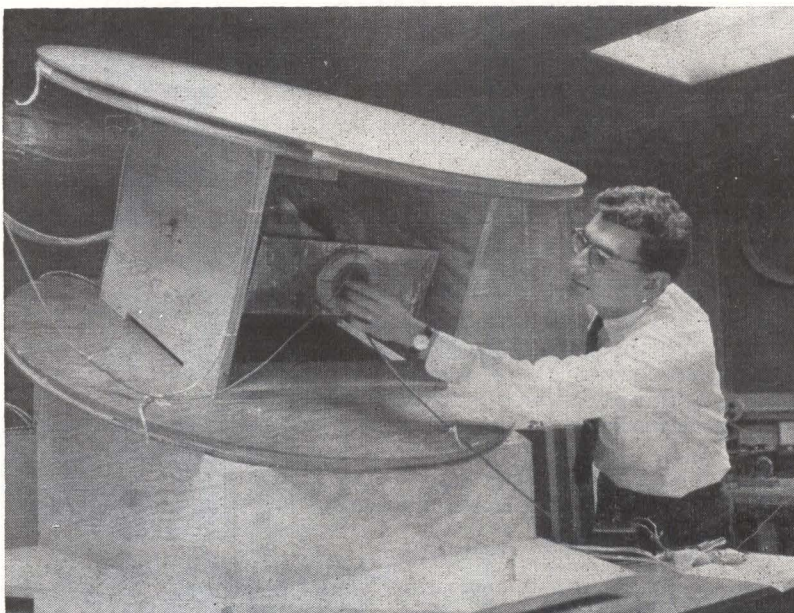
In solid-state materials, the aligned protons decay into randomness in microseconds to hours, depending on the material. However, by continuously aligning the protons with successive pulsing it is believed possible to obtain a directional reference in inertial space.

Duration and shape of the pulses have to be adjusted to the spin relaxation processes within the material. According to Berthold Zarwyn, director of Arma's basic research department, it is preferable to use materials where spin-spin relaxation time and spin-lattice relaxation time differ as little as possible since this ratio determines the gyro signal to noise ratio.

Spin-spin relaxation time characterizes the time it takes for an aligned system of spin vectors to be randomized due to interaction of proton spins. Spin-lattice relaxation time characterizes randomization time due to the fluctuating magnetic field of the lattice acting on a system of aligned spins. Ordinarily spin-lattice relaxation time is much longer than the spin-spin time in solids, whereas in liquids and gases they are almost equal.

**SENSING**—Within a time that is short relative to the spin-spin relaxation time, another pulsed magnetic field is applied and the deviation from the resonance condition that existed during the previous aligning pulse is measured. For this purpose, ordinary sensing coils are used; the induced voltage is a measure of the magnetization resulting from the spin vector alignment.

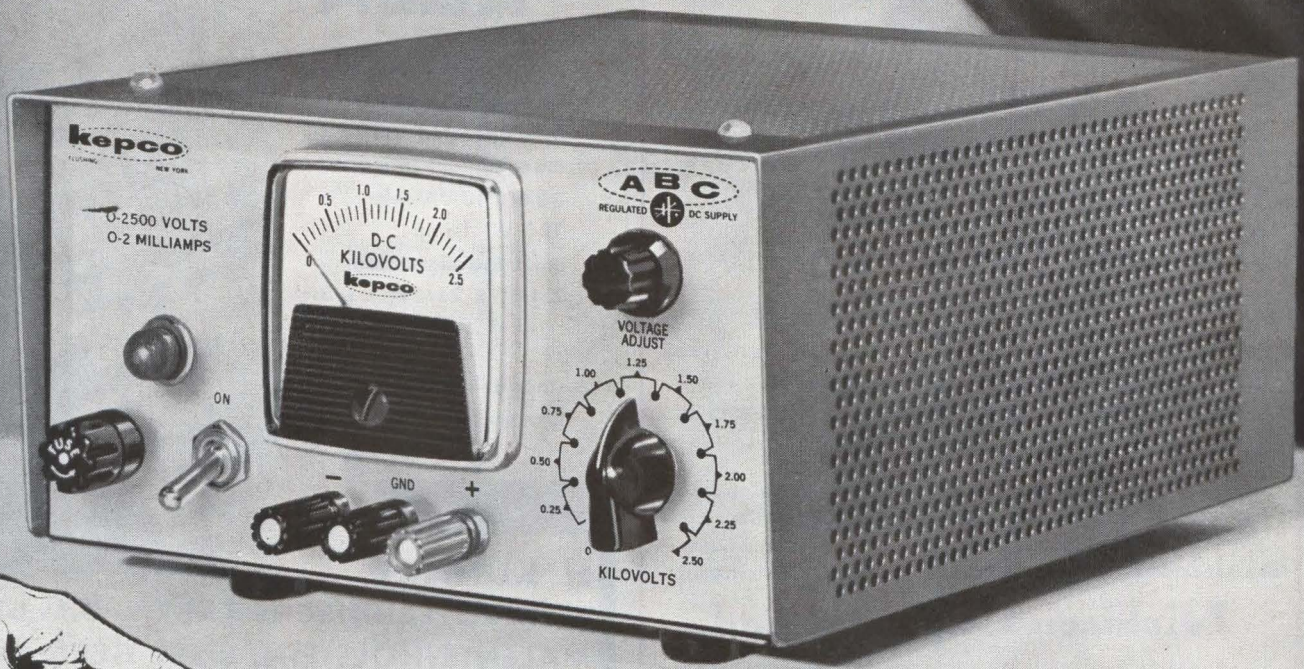
Zarwyn said his group had experimented with several solid ma-



POSITION OF sample material is adjusted in experimental model of nuclear gyroscope by Arma scientist Arthur Eberstein



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| ABC 7.5-2M  | 0-7.5           | 0-2   | 0.5               | 0.002                      | 0.01            | 0.05+0.5             | \$159 |
| ABC 15-1M   | 0-15            | 0-1   | 0.5               | 0.008                      | 0.01            | 0.02+0.2             | \$159 |
| ABC 30-0.3M | 0-30            | 0-0.3 | 0.3               | 0.05                       | 0.02            | 0.1 +1               | \$119 |
| ABC 40-0.5M | 0-40            | 0-0.5 | 0.5               | 0.04                       | 0.02            | 0.04+0.2             | \$159 |

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|-----------|-----------------|-------|-------------------|----------------------------|-----------------|----------------------|-------|
|           | VOLTS           | MA    |                   | DC to 100 CPS              | 100 CPS to 1 KC | 1 KC-100 KC (+ μhy)* |       |
| ABC 200M  | 0-200           | 0-100 | 0.5               | 1                          | 0.5             | 2+1                  | \$199 |
| ABC 425M  | 0-425           | 0-50  | 0.5               | 4                          | 1               | 2+1                  | \$199 |
| ABC 1000M | 0-1000          | 0-20  | 0.5               | 25                         | 2               | 2+1                  | \$274 |
| ABC 1500M | 0-1500          | 0-5   | 0.3               | 150                        | 2               | 2+1                  | \$274 |
| ABC 2500M | 0-2500          | 0-2   | 0.3               | 625                        | 2               | 2+1                  | \$334 |

\*Effective series inductance.

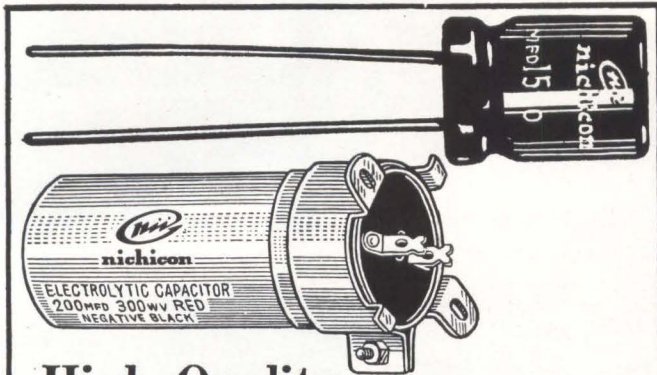
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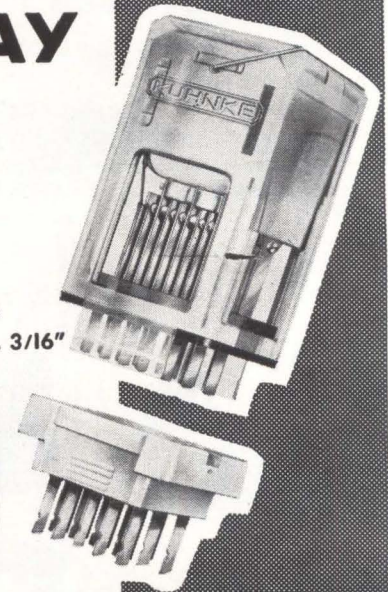
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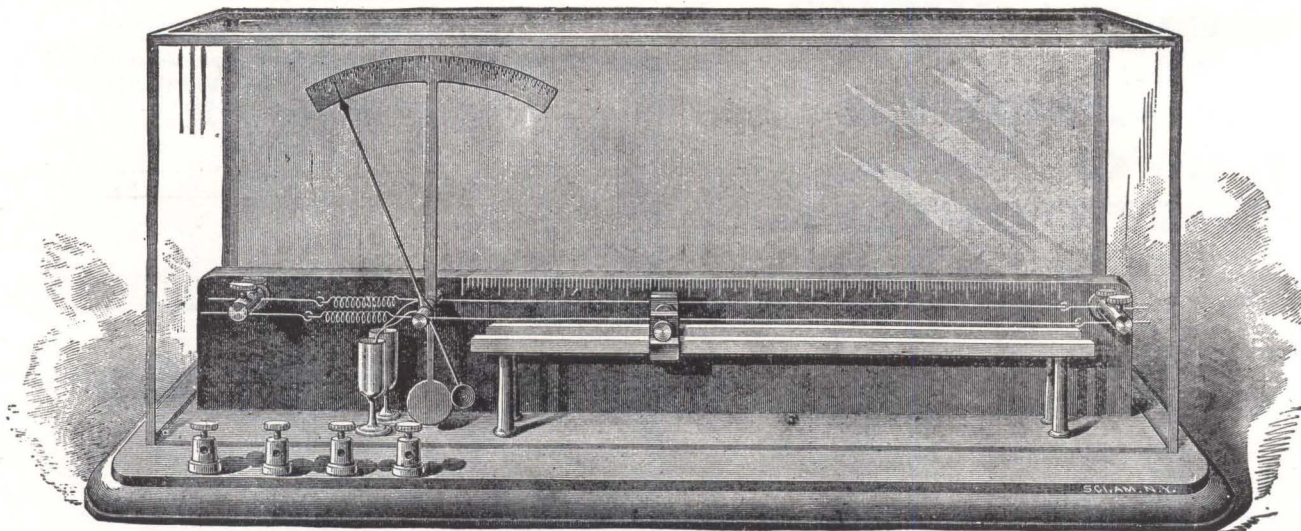
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## EXOTIC GUIDANCE SYSTEMS

Two other approaches to guidance, in addition to the nuclear gyro, are being developed by Air Force Systems Command's Research and Technology Division, and were described at the recent American Ordnance Association Meeting in New York by Major Gen. Marvin C. Demler.

- The electrostatic gyro, which exploits the suspension forces between charged surfaces to levitate a spinning spherical rotor in an evacuated case. The rotor is brought up to speeds of the order of 30,000 rpm by induction and allowed to coast down in the vacuum; this is estimated to take between 150 and 500 days.
- Guidance Using Stable Tuning Oscillators, or GUSTO, holds promise for satellites. It uses atomic clocks accurate to a part in  $10^{12}$ . One clock is in the satellite, the other on earth. The two clocks can be compared to each other, or the doppler frequency change that takes place in transmitting a signal from ground to satellite can be measured

materials having relaxation times of the order of milliseconds. Before a practical gyro can be obtained, he said, the size and weight problem caused by the use of big coils to shield the gyro from stray magnetic fields must be solved. Arma is investigating superconducting solenoids for this purpose, as well as ceramics covered with thin superconducting films which can sustain higher magnetic fields than bulk superconductors. "In our opinion this will give the necessary degree of shielding to make an actual gyro operational with the accuracy required for inertial applications and without bulky magnets," Zarwyn said. Other problems include obtaining better resolution and performance, proper switching techniques and materials selection.

The project is sponsored by the Aeronautical Systems division of Air Force Systems Command.

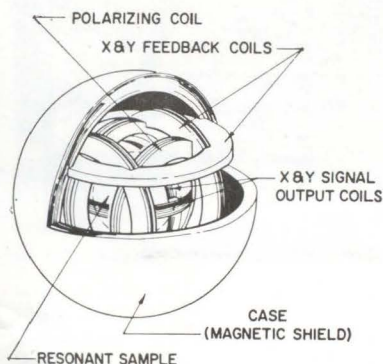
Other firms active in nuclear gyro work include GPL division of General Precision Inc. and Republic Aviation.

Republic is working on a magnetic induction gyro using water doped with paramagnetic salts. Here applied d-c and a-c magnetic fields align the nuclei. Rotation of the sample has the same effect as additional magnetic fields transverse to the original axis of alignment. These fields are measured by sensing the second harmonic content of the modulated a-c signal.

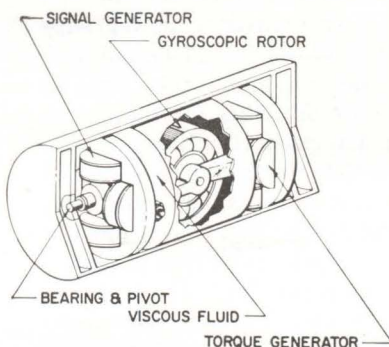
Republic is working on the gyro under contract from Navy's Bureau of Naval Weapons, claims that use of the nuclear principle provides lower drift rate than that of the best existing gyros, very low threshold, and unlimited angular motion.

General Precision is reportedly using optical pumping to align spin vectors.

MAGNETIC INDUCTION GYROSCOPE



CONVENTIONAL INTEGRATING GYROSCOPE

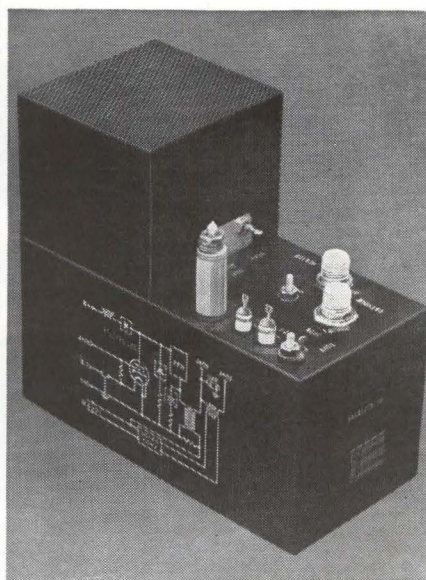


ARTIST'S VIEW of magnetic induction gyroscope under development by Republic Aviation Corp. (left) shows simplicity of construction and absence of moving parts, which is expected to eliminate the complexity and precision required of mechanical gyros (right)

# SARATOGA INDUSTRIES REPORT

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**SPECIFICATIONS** — B + 1500 volts; trigger input — 200 volt peak; variable from 200 pps to 3300 pps; recovery time, 100 Microseconds; output pulse,  $3\frac{1}{2}$  Microseconds wide; Amplitude 7.5 KV at 1.2 Amps. with rise time less than 0.3 Microseconds.

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# Will Gallium Alloys Provide New Electronic Light Source?

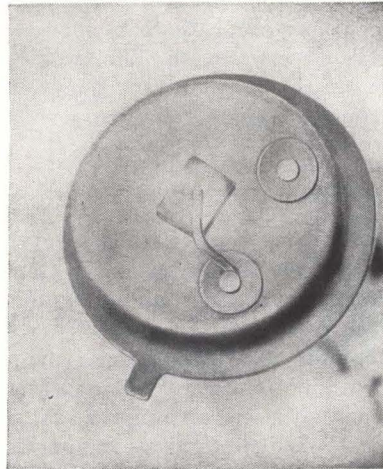
*Scientific community sees interesting potential for electroluminescent chips*

**DEVELOPMENT** of a new electroluminescent light source from a pinhead-size chip of crystalline chemical material was announced recently by General Telephone & Electronics Corporation. Although complete technical details have not been revealed, "this new diode represents a true research breakthrough with significant promise in both military and commercial lighting applications," according to Lee L. Davenport, President of GT&E Laboratories. "One or two years of further work must be accomplished, however, before its full potential can be realized," Davenport said.

The electroluminescent diode is composed of two crystalline semiconductor materials, gallium arsenide and gallium phosphide. Mechanism of injection electroluminescence, involved using these alloys, is scientifically simpler to understand than mechanisms involved using zinc sulfide or cadmium sulfide crystals. More straightforward understanding offers more chance of progress in solving existing problems connected with light efficiencies.

**RED LIGHT NOW**—Tiny crystal can convert electrical current directly into visible red light with a theoretical efficiency of 100 percent, according to GT&E. As a result, the crystal is expected to lead to a variety of applications where a small-point light source or high-directional beam is required.

Light intensity from gallium arsenide-gallium phosphide diode is typical of that obtained from gallium-arsenide diodes. Gallium arsenide differs from semiconduc-



*CRYSTAL radiates red light. Current is applied to diode through hair-like wire extending from perimeter of the mounting can*

tors like germanium or silicon in fact that light proton is produced in the former. At room temperature, overall efficiency of gallium arsenide-gallium phosphide crystal is now less than one percent. But work on internal absorption and reflection problems should result in higher efficiencies, according to company.

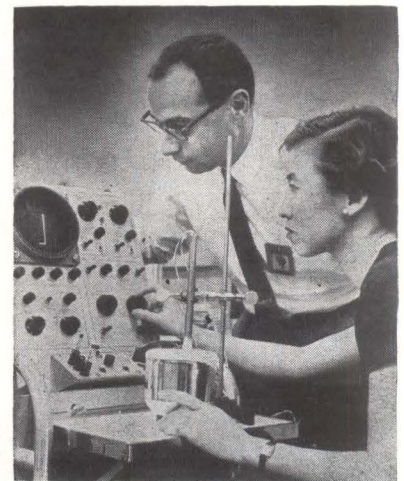
First applications of new light crystals will be in electroluminescent displays. Only a few volts are needed for power drive, and crystals can run off transistor power supplies. Therefore, it will be possible to use electroluminescent chips as tiny electronic lights for indicators in transistorized circuits.

Theoretical quantum efficiency of the gallium alloys is high. However, two practical problems still have to be solved before electronic lights can become practical. Current has to be pushed through these low-voltage diodes, and resistive losses will have to be reduced. Also, more efficient techniques will have to be developed to get the photons out of

the semiconductor junctions.

Formed from a vapor, the flat crystal diode is 1/30th of an inch square, and 1/300-in. thick. When current is applied to the face of the tiny device, its entire surface radiates an intense red light. Surface brightness of this light is substantially greater than similar red illumination from existing electroluminescent lighting. Present developmental efforts are being devoted to further increases in practical efficiency. Present work is directed toward developing efficient techniques for pushing maximum current through the diode and getting the maximum light out.

**WHITE LIGHT?** — Additional work into a variety of semiconductor materials will be directed towards broadening the range of colors emitted from the diodes with particular emphasis upon the attainment of white light for illumination purposes, according to

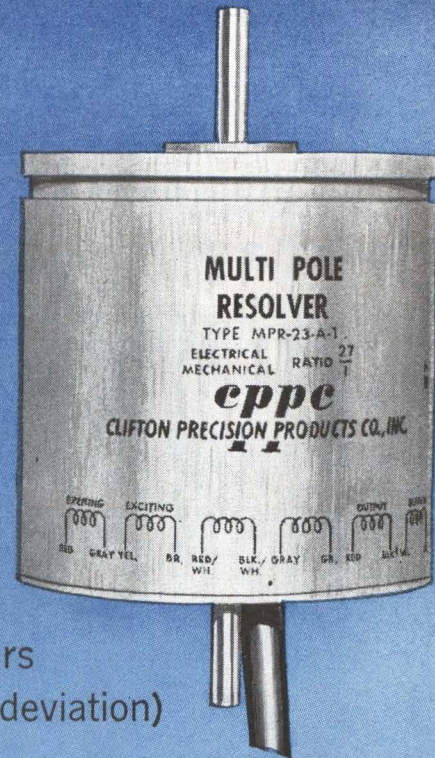


*CURRENT flow through gallium arsenide-gallium phosphide light source is viewed on oscilloscope trace by Sumner Mayburg and San-Mei Ku. During laboratory experimentation, crystal is immersed in liquid nitrogen in thermos container directly in front of Miss Ku*



# ENGINEERS!

## CONSIDER THE UNIQUE ADVANTAGES OF THE CLIFTON PRECISION VARIABLE RELUCTANCE MULTI-POLE RESOLVER



- Acts as a geared-up resolver without the gears
- Gives extreme accuracy (20 sec. of arc max. deviation)
- Constructed without slip rings and brushes

The Clifton Precision Multi-Pole Resolver is a reluctance type unit with all windings placed in the stator. Stepped-up ratios between a mechanical angle and an electrical output are obtained electrically without conventional gearing by varying the winding pattern and the number of teeth in the rotor lamination. Result—savings in cost by eliminating gears.

Another advantage of a reluctance type unit is the absence of sliding contacts with attendant elimination of brush problems such as wear, vibration and noise. In fact, life of the resolver depends on bearing life only.

Both stator and rotor are laminated. Because of the average effect inherent in a laminated construction, the accuracy of these units exceeds by many times the machining accuracy. Repeatability is better than  $\pm 3$  seconds of shaft angle and crossover null error spread over one full revolution of less than 20 seconds of arc is obtained.

This unit has been very effectively employed as a "vernier" resolver. When used in conjunction with a regular synchro resolver, extremely accurate system measurements result (see applications below).

Multi-Pole Resolvers are presently operational in the Skybolt missile and Mariner (Venus probe) tracking equipment.

For further information, contact: Sales Dept. 5050 State Rd., Drexel Hill, Pa. Area 215 MADison 2-1000, TWX 215 623-6068—or our Representatives.

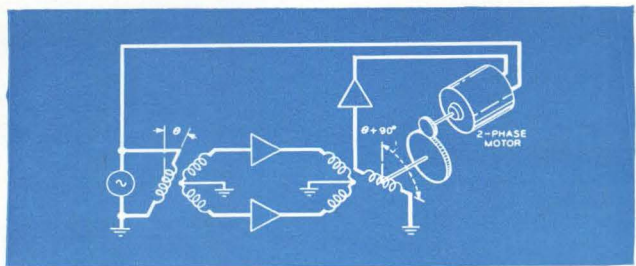
### APPLICATIONS

**VERNIER ANGLE ENCODER.** In this system a shaft and angle are converted into a pair of digital numbers (one coarse and one fine) by coupling a standard resolver directly to a multi-pole resolver.

The output of the resolver may be encoded by exciting the primary with a signal of 400 cycles per second and combining the induced secondary amplitude voltages (by means of two-phase shifting networks) into two-phase modulated voltages. The time interval between the respective zero crossings is converted into digital representation by an electronic stop watch (time encoder).

**VERNIER ANGLE READING SYSTEM.** A visual vernier angle reading system can be built by using the output of the multi-pole resolver to position a standard resolver. The control transformer resolver will go through "n" revolutions for each revolution of the multi-pole resolver (where "n" is the order of the multi-pole resolver). The reading of a dial coupled directly or through gears to the control transformer resolver provides the vernier reading. This technique is most useful in reading the position of a rotary table.

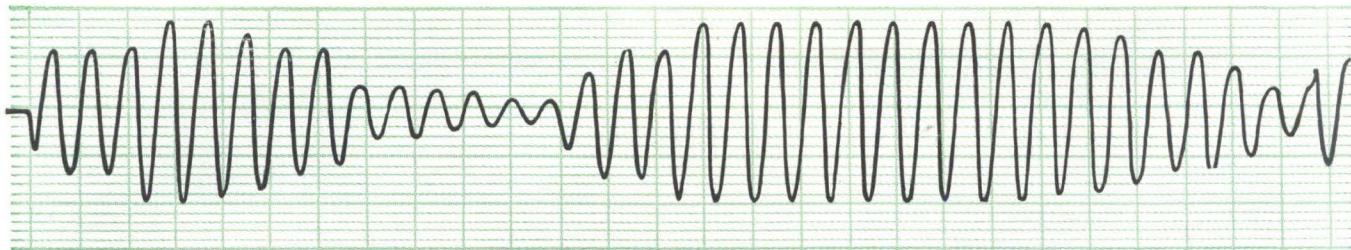
**A VERNIER FOLLOW-UP SYSTEM** can be utilized much like present two-speed synchro control transformer systems except that the geared-up synchros are replaced by multi-pole resolvers.



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company officials at GT&E.

Development of the electroluminescent diode source was accomplished by three members of a GT&E team: James F. Black, San-Mei Ku, and Harry F. Lockwood, under the supervision of Sumner Mayburg, scientists in charge of the laboratories solid-state electronics program.

Since most present electroluminescent devices operate in the green, the red light from gallium diodes should augment overall use for electroluminescent devices.

Initial use of the electroluminescent diodes likely will be as indicator lights for electronic equipment. However, according to Davenport, the new device offers greater long-range potential for specialized applications where incandescent lamps are presently used.

Several electronic laboratories are now conducting research on mechanisms of injection electroluminescence, and more reports about their work are anticipated in the coming months.

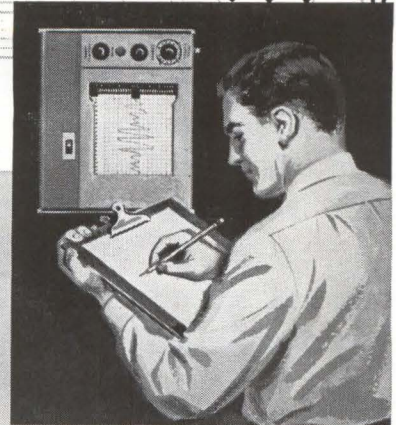
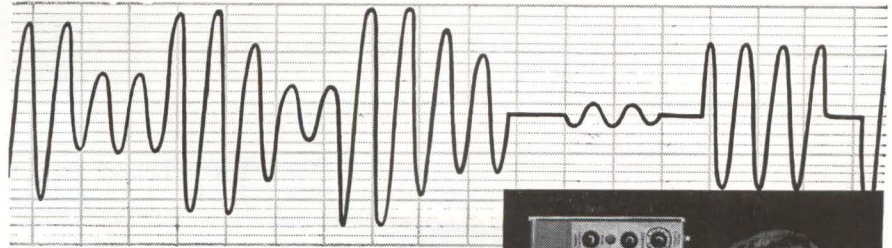
## Plastic Film Disappears In Space Environment

PLASTIC FILM that photolyzes or disappears in the environment of space has been developed by Goodyear.

The film and the wire grid for a passive communications satellite could be mated and packaged in a rocket nose cone, according to Goodyear. After launch, the film, used as a bladder, would be inflated to erect the grid structure. Ultraviolet rays from the sun would then cause the film to disappear, leaving the grid to act as a reflector for radio waves.

Goodyear sees several advantages with this technique. Since the structure does not depend on gas pressure for rigidization, it is not subject to serious degradation due to meteoroid penetration, nor will it undergo large surface changes due to thermal variations.

Similar techniques are being proposed for other applications such as space-borne antennas, Goodyear said.




# New Bausch & Lomb V.O.M.-5 RECORDER

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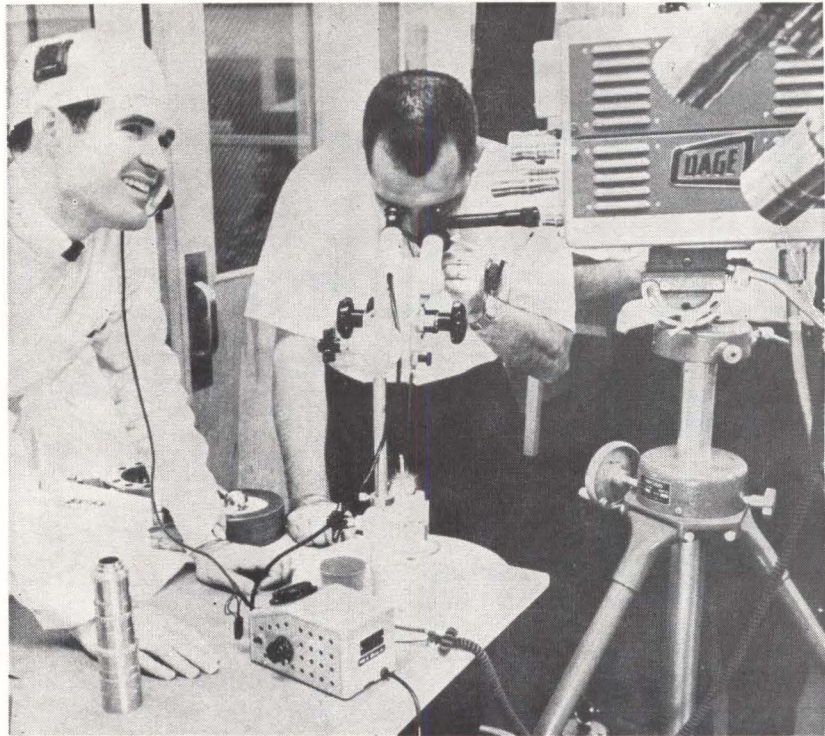
# Microscope and Tv Help Train Assemblers

*Numerous personnel simultaneously learn production techniques.*

By HARTMUT E. KELLER  
Carl Zeiss, Inc.  
Los Angeles, Calif.

**RAPID** training of many personnel in miniature assembly and finishing techniques presented quite a problem in Autonetics' production of inertial guidance system components for Minuteman intercontinental missiles. Because of drastic environmental requirements, the number of personnel in assembly rooms must be restricted to achieve precise control of temperature, humidity and dust. For example, dust count is maintained at about 5 percent of normal for production of velocity meters used in the missile's inertial navigator. This assembly operation was the first to receive the microscope-tv training preparation.

The basic idea is to spread people about in various clean assembly rooms and televise training information to them from a room containing instructor personnel. How-



SPECIAL ADAPTER enables tv camera to view miniature components through demonstration eyepiece attachment on binocular viewing tube of Epi-technoscope

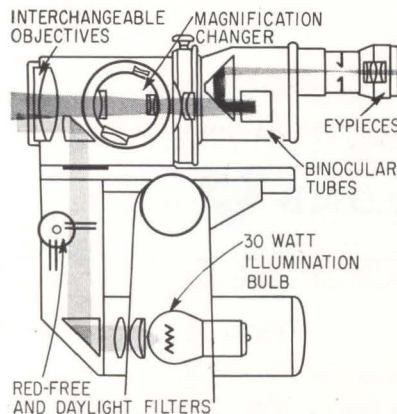
ever, microscopes normally used for assembly of miniature components are not equipped to carry a tv camera. A Carl Zeiss Epi-technoscope allows for tv camera attachment and was found to be ideal for televising miniature assembly and finishing procedures.

**VIEWING EQUIPMENT** — The Epi-technoscope is a stereoscopic instrument giving a three-dimensional image with great depth of field. A built-in magnification changer gives five magnifications, parfocal to each other. Four different focal objectives are available: 125 mm, 200 mm, 300 mm, 500 mm. The working distance with these various objectives is approximately equal to focal length. One of the outstanding features of the Epi-technoscope is the built-in light source that illuminates the object in nearly the same direction as it is observed to permit viewing

of deep-lying objects, narrow crevices, dead holes and orifices. Equipped with a binocular tube, the microscope also has demonstration attachment. Normally used for a second viewer, this attachment takes a special adapter that in turn attaches a close-up tv camera. A moveable pointer needle enables the instructor to direct attention to a specific object or motion within the instruments viewing field.

Either an inclined or straight binocular tube can be used. This assures a convenient and comfortable position of the head of the observer in any direction of observation. The binocular tubes can be used with either 12.5X or 20X eyepieces. Both are focusing eyepieces and can be supplied with reticules for very critical photographic focusing.

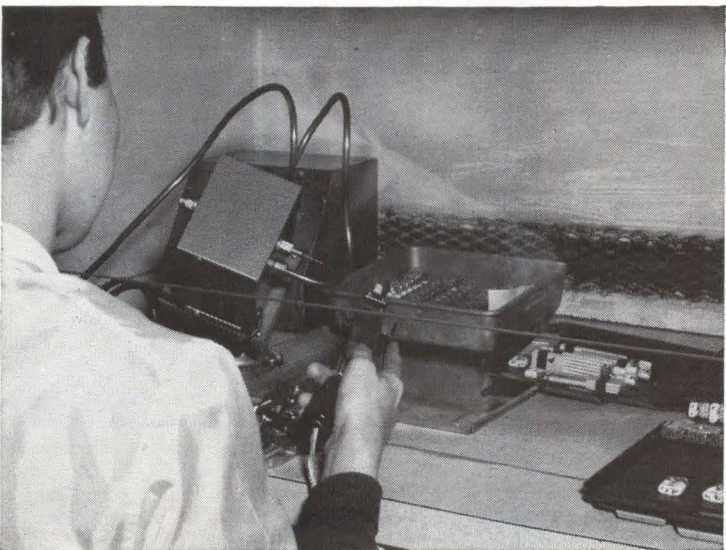
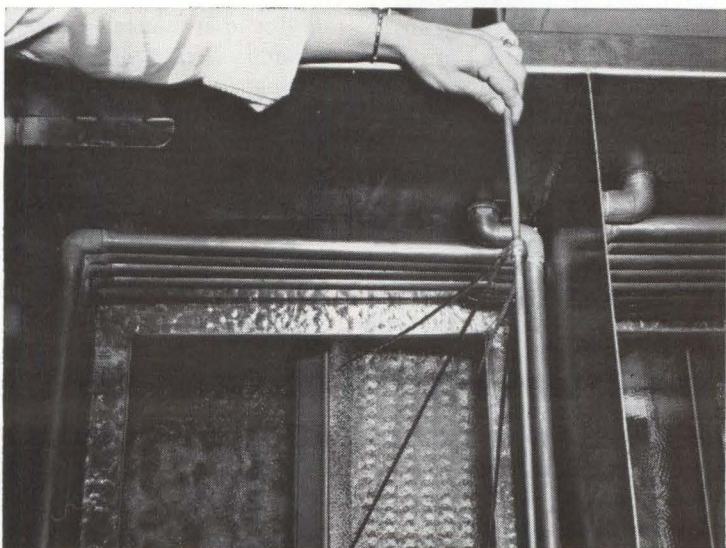
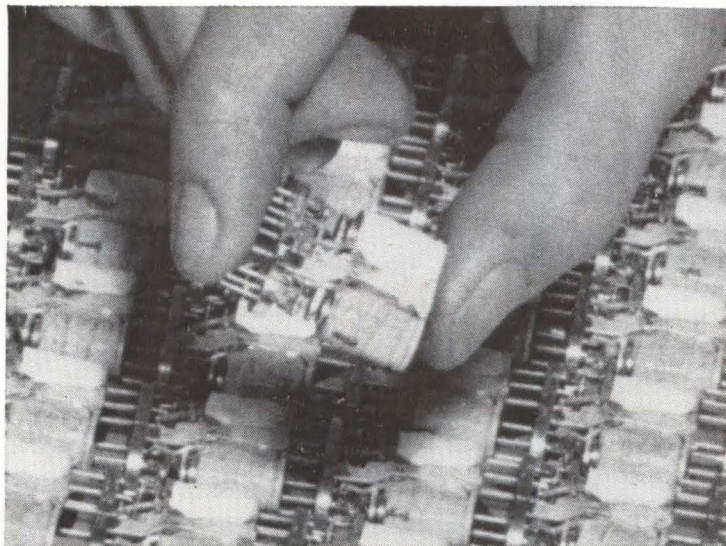
**PROCEDURE**—A continuous image of the instructor's motions, as seen through the Epi-technoscope,



ILLUMINATION is directed within microscope by optical system so that narrow cavities and deep lying objects can be viewed



# How Potter & Brumfield precision-cleans missile relays for top reliability!



**PROBLEM:** How to reduce an unacceptably high reject rate on critical "crystal-case" electrical relays (first photo) at Potter & Brumfield, Division of American Machine & Foundry Company... eliminate employee problems of headaches and nausea due to solvent vapors.

**SOLUTION:** A new cleaning system using "Freon" fluorinated solvents. "Freon" is an excellent selective cleaning agent. It removes solder flux, dust, lint and other contaminants, yet doesn't harm delicate relay parts. Also, "Freon" is virtually non-toxic, thus eliminating complaints about vapors.

In the cleaning process, a basket of relays is first given a 15-second ultrasonic bath in "Freon" TMC, then an ultrasonic bath in "Freon" TF for 15 seconds (second photo), and a 15-second rinse in TF vapor. Because of its low surface tension, "Freon" quickly penetrates the tiny spaces in the relays, allowing precision cleaning of delicate parts.

As a final cleaning step, the relay contacts are washed in a spray of "Freon" TF, while being electrically actuated (third photo). This assures that no particles are entrapped between the contacts. Only the high dielectric strength of "Freon" makes this operation possible.

According to Potter & Brumfield, the adoption of "Freon" solvent cleaning has upgraded product quality, meeting their critically high standards, equivalent to a 17% increase in production capacity while at the same time decreasing labor costs. They point out that "Freon" dries quickly and leaves no residue, and that its non-flammability and low toxicity let them operate without expensive ventilating equipment. They've found "Freon" solvents economical to use because they can be recovered in simple equipment for reuse... over and over again. Most important, "Freon" solvents have eliminated employee complaints on nausea and headaches.

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We'll be glad to give you help in selecting "Freon" solvents for use in your own cleaning operation. Just write on your letterhead to Du Pont, 2420E12 Nemours Bldg., Wilmington 98, Delaware.

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These tape drives are now operating in thousands of computer systems around the world — providing daily proof through performance of Clairex reliability!

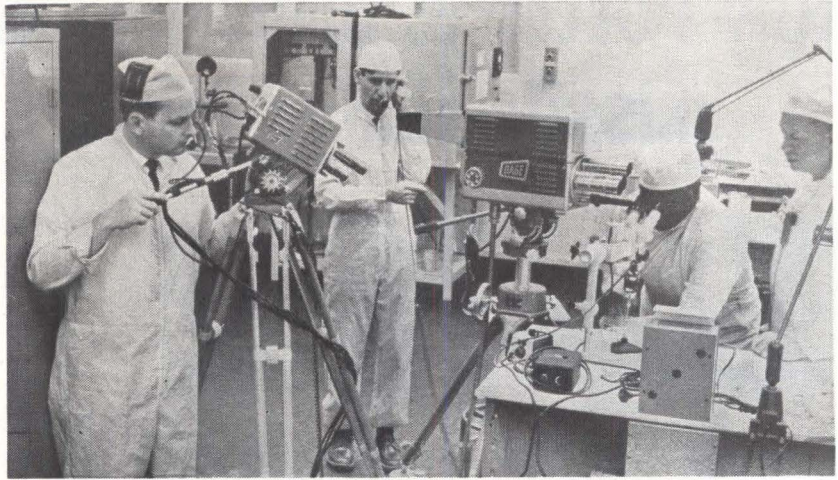
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TECHNICIAN INSTRUCTOR teaching assembly techniques and three cameramen are only personnel in main assembly clean-room. Other assembly rooms contain trainees, also in restricted numbers so as not to increase temperature, humidity and dust content

is transmitted by closed circuit tv to 4 television receivers situated in classrooms at the Autonetics plant. The image is magnified 50 to 100 times. The Epi-technoscope as used at Autonetics magnifies 40 times, with the additional enlargement provided by the tv camera and transmitting equipment. The system is able to enlarge the image of an object the size of a pencil head to fill a 21-inch screen. If required, the Epi-technoscope can provide magnifications ranging from 3 to 63 with various eyepieces and objectives.

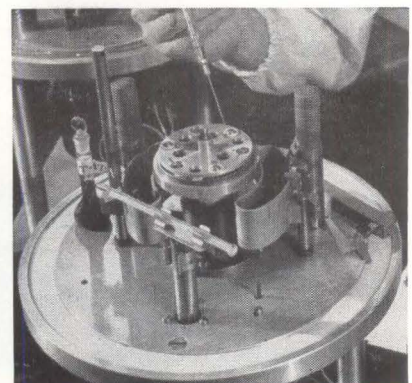
A second television camera is used in the clean room to transmit long-range views of the instrument and its operator in normal size.

**FILM PRODUCTION** — Taped training films are produced by Autonetics by means of the same microscope-television combination. Such films came increasingly into demand as the Minuteman missile neared production status and training activity increased accordingly. Television tape has two advantages over motion picture film for this application, Autonetics points out. First, tv tapes can be recorded with normal light, whereas motion picture films would require special lighting and other technical arrangements not permissible in dust-free areas. Second, tapes can be viewed immediately, and segments re-taped on the spot if necessary.

## Blue Print Distribution with 2-Mile Tubes

INSTALLATION of a pneumatic carrier system for distributing blueprints to shop areas is being done at Boeing's Transport Division. Expected to pay for itself within a year through time savings, the system cost \$150,000 and uses more than 2 miles of oval-shaped tubing that connects central files to 19 blueprint stations around the plant. Prints placed in 18-inch long cylindrical carriers travel at 35 feet per second; 3,200 prints can be routed in one hour. Digital coding technique routes carrier through system switches to proper station.

## Bearings Evaluated



LIFE of memory-drum bearings is determined by Sperry Gyroscope Ball Bearing Simulator. Test time has been cut to 1/200 of previous run-to-failure tests.



# EDITORIAL INDEX

# electronics

July through December, 1962, Vol. 35

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(See also Converters; Power Supplies)

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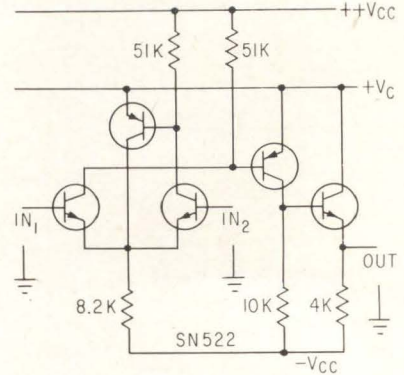
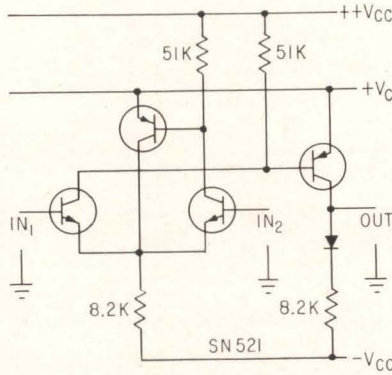
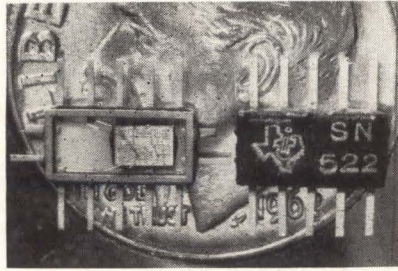
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## Operational Amplifiers Are Getting Smaller

*Integrated circuits have pnp and npn transistors in single silicon block*

**ANNOUNCED** by Texas Instruments Inc., Semiconductor-Components Div., P. O. Box 5012, Dallas 22, Texas, the series 52 linear versions of fully integrated circuits consists of the SN521 basic d-c operational amplifier and the SN522 which is essentially the same amplifier with emitter-follower output. The SN521 open-loop voltage gain is 62 db, common-mode rejection is

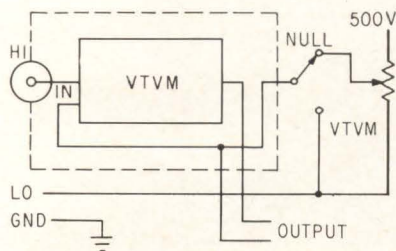
58 db, d-c offset referred to input is 2 mv and  $\frac{1}{2}$ -power frequency point is 60 Kc. Input impedance is 18,000 ohms differential and 10,000 ohms to ground, output impedance is 8,000 ohms and d-c drift referred to input is 10  $\mu$ v per degree C. The SN522 has the same characteristics except output impedance is 150 ohms. The new series are mounted in a flat-form, hermetically-sealed package  $\frac{1}{4} \times \frac{1}{8} \times \frac{1}{2}$  inch and weighs less than 0.1 gram. For the first time, two pnp and five npn transistors have been diffused in a single block of silicon. Each transistor can be used as a single diode

if desired. The circuit bar also contains six tapped resistors with values from 5,000 to 50,000 ohms. The simultaneous-diffusion fabrication technique results in transistor closely matched inputs and since all components are in close thermal contact, excellent input match is maintained throughout operational temperature range. Use is in analog-to-digital converters, feedback amplifiers, integrators, differentiators, servo and other drive amplifiers.

CIRCLE 301, READER SERVICE CARD

## Measuring Differential Voltages from 10 Microvolts

**NEW** from Keithley Instruments, Inc., 12415 Euclid Ave., Cleveland 6, Ohio, the model 660 Guarded Differential Voltmeter is a potentiometric design that operates between 10  $\mu$ v and 500 v, and features a 0.02 percent limit of error for readings between 100 mv and 500 v



with 0.005 percent repeatability. A zener reference, stable to 0.002 percent per year results in a power supply stability better than 0.005 percent indefinitely. Maximum null sensitivity is 100  $\mu$ v full scale with 2  $\mu$ v resolution. Other features are in-line digital readout with automatically-lighted decimals, 10 mv recorder output, polarity switch, floating operation up to 500 v off ground, eleven vtvm ranges, better than 45 db of 60 cps rejection and fast overload recovery. Overall stability of 0.01 percent per 24 hours is useful for extended measurement duration. The device operates by the potentiometric method with a

stable 500 v supply. A Kelvin-Varley divider (see sketch) performs the potentiometer function and a chopper-stabilized vtvm is the null detector. Full guarding of the input and null detector avoids leakage. Voltage required for true null is read from five in-line dials. (302)

## Low Noise Amplifier Has High Input Impedance

DEVELOPED by Denro Labs., 2801 15th St., N. W., Washington 9, D. C., the type 600 series Micronoise amplifiers have an input impedance



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PHOTO R. BOUILLOT

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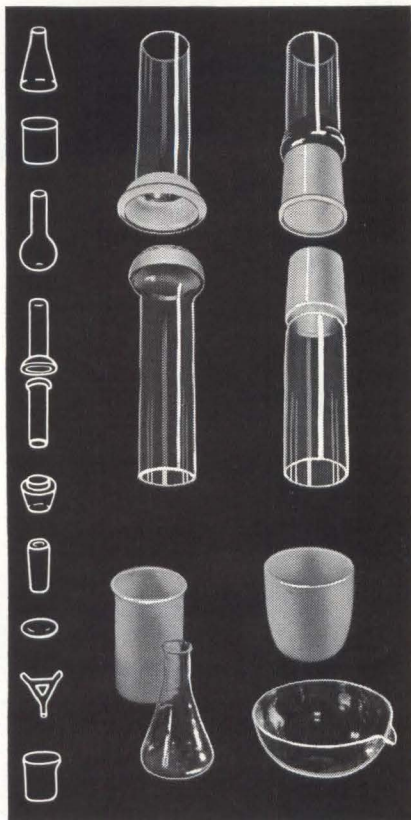
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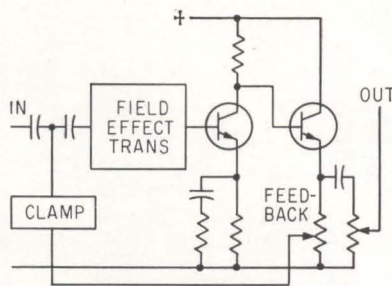
For more details see Chemical Engineering Catalog, Electronic Engineers Master, or write for our 32 page catalog.

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RT. 202 & CHANGE BRIDGE RD.  
MONTVILLE, NEW JERSEY

resistive component of over 60 meg-ohms shunted by less than 100 pf, integrated noise under 8  $\mu\text{v}$  referred to open or shorted input over a 50 Kc bandwidth, a frequency response between 5 cps and 20 Kc  $\pm 1$  db and 1.5 cps to 50 Kc  $\pm 3$  db and a voltage gain between 10 and 50. Output impedance is 3,000 ohms at 0.75 v rms and rise time is approximately 10  $\mu\text{secs}$ . The device is intended for low-level measurements where high input impedance and minimum noise are required. It's small size ( $1\frac{1}{2} \times 2\frac{1}{2} \times 4\frac{1}{2}$  inches) and weight (9 oz) permits convenient locating. In the sketch, the field-effect transistor has a typical input resistance of over 100 meg-ohms shunted by less than 100 pf. The integrated noise with input open or shorted is under 8  $\mu\text{v}$  rms

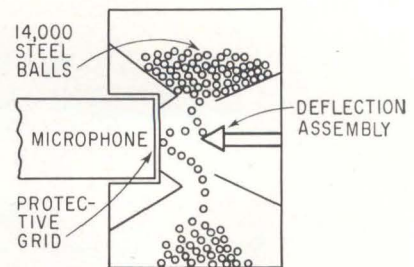


permitting detachable signal energies in the order of  $10^{-17}$  to  $10^{-18}$  watts at the low-frequency end. To avoid junction saturation and long capacitor discharge time from excess input signals, a fast-responding, high-impedance, low-noise clamping circuit is used. Recovery time is 1 to 2 seconds from a 500 v overload at the input. Under normal operating conditions, the clamping circuit presents over 1,000 meg-ohms resistive and 10 pF maximum capacitive loading to the input with noise contribution of 1  $\mu\text{v}$  rms in total bandwidth. The field-effect stage is followed by a medium-gain degenerated stage feeding the low (3,000-ohms) output impedance emitter follower. Devices are available with either BNC or UHF (female) connectors.

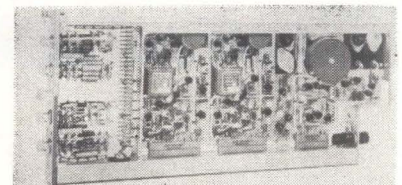
CIRCLE 303, READER SERVICE CARD

### Microphone Calibrator Generates White Noise

ANNOUNCED by B & K Instruments, Inc., 3044 West 106 St., Cleveland



11, Ohio, the noise source model 4240 is a small mechanical-acoustical device producing an approximate white noise spectrum with nearly Gaussian amplitude distribution. It can be mounted on a microphone for quick and reliable field calibration check of sound level meters. Each noise source is individually calibrated to an accuracy of  $\pm 1.5$  db and basically consists of two chambers containing approximately 14,000, 1-mm steel balls. During operation, the balls fall from the upper chamber and strike a metal diaphragm while dropping to the lower chamber. This procedure lasts for about 14 seconds and may be repeated by rotating the plastic housing through 180-degrees. The balls striking the metal diaphragm cause an rms sound pressure level of approximately 108 db to be produced at the microphone diaphragm. (304)



### D-C Amplifier Is Dual Channel Unit

REDCOR CORP., 7760 Deering Ave., Canoga Park, Calif. Model 500 is a dual channel d-c amplifier. Two single-ended amplifiers are contained in one case with a common power supply. Embodying completely solid-state design, the plug-in circuit cards used in the amplifier are interchangeable with those in the model 361 differential amplifier. Features include: adjustable gain and bandwidth; bandwidth unaffected by gain change; low noise level; high output current; high input impedance; extreme accuracy, linearity and stability. (305)



# Literature of the Week

**PHOTOELECTRIC PULSE GENERATORS** Dr. Johannes Heidenhain, 8225 Traunreut Uber Traunstein, Western Germany, has published a brochure on photoelectric pulse generators for the measurement of length, angles and revolutions. (306)

**CRYOGENIC QUALITY METER** Space Sciences, Inc., Natick, Mass. Product data describing a new, high-accuracy cryogenic quality meter have been published. (307)

**AIR CORE INDUCTORS** Illumitronic Engineering Corp., 680 E. Taylor Ave., Sunnyvale, Calif., has available a 10 page folder on air core inductors featuring highest heat resistance up to 500 F. (308)

**SOUND-LEVEL METER** B&K Instruments, Inc., 3044 W. 106th St., Cleveland 11, O. An 8-page brochure on the model 2203 precision sound level meter and 1613 octave filter set is announced. (309)

**TWO-POLE RELAY** Branson Corp., 41 S. Jefferson Road, Whippany, N. J. Technical bulletin covers half-size crystal can relay, model SR, which permits close stacking of p-c boards and dense switching per unit volume. (310)

**MICRO DIODES** Micro Semiconductor Corp., 11250 Playa Court, Culver City, Calif. Bulletin 119 describes high power (1.5 w) fast recovery (0.5  $\mu$ sec) micro diodes. (311)

**ANALOG/DIGITAL COMPONENTS** Scientific Data Systems, Inc., 1649 Seventeenth St., Santa Monica, Calif. An 8-page bulletin gives full information on a line of fast, low cost silicon analog/digital systems components. (312)

**R-F SHIELDED ENCLOSURE** Erik A. Lindgren & Associates, Inc., 4515 N. Ravenswood Ave., Chicago 45, Ill. Singlesheet brochure contains description, specifications, performance data and prices of a new portable r-f shielded enclosure. (313)

**LAMINATED PLASTICS** Insurok Division of The Richardson Co., DeKalb, Ill., has published an engineering booklet about high pressure laminated plastics, properties, characteristics and applications. (314)

**SPACE AGE ELECTRONICS** DuKane Corp., St. Charles, Ill., has published an illustrated brochure outlining its capabilities in the design and manufacture of space age electronic equipment. (315)

**STRAP FRAME GRID TUBES** Sylvania Electric Products Inc., 1100 Main St., Buffalo 9, N. Y., offers a booklet titled "Strap Frame Grid Subminiature Tube Manual." (316)

**CERAMIC TRANSDUCERS** Gulton Industries, Inc., 212 Durham Ave., Metuchen, N. J. An 8-page brochure

covers Glennite ceramic transducers, including high-temperature transducers. (317)

**SCIENCE SERVICES** Texas Instruments Inc., 1100 Exchange Bank Building, Dallas 35, Texas. An illustrated brochure describes the company's part in government and commercial programs which span the spectrum of earth and space science technologies. (318)

**RECORDER/REPRODUCER** Magnasync Corp., 5546 Satsuma Ave., N. Hollywood, Calif. Four-page brochure illustrates and describes model TR-1510 multichannel recorder/reproducer for audio monitoring. (319)

**PRODUCTS DIRECTORY** General Electric Co., Schenectady 5, N. Y. Directory lists all the company's electronic component-products, and for each product, gives all direct sales locations by state and city. (320)

**DIGITAL VOLTMETER** Cohu Electronics, Inc., KinTel Div., 5725 Kearny Villa Road, San Diego 12, Calif. Data sheet describes a digital voltmeter for submarine and other special environment applications. (321)

**LIGHTWEIGHT LASER SYSTEM** Maser Optics, Inc., 89 Brighton Ave., Boston 34, Mass. Bulletin illustrates and describes series 600 lightweight laser system designed for operation at room temperatures. (322)

**METAL FILM RESISTORS** Mepco, Inc., 37 Abnett Ave., Morristown, N. J., has issued a revised technical data sheet covering its type FE metal film resistors. (323)

**MICROWAVE COMPONENTS** Alpha Microwave, Inc., 381 Elliot St., Newton Upper Falls 64, Mass., offers a brochure describing its facilities for designing and manufacturing microwave components. (324)

**WAVEGUIDE COMPONENT SUPPORT** Orbitronics, Inc., 3660 E. 40th Ave., Denver 5, Colo. Four-page bulletin discusses microwave waveguide component support which eliminates the problems of alignment and transportation. (325)

**SILICON TRANSISTORS** Transitron Electronic Corp., Wakefield, Mass., offers a bulletin on the 2N2427 low level diffused mesa type small signal silicon transistors. (326)

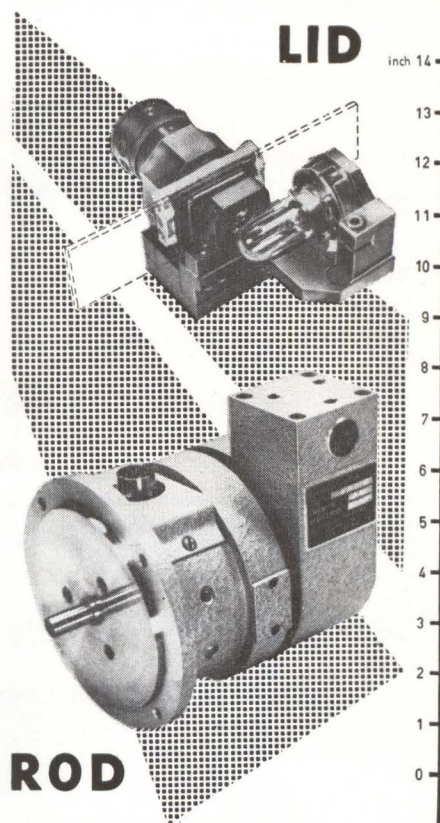
**TRANSDUCERS** U.S. Gauge, a division of Ametek, Inc., Sellersville, Pa. Bulletin F-057 describes a potentiometer pressure transducer designed to withstand 50 g shock and acceleration loads. (327)

**ONE-PART EPOXY RESIN SYSTEM** Minnesota Mining & Mfg. Co., 2501 Hudson Rd., St. Paul 19, Minn., has published a bulletin on Scotchcast brand resin No. 291, a one-part filled, semi-flexible, 100 percent solids epoxy resin system. (328)

## PHOTO-ELECTRIC PULSE GENERATORS

fo

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ANGLE-MEASURING  
SPEED-MEASURING  
REVOLUTION-MEASURING



RESOLUTION TILL 0,01 mm  
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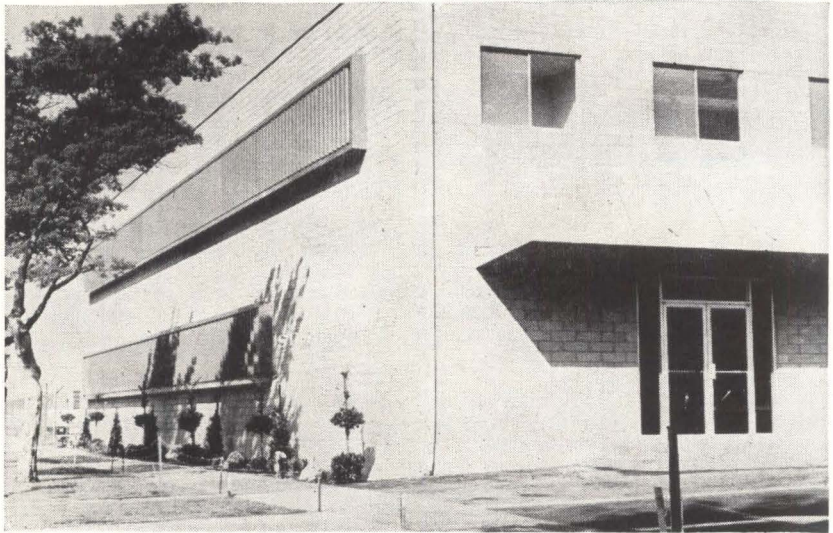
# Computer Maker Occupies New Plant

**SCIENTIFIC DATA SYSTEMS, Inc.**, has moved its engineering and administrative staffs into a new 19,000-square-foot, two-story building in Santa Monica, Calif.

Max Palevsky, SDS president, said that there are now 85 people in the new facility and it could comfortably house 150. Plans are to construct a modular addition of approximately the same size next summer.

A glassed-in computer display room off the lobby contains an operating SDS 920 system. On the second floor there is a program preparation room and two classrooms for programming and maintenance classes. Classes in both functions are conducted by SDS every six weeks.

SDS' original quarters in Santa



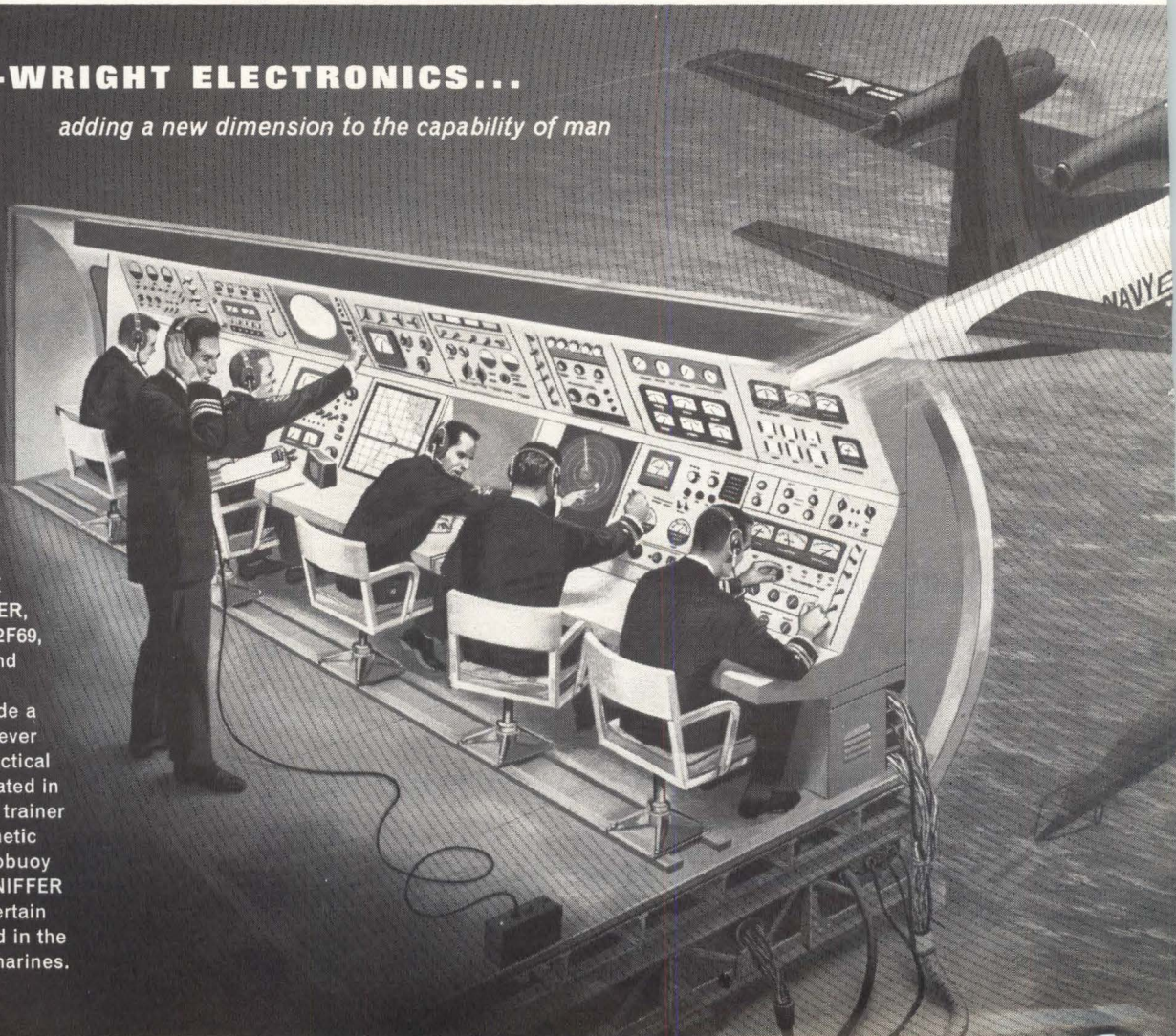
Monica, with 11,000 square feet, will house computer and component production units.

The company is shipping one computer a week now and expects to ship two a week by next fall.

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**ANTI-SUBMARINE WARFARE TRAINER**, designated Device 2F69, combines analog and digital computer techniques to provide a degree of realism never before achieved. Tactical systems fully simulated in this Curtiss-Wright trainer include radar, magnetic anomaly, Julie sonobuoy system, Jezebel, SNIFFER trail detector and certain other weapons used in the destruction of submarines.





The present backlog is approximately \$2.5 million. SDS manufactures the 910 and 920 computers, digital components including analog-to-digital and digital-to-analog, converters and multiplexers, and digital systems. The company was formed in 1961.

### Lear Siegler Forms Defense Systems Group

IN A MOVE to strengthen its position in the military systems contract field, Lear Siegler, Inc., Santa Monica, Calif., has formed a new group called Defense Systems Operations, according to an announcement by John G. Brooks, chairman of the board.

Named to head the new organization is Dan W. Burns, a corporate vice president.

Brooks said Defense Systems Operations is designed to make the most effective use of the capabilities of Lear Siegler's six divisions and one subsidiary engaged in military contract work. These are As-

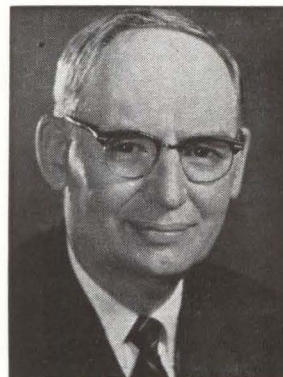
tronics, Astro Structures and Electronic Instrumentation—all in California; Data and Controls, Long Island City, N. Y.; Instrument, Grand Rapids, Mich.; Power Equipment, Cleveland, O.; and Lear Siegler Service, Inc., based in Grand Rapids, Mich.

Defense Systems will be responsible for multi-division efforts in systems relating primarily to tracking and control; communication and data; range instrumentation and support; instrumented satellite and space probes and tactical weapons.

### General Instrument Names Meinken

THE AUTOMATIC MFG. DIVISION of General Instrument Corp., with plants at Newark, N. J., and Beckley, W. Va., has announced appointment of Kenneth C. Meinken, Jr. as vice president. He will share operating responsibilities with Patrick J. Brady, vice president of the division since 1957.

Meinken left the division in 1956. Prior to rejoining General Instrument, he was vice president of General Atronics' Electronic Tube and Instrument division, in Philadelphia, Pa.



### DeForest Pioneers Elect President

AT THE ANNUAL MEETING of the DeForest Pioneers, Inc., recently held in New York City, Sidney A. Wood (picture) was elected president of the organization. He succeeds Allen

## PROJECT IN POINT: This P3V crew thinks it is closing on an enemy sub!

Simulation reflects the ultimate in the *application* of science and technology. It is the electronic bridge from research to reality. At Curtiss-Wright, electronics simulation systems orient men and machines to missions for many military and industrial programs.

**Project in Point:** At the Patuxent River Naval Air Station, P3V crews will receive both flight and tactics training on the most complete anti-submarine warfare trainer ever developed. Designed and manufactured by Curtiss-Wright in conjunction with the U.S. Naval Training Device Center, the simulator permits *entire* missions

to be "flown"—search, classification, localization, attack, and destruction of enemy submarines.

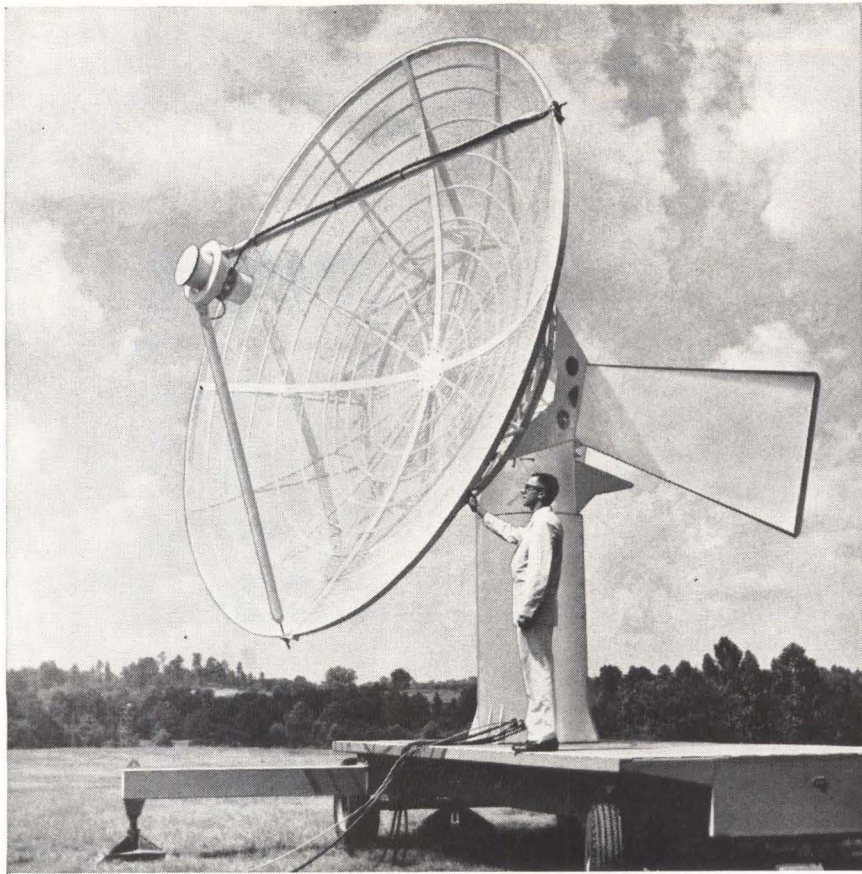
Advanced activities like this have created immediate opportunities at Curtiss-Wright Electronics Division for solid state circuit designers, digital computer programmers and others experienced in the application of real-time digital computation to the most challenging problems in simulation. For complete information, please write Mr. Gene Y. Kelly, Manager of Professional Placement, Electronics Division. An equal opportunity employer.



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# SCIENTIFIC-ATLANTA, INC.

20

B. DuMont, New Jersey industrialist and electronic scientist.

Wood is chairman of the board of Wilbur B. Driver Co., Newark manufacturer of electrical and electronic alloys.

DeForest, inventor of the three-element vacuum tube and often referred to as the Father of Radio and Electronics, died in June, 1961, at the age of 86.

The DeForest Pioneers, Inc. was organized in 1952, and according to their by-laws "for the express purpose of bringing together the men who worked and associated with Dr. DeForest, to perpetuate the memories of those days and to pay tribute to his transcendent genius."



National Company Names Sproul

ROBERT SPROUL has been appointed director of engineering of National Co., Inc., Malden, Mass.

Starting with the company as a section head in 1957, Sproul advanced to the post of chief engineer of the Communications Systems department. In this capacity he coordinated several of the company's major military communications systems developments.

## Ling Electronics Advances Klein

LING ELECTRONICS division of Ling-Temco-Vought, Inc., Dallas, Texas, has announced the promotion of E. P. Klein to executive manager of engineering, a new position created with the reorganization of the division's engineering department.

Serving on Klein's staff are



Emory Johnson, chief engineer, high-power electronics; Ken Metzgar, chief engineer, environmental products; Al Carr, chief manufacturing engineer; Scott Cooper, manager of engineering test; and Al Landsman, manager of engineering services.

Klein was formerly Ling's chief systems engineer.

## PEOPLE IN BRIEF

**F. Robert Naka** moves up to technical director for control and sensor systems development at The Mitre Corp. **Robert H. Damghajian**, formerly with Bendix Corp., joins the Industrial Electronics div. of Aero Service Corp. **Theodore H. Crane** promoted to director of research and product development at High Vacuum Equipment Corp. **R. L. Halpern**, previously with Lockheed Aircraft Corp., appointed director of electronic systems at Northrop Ventura. **Edward E. Bauman**, ex-North Electric Co., named v-p and elected to board of directors of Signalite Inc. **H. D. Sprinkle** leaves Litton Systems Inc. to become mgr. of Sylvania's Systems Technology Laboratory. **Herbert C. Cress**, consultant to Huyck Systems Co., is appointed works mgr. Chicago Aerial Industries advances **John H. Wolvin** to director of research, and **Jerome S. Goldhammer** to staff assistant for planning. **Herbert C. Jenkins**, from Sonotone Corp. to Burroughs Corp. as quality assurance and reliability mgr. for the Electronic Components div. **John D. Stimson** promoted to mgr. of the United AeroSpace div. of United Electrodynamics, Inc. Operations Evaluation Group ups **George A. Westlund** to chief of the computer section. **David F. Sanders**, former president of Lockheed Electronics Co., announces formation of Squires-Sanders, Inc., of which he will be president. Vice president of the new firm will be **W. K. Squires**, former chief scientist for Lockheed Electronics. **Alexander Kreithen** elevated to v-p of Documentation Inc.

December 28, 1962



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# NOW FROM SPERRY

Megawatts at L band . . .

A megawatt or more at X band . . .

or in between



TYPICAL TUBES FROM SPERRY'S MEGAWATT LINE

| Type    | Frequency<br>Mc | Bandwidth<br>Mc (1 db) | Peak Po<br>MW | Avg Po<br>kW | Gain<br>db | Joules/<br>Pulse |
|---------|-----------------|------------------------|---------------|--------------|------------|------------------|
| SAL-305 | 1215-1365       | 150                    | 12.5          | 60           | 36         | 375              |
| SAL-320 | 1300            | *                      | 20            | 60           | 50         | 600              |
| SAS-159 | 2856            | *                      | 25            | 24           | 50         | 62.5             |
| SAC-167 | 5400-5800       | 100                    | 1.25          | 8            | 47         | 37.5             |
| SAX-151 | 9000-9500       | 500                    | 1.0           | 10           | 40         | 30               |
| SAX-191 | 8830-9200       | 370                    | 1.25          | 6            | 50         | 37.5             |

\*Fixed-tuned—optimized for linear accelerator service.

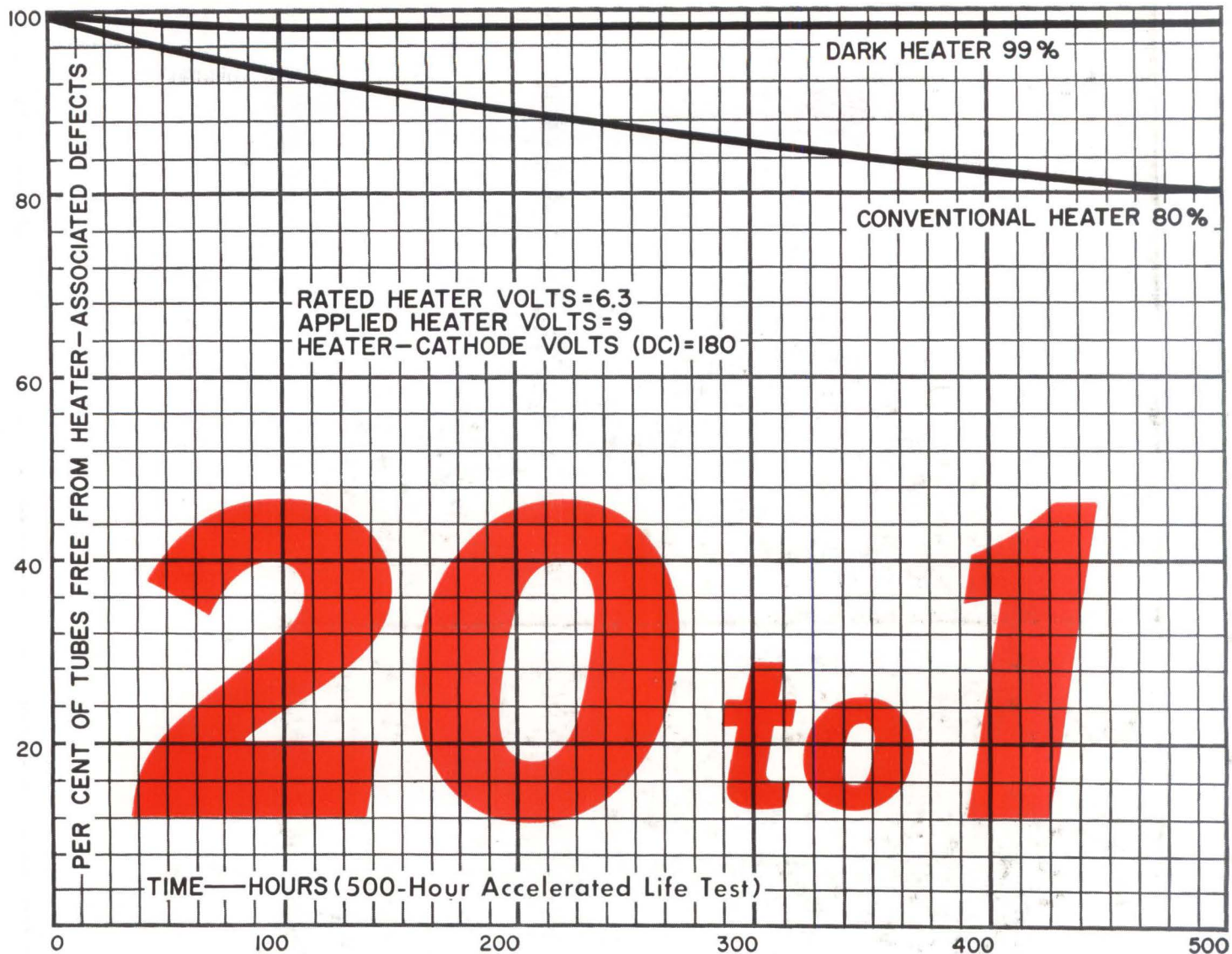
For details on Sperry's broadband, high average power, phase linear, high pulse energy megawatt klystrons, write Section 169. Information about a wide selection of classified Sperry microwave tubes is available with proper security clearance and "need to know." Sperry is represented nationally by Cain & Co.



SPERRY RAND CORPORATION  
GAINESVILLE, FLA. / GREAT NECK, N. Y.

CIRCLE 901 ON READER SERVICE CARD





## *reduction in tube failure due to heater-associated defects with revolutionary new RCA "Dark Heater"*



Reduction of tube failures due to heater-associated defects by the amazing factor of 20 to 1 after a 500-hour accelerated heater life cycling test—that's the latest performance triumph chalked up by the revolutionary RCA "Dark Heater". While

tubes with conventional heaters experienced 20 heater-associated defects per 100 tubes, tubes with the "Dark Heater" experienced only one!

Tests were conducted at 143% of rated heater voltage (9 volts for a 6.3-volt type) and at a heater-cathode voltage of 180 volts. Operating cycle was one minute on two minutes off. These 500-hour life tests are the equivalent of operation of a heater for 14,500 hours at normal heater voltage. These tests represented more than a quarter of a million tube hours.

The principle of this remarkable electron tube innovation is quite simple. Since a dark

body emits heat more efficiently than a white body, the "Dark Heater" can operate at about 350°K below the temperature of a conventional heater—yet still produce the required cathode temperature. This means:

- **Longer Heater Life**—as the tests prove, these lower temperatures result in a 50% increase in the ultimate tensile strength of the operating heater wire, and reduce internal stress by 25% during heater "on-off" cycling.
- **Less Chance of Heater Failure.** Reduced operating temperatures and smaller thermal change in cycling minimize tendency toward recrystallization and burnout.
- **Heater-Current Stability on Life.** Conventional heaters often show rising heater current characteristic on life. The "Dark Heater", however, maintains a remarkably stable current characteristic throughout its life.

- **Reduced AC Heater-Cathode Leakage and Hum.** Use of the "Dark Heater" reduces AC leakage and hum particularly "spike" or pulse leakage currents. In addition, lower heater temperature reduces both AC and DC leakage from heater to cathode and heater emission to other tube electrodes.

- **Improved Mechanical Stability.** Cooler operation minimizes changes in heater shape during life, reducing the chance of heater damage or shorts.

- **Greater Safety Margin in H-K Voltage Ratings.** Cooler operation means greater safety margin in present H-K voltage ratings.

Engineering is complete on the inclusion of the Dark Heater in some 200 of the most popular, high-volume OEM RCA receiving tubes—and most are already being delivered. For full information on "Dark Heater" tube types now (or soon to be) available, consult your RCA Field Office.



The Most Trusted Name in Electronics

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